ANALYSIS OF A VARIABLE SPEED DOUBLE-FED INDUCTION GENERATOR WIND TURBINE DURING NETWORK VOLTAGE UNBALANCE CONDITIONS.

Joseph Kearney  
*Technological University Dublin*, joseph.kearney@tudublin.ie

Michael Conlon  
*Technological University Dublin*, michael.conlon@tudublin.ie

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ANALYSIS OF A VARIABLE SPEED DOUBLE-FED INDUCTION GENERATOR WIND TURBINE DURING NETWORK VOLTAGE UNBALANCE CONDITIONS.

Joseph Kearney and Michael F Conlon
Dublin Institute of Technology, Ireland

ABSTRACT
The behaviour of Double-Fed Induction Generators to supply network voltage unbalance is investigated. The paper shows the effects that voltage unbalance can have on a DFIG, using Matlab/Simulink. The results from simulations show that voltage unbalance affects both the induction generator and the rotor converter, due to the high unbalanced currents generated. The ability to modify the control strategy of a DFIG to compensate for voltage unbalance is outlined and simulations show the improvements to the performance of the DFIG.

Keywords: Power Quality, Wind Power, Voltage Unbalance, DFIG

INTRODUCTION
Usually the most productive sites for the development of wind turbines and wind farms are in remote rural areas where distribution networks can be weak and voltage unbalance can be a common feature. This is certainly the case in Ireland where the majority of the wind energy developments have been on the north and west coast of the island [1]. This is also the region in which the transmission and distribution network is weakest.

Problems of power quality can arise with regard to the connection of embedded generation, including wind generation. On weak networks, the connection of wind generation can give rise to voltage fluctuations, including flicker and voltage control [2]. At the same time, power quality problems inherent to the network can cause difficulties with regard to the connection of wind generation. In the event of voltage depressions in the vicinity of system faults, wind generators can experience difficulties in remaining connected; the voltage ride-through problem [2]. Voltage unbalance can also give rise to excessive unbalanced stator currents in wind generators, causing generators to trip out. The authors have monitored the voltage unbalance at a small wind farm in County Cavan in the Republic of Ireland over an extended period and have gained an insight into the extent and variability of voltage unbalance experienced by wind generation.

This paper looks specifically at the behaviour of a double-fed induction generator (DFIG) in response to a voltage unbalance introduced into the network to which it is connected. Matlab/Simulink is used to model and simulate a DFIG and the behaviour of the induction generator and the grid/rotor converters is investigated.

SIMULATION STUDY
Induction generators subjected to network voltage unbalance can overheat due to the excessive currents, and mechanical stress can occur due to torque pulsations. The rotor converter in a DFIG is also susceptible to high currents during periods of voltage unbalance.

The DFIG wind turbine in this study is modelled in Matlab/Simulink [3] to analyse the behaviour of both the induction generator and rotor converter to grid network voltage unbalance. The rotor converter in particular is analysed during network voltage unbalance conditions. The system under investigation is shown in Fig. 1. The network to which the DFIG is connected is represented by a constant voltage and a distribution line with a length of 30 km. The line series resistance is 0.115 Ω/km and the reactance is 0.33 Ω/km.

The distribution line is operated at a voltage of 25kV. The fault level at Bus A in Figure 1 is 10 MVA. The DFIG is connected via a 25kV/690V three-phase transformer. The generator rotor is connected to the grid side via a rotor converter, a dc bus [1.2 kV] and a grid side converter. The DFIG has a total rating of 1.5MVA, and for a speed variation of 30% the rotor converter has a rating 30% of the induction generator.

As shown in Fig. 1, a single-phase load of 6 MVA is supplied at bus B. This single-phase load introduces a voltage unbalance of 9% at Bus B. The voltage unbalance is expressed as the ratio of the negative sequence voltage to the positive sequence voltage [4].

SIMULATION OF VOLTAGE UNBALANCE
Initially the effect of the voltage unbalance on the stator of the generator is considered. Under network voltage unbalance conditions a negative phase sequence component occurs. Fig. 2 shows the instantaneous voltage and generated current at Bus C (Fig. 1) predicted by the Matlab/Simulink simulation. The single-phase load is switched-in at 0.35 seconds and introduces a voltage unbalance of 9%.
unbalance. Clearly, the current is significantly unbalanced after this time.

Figure 2 Stator Current

Although the voltage unbalance factor is approximately 9%, the accompanying negative sequence current unbalance factor is about 30%, as shown in Fig 3. As described in [4], this is because the negative sequence impedance of an induction generator is considerably lower than the positive sequence impedance at normal operating slip speeds.

Figure 3 Stator Voltage and Current Unbalance

Investigations into voltage unbalance and sag conditions in a variable speed drive incorporating a PWM converter was evaluated by [8]. Some of the conclusions reached are that current unbalance can be up to 100% for an input voltage unbalance of only 5%. Fig. 4 is a plot of the voltage and current unbalance at the DFIG grid-side converter. For voltage unbalance of 9% the current is approximately 22% unbalanced.

POWER AND TORQUE PULSATIONS

The persistence of an unbalanced voltage condition presents serious problems to induction generators. Under network voltage unbalance conditions a negative phase sequence occurs, which can result in power and torque oscillations.

Figure 4 Grid-Side Converter Voltage and Current Unbalance

Fig. 5 shows the results of the Matlab/Simulink simulation on the 1.5 MW DFIG with voltage unbalance occurring after 0.35 seconds. Power pulsations can clearly be observed at the stator connection of the DFIG due to network voltage unbalance of 9%.

Figure 5 Power Pulsations on DFIG Due to Network Voltage Unbalance

When using symmetrical components, a separate equivalent circuit can be obtained for positive and negative sequence components [4].

The positive and negative sequence torques are:

\[ T_1 = \frac{P_1}{\omega_m} = \frac{P_2}{\omega_s(1-s)} = \frac{3 I_{1r}^2 R_f}{s \omega_s} \]  

(1)

\[ T_2 = \frac{P_2}{\omega_m} = \frac{P_2}{\omega_s(1-s)} = \frac{3 I_{2r}^2 R_f}{(2-s)\omega_s} \]  

(2)

The developed torque is:

\[ T = T_1 + T_2 = \frac{3 R_f}{\omega_s} \left( \frac{I_{1r}^2}{s} + \frac{I_{2r}^2}{(2-s)} \right) \]  

(3)

The positive and negative sequence currents are functions of their sequence voltages, machine parameters and the
slip s. An oscillating torque is introduced at twice the supply frequency as a result of the negative sequence currents. The power can also be expressed in terms of positive and negative sequence components as:

\[ P_{in} = \text{Real}[3^s(V_1 I_1^* + V_2 I_2^*)] \]  (4)

Fig. 8 gives a good indication of torque pulsations introduced as a result of network voltage unbalance.

**Figure 8 Torque Pulsations on DFIG Due to Network Voltage Unbalance**

**EFFECTS OF VOLTAGE UNBALANCE ON A DFIG CONVERTER**

This section of the study deals with the effects that network voltage unbalance has on the rotor converter. Voltage unbalance can cause voltage harmonics on the dc bus of a DFIG, and lead to current harmonics. Positive and negative sequence components can be used to analyse the effects of voltage unbalance on converters. The cross product of positive and negative sequence components of voltage and current generate a \((2-\omega)\) frequency power ripple (where \(\omega\) is the rotational speed) causing dc link voltage and current ripple [5,7].

Increased current harmonics on the dc link can shorten the life of the capacitor, or lead to capacitor failure. The bus ripple voltage can also lead to the generation of pulsating torques at the second line harmonic, similar to the effects on the induction generator shown in the previous section.

The Matlab/Simulink used in this paper is controlled in the d-q reference frame, with the d-axis aligned with the stator voltage vector [8]. Under the influence of voltage unbalance the stator \(I_d\) and \(I_q\) components will oscillate at twice the network frequency [7] shown in Fig 10.

**Figure 10**

By using a band-pass filter to isolate \(\tilde{I}_d\) and \(\tilde{I}_q\) (where \(\tilde{I}_d\) and \(\tilde{I}_q\) are the double frequency terms produced by the network voltage unbalance), the current unbalance factor can be obtained,

\[ CUF = \sqrt{\tilde{I}_d^2 + \tilde{I}_q^2} \]  (5)

**Figure 11**

A comparison of VUF’s obtained using stator symmetrical components and equation (5) is shown in Fig.11. It can be observed that that both methods produce a voltage unbalance in the region of 9%.

**ALLEVIATION OF THE EFFECTS OF NETWORK VOLTAGE UNBALANCE**

The issues associated with the connection of wind turbines and DFIG’s to network grids with voltage unbalance, have been investigated [6,7]. In a DFIG the grid-side converter, dc link capacitor and transformer may function as a STATCOM. [6] uses this approach to design a control system to alleviate the problems on the DFIG as a result of unbalance voltage in the supply grid. [7] presents a novel controller design for a DFIG that provides adjustable speed and reactive power control and also reducing torque pulsations due to supply voltage unbalance. This design is based on using the stator and rotor \(I_d\) and \(I_q\) current...
components to compensate for the torque pulsations. The
torque equation of a DFIG is given by [7]

\[ T_{em} = \frac{p}{2} L_m (i_{sq} \cdot i_{rd} - i_{sd} \cdot i_{rq}) \]  

(6)

Where \( L_m \) is the magnetising inductance, \( i_{sd} \) is the stator
direct component, \( i_{sq} \) is the stator quadrature component,
\( i_{rd} \) the rotor direct component and \( i_{rq} \) is the rotor
quadrature component. From the appropriate induction
machine q and d equivalent circuits the magnetising
current is defined as

\[ i_{msd} = i_{sd} + i_{rd} \]  

(7)

\[ i_{msq} = i_{sq} + i_{rq} \]  

(8)

The torque equation can now be expressed as

\[ T_{em} = \frac{p}{2} L_m (i_{msq} \cdot i_{rd} - i_{msd} \cdot i_{rq}) \]  

(9)

When the dq frame is synchronously rotating, the stator
voltages are balanced, and the generator is in steady-state,
all dq quantities are dc. The torque equation is then

\[ T_{em} = \frac{p}{2} L_m (I_{msq} \cdot I_{rd} - I_{msd} \cdot I_{rq}) \]  

(10)

With \( I_{msq} \), \( I_{rd} \) and \( I_{msd} \), \( I_{rq} \) constant the torque will also be
constant. However when voltage unbalance occurs in the
supply network, this will cause perturbations in \( I_{msd} \) and
\( I_{msq} \) at twice the synchronous frequency. The torque
equation for unbalanced network voltage is [7],

\[ T_{em} = \frac{p}{2} L_m [ (I_{msq} + \tilde{I}_{msq}) (I_{rd} + I_{rdcomp}) - (I_{msd} + \tilde{I}_{msd}) (I_{rq} + I_{rqcomp})] \]  

(11)

\( I_{rdcomp} \) and \( I_{rqcomp} \) are compensating currents which can be
added to the rotor converter control currents to cancel the
effects of the oscillating \( I_{msd} \) and \( I_{msq} \). The compensating
currents can be determined by equating the terms of the
balanced equation (10) with the unbalanced equation (11).

\[ I_{msq} I_{rd} = (I_{msq} + \tilde{I}_{msq}) (I_{rd} + I_{rdcomp}) \]  

(12)

\[ I_{msd} I_{rq} = (I_{msd} + \tilde{I}_{msd}) (I_{rq} + I_{rqcomp}) \]  

(13)

\[ I_{rdcomp} = -\tilde{I}_{msd} I_{rd} / (I_{msq} + \tilde{I}_{msq}) \]  

(14)

\[ I_{rqcomp} = -\tilde{I}_{msq} I_{rq} / (I_{msd} + \tilde{I}_{msd}) \]  

(15)

To alleviate the effects of voltage unbalance on DFIG’s
the current controllers for active power P and reactive
power Q require compensation terms. The current
compensation terms were incorporated in the DFIG
Matlab/Simulink model in the rotor-side current control
loop Fig. 12.

A single-phase load is introduced as shown in Fig. 1, and
the model simulated in Matlab/Simulink for a simulated
time of 0.5 seconds. The simulation takes about 0.3
seconds to reach steady state. The single-phase load is
therefore switched-in at 0.35 seconds and the A phase
drops in magnitude from 1.0 pu to 0.88 pu Fig. 13.

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**Figure 12 Current Control**

**Figure 13 RMS Stator Voltage & Current**

This represents a drop in the A phase voltage from a
nominal value of 332 V to 288 V and results in the
network voltage applied to the DFIG becoming
unbalanced. A timer (set at 0.4 seconds) is used in the
simulation model to delay the switching-in of the control
compensation terms, Fig. 12.

Fig. 14 shows the amplitude of the dc link bus voltage at a
steady value of 1200 V at 0.34 seconds. When the
unbalance load is switched in at 0.35 seconds it introduces
a negative sequence voltage of 9% which creates double
frequency oscillations on the dc link bus. Control loop
compensation is introduced at 0.4 seconds and the dc link
voltage oscillations decrease. The reduction in the rotor power oscillations at the grid-side converter can be seen in Fig. 15.

![Figure 14 DC Link Voltage](image1)

**Figure 14 DC Link Voltage**

The compensation terms become active at 0.4 seconds and there is a reduction in dc link voltage oscillations and rotor power oscillations, however Fig. 13 shows that there is an increase in stator current.

![Figure 15 Rotor Power Grid-side Converter](image2)

**Figure 15 Rotor Power Grid-side Converter**

The voltage profile on the rotor (grid-side converter) is similar to the stator, Fig. 16 with the A phase dropping to 0.88 pu.

![Figure 16 RMS Rotor Voltage & Current Grid-side Converter](image3)

**Figure 16 RMS Rotor Voltage & Current Grid-side Converter**

CONCLUSION

The effects of voltage unbalance on a DFIG were investigated. Simulations showed that voltage unbalance when applied to a DFIG results in large current oscillation in both the induction generator and converter. A model of a DFIG in Matlab/Simulink was adapted and modified to incorporate a compensating control structure to alleviate the detrimental effects that network voltage unbalance has on DFIG’s. The simulation results showed the improvement in the behaviour of the DFIG to network voltage unbalance when compensation was introduced.

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