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An analysis of harmonic heating in smart buildings and distribution network implications with increasing non-linear (domestic) load and embedded generation

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Abstract: Harmonic distortion is generally not taken into account within domestic installations and the associated wiring systems, as its potential is considered sufficiently small to be neglected. Standards to limit harmonic manifestations in the low voltage (LV) network are available, but these can be breached as a consequence of advancements in power electronics in some modern household devices contributing higher levels of harmonic distortion than permitted. While these devices *individually* might not be considered serious in terms of system level harmonic distortion manifestations, electrical equipment failures and insulation failures - increasingly being derived from harmonic cable heating - suggest a different story. A 10% increase in THD in a circuit will result in an increase of 10% in cable heat. Recently, attempts have been made to offer harmonic derating factors for building electrical circuit design in BS7671, but this approach currently prioritizes large power devices. This article explores the need for harmonic considerations during the design stage of electrical services engineering projects. Best practice suggestions, in the context of the dissemination of heat caused by harmonics related to household load deployments/configurations, are also provided based on the analysis conducted with real household data. This is further extended to a practical distribution network where the effect of harmonic heating at the network level is explored. The results suggest that the harmonics in the distribution network can amass to cause a cumulative effect on the network. Furthermore, it can be observed from the results that in a distribution network containing (domestic) solar photo voltaic (PV) systems, the harmonic heating issue can be reduced. This benefit is not without consequence however, as increasing PV penetration does not reduce the harmonic content of the overall system and therefore presents a further concern that may need to be addressed in due time.

Keywords:

Harmonic Distortion (THD), Distribution network analysis; Photovoltaic systems; Non-linear load; Harmonic load flow; Cable heating;

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Nomenclature

THD – Total harmonic distortion

$THD_{i/v}$ – Total harmonic distortion of current or voltage

I, i – RMS current

I_1 – Fundamental current

I_n – Harmonic current (n=2,3,4,...)

R_{AC}, r_{AC} – AC resistance

R_{DC}, r_{DC} – DC resistance

σ – Conductivity

P_L – Power loss

P_{L_normal} – Normal power loss (loss with out considering harmonics)

Introduction

The distribution network maintenance of standard operating voltage and current profiles is addressed as a power quality (PQ) problem that is complicated by the variation of load type connections and the associated demand intermittencies. The PQ problem is further exasperated with the introduction of smart devices or smart loads in the distribution network most of which being non-linear in nature. In this regard, the presence of harmonics in the electrical network may be the cause of increased losses within transformers, overloading in neutral conductors, disturbances in the torque of motors, etc. [1]. A detailed review on harmonics in the distribution network, modelling of harmonic load and harmonic mitigation in the context of increased penetration is discussed in [2]. “Smart distribution-grids” or distribution networks with smart devices claim the potential to improve the performance of the electric power system, as well as offering the same performance as existing technologies, but in a more cost-effective way. However, these smart devices also require a proper harmonics mitigation technology, otherwise these also have some adverse consequences on PQ [3]. To add further to the problem, the inclusion of distributed energy resources, which employ power electronic converters/inverters, are also affecting power quality in the system [4]. The interaction between distributed generators and electrical vehicles with the grid is discussed by Gil-de-Castro, Rönnberg and Bollen [5]. Their work suggests that the harmonics from individual domestic devices can flow to the grid and can cause an impact on other grid-connected devices. However, that study was limited to the harmonic interactions between grid connected devices and domestic devices and did not consider the interaction between individual appliances in the (domestic) household environment. The interactions between grid connected devices at harmonic frequencies can also introduce a harmonic resonance mode in the system [1]. Inverters associated with distributed generation (DG), are becoming one of the major sources of non-linearity in a building environment. Furthermore, inaccurate filter design could also lead to voltage distortion which can severely affect the consumer

appliances. A harmonic resistance damping method was developed by Munir, Li and Tian to dampen the DG inverter harmonics in this regard [6]. The harmonic environment across the distribution network will severely affect the synchronization algorithm in the grid connected inverters as discussed in [7], where the authors propose an improved algorithm for synchronising under such conditions. The harmonic impact of a residential PV system using recorded data is presented in [8] where the non-linear loads are also considered in the analysis. The harmonic voltage profile is considered here as the manifestation of the harmonic distortion occurring in the network. The results indicate a considerable distortion of voltage at the point of common coupling (PCC) under various PV penetration scenarios. However, the effect of current distortion was not afforded a similar focus in the analysis. The combined effects of solar PVs and plugged in electric vehicles (PEVs) on the feeder and transformer loads and how they affect the network voltage profiles and derive harmonic distortions in an urban area distribution system, are investigated in [9]. The authors present changes in the characteristic daily load and voltage profiles as well as changes in the total harmonic distortion of the system voltage (THD_v) caused by the simultaneous operation of PVs and PEVs. Furthermore, the results suggest that an optimised engagement ratio (PV/PEV) can impact load reduction and produce a reduction in voltage variations, while potentially resulting in an increase THD_v. This is also evident in the analyses presented later in this paper.

Harmonic heating effects are examined by Palmer *et al.* [10] where pipe type cable modelling is employed through finite element analysis that utilizes the Nehar McGrath harmonic heating model. Cable heating effects in the presence of harmonic distortion are analysed and experimentally verified by Blackledge *et al.* [11]. The authors briefly explain a cable heat transfer method and also discuss the harmonic rating factor introduced in BS 7671 [12]; the national standard in the United Kingdom for electrical installations. The paper also contains a comprehensive discussion about the harmonic heating effect caused by harmonics in a building. In [13], the authors considered the losses in audio visual devices. The paper utilized time of use survey data concerning the audio-visual device to quantify the amount of power that can be saved. It was observed that *THD* reduction (by a factor of 10) could reduce the energy loss significantly and inculcate a saving of seven million of euros. Basically, the ampacity of power cables is limited or determined by the maximum operating temperature within which the insulation can maintain its optimal performance. For example, the cables constructed with a cross-linked polyethylene (XLPE) dielectric are typically restricted to a maximum temperature of 90°C [14]. An increase in temperature will lead to faster deterioration of the conductor and significantly lowers the operating life. Harmonics cause increased heating of the conductor while the current carried may be less than the rated current.

Currently, (ET 101:2008, the Irish electrical installation standard) for installations <1kV) [15] recommends a neutral overcurrent relay connection to protect against excessive harmonics in a 3 phase system. Such a relay facilitates automatic disconnection when excess current contributed by harmonics is detected in the neutral. However, this method only accounts for triple-*n* harmonics and does not sufficiently address the other orders of harmonics that can arise in such environments. But again, THD cannot solely be considered as the measure of harmonic content in the system. Instead, for power efficient operation, device manufactures obligations to follow strict regulations to limit actual harmonic content of their equipment should be prioritised.

The contribution to the wider discussion presented in this paper lies in an efficient extrapolation of harmonic heating analysis from the building environment to the distribution network environment where the heating effect of harmonic current is currently overlooked. The analysis

will suggest to distribution network operators (DNOs) that caution is required if sustained increases in non-linear load penetration are to be facilitated without means of active mitigation as they may adversely limit the maximum operating capability of the network. This issue could be further exasperated with the influence of embedded generation such as domestically connected solar PV and this paper will present analysis in this regard.

The work also intends to offer a guide for consumer awareness and safe/best operating practices to safeguard their home and equipment against the destructive impact of harmonics. The authors contend that there is insufficient literature available in published materials pointing to the harmonic heating characteristics in electrical networks and almost none in distribution network. In this regard, the studies presented here will assist as a reference for researchers and operation and planning engineers.

In summary, the objective of this paper is

- To conduct harmonic heating analysis in a building energy circuit.
- To extrapolate the harmonic heating analysis to a network model from the Building energy system analysis methodology
- To provide DNOs a simple and straight forward analysis and interpretation methodology to perform harmonic analysis
- To provide DNOs an insight to the magnitude of harmonics and its possible adverse effect in a distribution network.
- To visualise the change in harmonic propagation with solar PV integration.
- To provide recommendations to consumers to reduce the impact of nonlinear loads to the building energy system based on the analysis and result.

The paper is sectioned in to 4 parts, where section 2 discusses the load modelling and network modelling. The subsequent section discuss harmonic power flow and methodology of the paper. The results and conclusion follows later in section 4.

Load and Network Modelling

A typical residential environment contains a variety of electrical equipment, most of which can be classified as non-linear load. The proliferation of non-linear load in the residential sector is due to the application of electronic switching devices commonly known as switch mode power supplies contained within power supplies. The first step in performing harmonic analysis is to obtain the magnitude of current consumed by these non-linear harmonic loads in the domestic household.

Various literatures discuss the PQ issues of the energy efficient harmonic loads but the performance during the operating conditions of said load is often neglected. Furthermore, the PQ studies for the most common and often highest power consuming appliances such as washing machines and vacuum cleaners are not widely conducted. During the power quality analysis of the energy efficient appliances of a building, it is often found that some of the harmonic loads change their active and reactive power consumption or harmonic current injection characteristics depending on their operating mode from the pre-specified values. Non-linear devices such as smart multi-media devices, desktop PCs, laptops, etc. are representative of the most typical single phase converter based loads, with similar current and voltage characteristics.

Modelling of these nonlinear loads is achievable in any simulation platform such as MATLAB™. For instance, non-linear load design based on single phase diode-bridge converter using a Norton equivalent circuit are considered in [13]. These models are developed for single phase loads, and performance has been tested with single load representations only. Mazin *et al.* [16] describe the harmonic contribution of residential loads by studying the characteristics of load side and source side harmonic impedances. It is also common knowledge that in residential buildings individual loads always consume reactive current and consume harmonic currents at the same phase angle with respect to its supply voltage in the same operating condition. Therefore Salles *et al.* [17], in this regard, suggest that typical spectra can be used to model a harmonic-producing load. In this paper, the linear and non-linear harmonic load models have been developed by controlled current sources in Simulink power system (SPS), based on available harmonic information (% of THD, harmonic current spectrum and phase angle) domestic load data. A Simulink-developed load model was subsequently verified with experimentally collected data based on measurements from more than 200 harmonic producing appliances in a residential building where the variation of voltage THD is found to be in range of 1.2 to 1.7% [18]. In most readings considered, the magnitude of the harmonic current order above 21st order is found to be less than 5% of the fundamental. The measurements were performed using an instrument power quality analyser C.A.8230 Ampflex, from Chauvin Arnoux [19]. General household equipments/devices are considered. In Ireland, the use of electricity in the home accounts for approximately one third of the total electricity produced [20]. Table 1 illustrates a sample of (measured) power ratings associated with common appliances found in Irish homes [21]. A Simulink model of the appliances is utilized to develop harmonic profiles that are employed in the network analyses.

Table 1: Power consumption capacity of the electrical appliances of a building in Dublin

Table 1: Harmonic Devices different combinations and their resultant THD percentage

Electrical Appliances		Active Power (P)	Reactive Power (Q)	Harmonic Power (H)	Apparent Power (S)
		(W)	(VAR)	(VAR)	(VA)
Non Linear Harmonic Load					
Static	Compact Fluorescent Lamp (CFL)	14	5.5	19	25
	Microwave oven	1250	220	300	1304
	Refrigerator	110	120	15	163
	Smart TV (26")	55	16	78	97
Dynamic	Washing Machine	600 - 1930	410	200	1983
	Vacuum Cleaner	335 - 1100	100 – 500	170 - 510	730 -1120
	Laptop	85	38	190	212
Linear Load					
Static	Heater (bedroom)	2000	0	0	0
	Electric Cooker (Oven)	1200	0	0	0

The network, illustrated in Figure 1, is modelled using OpenDSS (Open Source Distribution System Simulator) software, which has harmonic analysis capability. This urban distribution network is representative of an actual suburban low voltage distribution network in Dublin city, Ireland and contains a supply transformer and a radial distribution system. The network contains nine 3 phase radial distribution lines delivering power to 74 household loads through the associated distribution lines. The rating of the loads vary depending on the dwelling size, demographic and number of occupants. The network lines are modelled as overhead lines and the sub-feeders cables are 120 mm² and 70mm², with copper and/or aluminium conductors and cross-linked polyethylene (XLPE) and/or polyvinyl chloride (PVC) insulation material. The consumer distribution conductors are 25mm² concentric neutral cable. The network configuration model is consistent with that presented in [22]. The OpenDSS network model incorporates the harmonic profile for the individual loads as defined using the recorded data and simulation. The loads are modelled as the lumped constant PQ load i.e. constant active and reactive power consumption and represented by current injection model to incorporate harmonics [13]. Random distribution of solar PV is considered across the network with the individual PV power ratings of 5.25kW. That is the maximum power that can be delivered by a single solar PV system is 5.25Kw. The domestic loads and PV generators utilised in the network harmonic analyses are based on the allocations employed in [23]. The network model utilized is modelled in OpenDSS using [22] and the *hosting capacity* of the network and the PV connection position/location is based on [23]. The network model is a section of urban distribution feeder from Dublin. It has 9 section connecting 10 nodes (mini pillars) of distribution 3 phase feeders starting from the distribution transformer (10/0.4kV) and denoted in red and blue colour as AB,BC, CD and so on. It consist of 74 households (numbered 1 to 74) supplied by these 10 mini-pillar connections. Each household is connected by single phase supply provided by the closest mini pillar. Further detailed modelling aspect of the network is discussed

in reference [22]. The same network and parameters are utilized by authors in [23] and has performed hosting capacity analysis with solar PV system in the network. The connected node and rating of solar PV, and maximum hosting capacity is adopted from this paper. The *hosting capacity* is defined as the ratio of total amount of PV power generated in the network to the KVA rating of transformer connected to the feeder. In this analysis it is 36.9%. The structure of network and the location of PV modules are given in Figure 1.

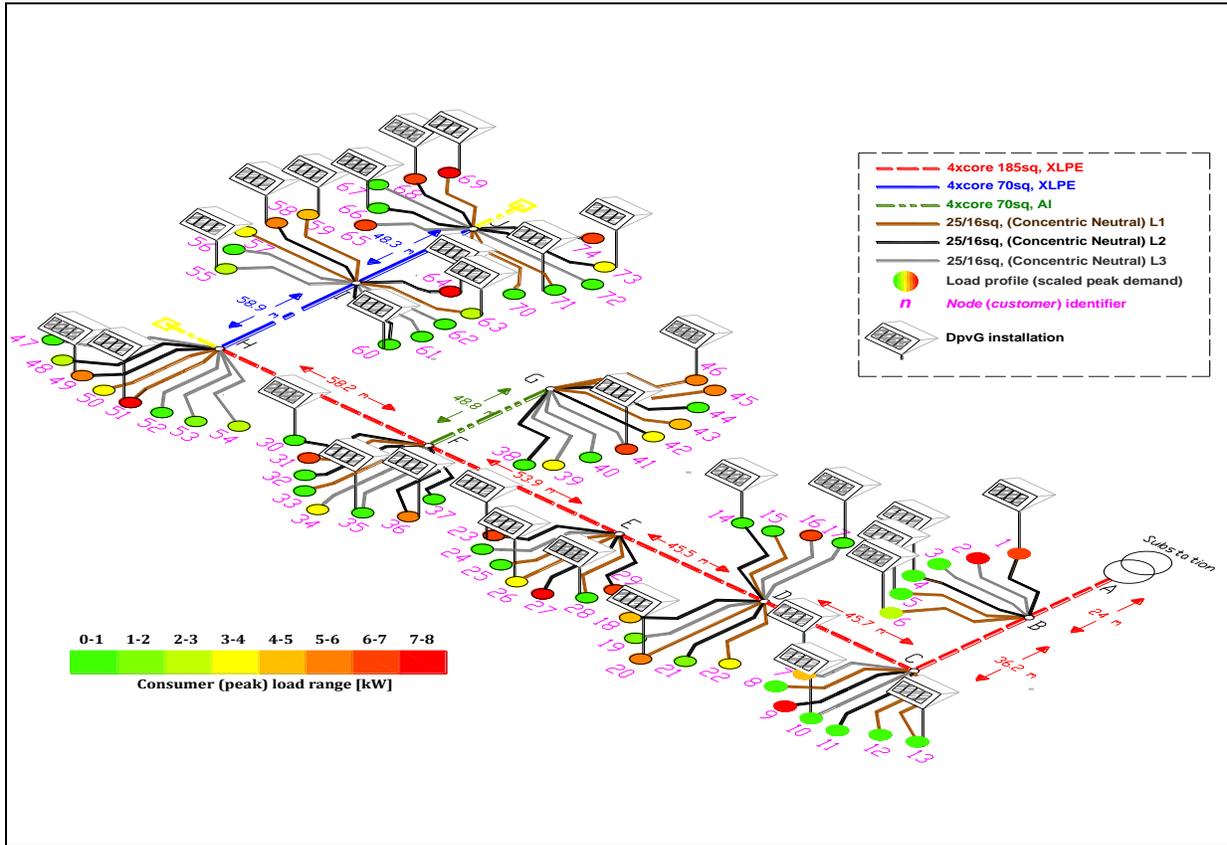


Figure 1 Urban Distribution Network model [22] incorporating the domestic load/PV profiles in [23].

Harmonic Power flow Analysis

The OpenDSS simulation software was utilized to perform power flow and harmonic power flow on the network model developed in the previous section. The software is especially applicable for distribution network analysis (with high R/X ratios) and has a well modelled simulation engine for the harmonic power flow [24]. The harmonic power flow is performed for the specified number of harmonic orders which in this case was up to 29. The harmonic order is referring to the integer multiple of fundamental frequency, that is, 2,3,4,5...n (*n is the harmonic order*). Usually even order harmonics are ignored as the electrical quantities exhibits half wave symmetry. The higher order harmonics are also ignored as their magnitude are negligible and their associated effects are significantly low when compared to the lower order harmonics. The results of harmonic power flow will depend on the harmonic phase angle as harmonic cancellation is incurred [25]. However,

for the presented analysis the extreme operation limit is considered and the harmonic phase angles are ignored so that the power flow depends only on the individual harmonic components.

The PV system considered in the analysis is obtained from Electric Power Research Institute (EPRI) technical update [26] which deals with the stochastic analysis for finding PV hosting capacity in the distribution network. The harmonic distortion in the PV module is abiding to the IEEE 519 standards and the power factor at the front end of the inverter is set to 0.95. The data from [26] is used to specify the harmonic spectrum of PV module modelled in the OpenDSS. Linear scaling is also applied here to match the power rating of the module employed.

Network Load and Harmonic Scaling

The individual load model of the network is created from the average load consumption data obtained. The harmonic profile was however extrapolated and scaled from the household harmonic model simulated in the first part of this work. The scaling factor was linear, which was a reasonable assumption as individual house THD was assumed to be same to have a consistent and comparable result. This is also due to the additive nature of harmonic current[27]. The mathematical justification of linear scaling is presented below.

Let $I_1, I_2, I_3 \dots I_n$ be the harmonic current spectrum for a load of 'X' kW. The current THD is given by equation,

$$THD = \frac{\sum_{i=2}^n \sqrt{I_i^2}}{I_1} \quad (1)$$

Here, I_n is the individual harmonic current and I_1 is the fundamental current.

When the load is reduced to half and the current spectrum is scaled by half we get, the load as 'X/2' kW and current spectrum as $I_1/2, I_2/2, I_3/2 \dots I_n/2$. Now the THD for this current spectrum, is given by

$$\begin{aligned} THD &= \frac{\sum_{i=2}^n \sqrt{\left(\frac{I_i}{2}\right)^2}}{\frac{I_1}{2}} \\ &= \frac{\sum_{i=2}^n \sqrt{I_i^2}}{I_1} \end{aligned} \quad (2)$$

Which is same as initial THD value given in equation (1). Thus, a linear scaling factor for harmonic spectrum is a justifiable method to keep a constant THD value for all load.

The harmonic power flow analysis procedure, incorporating the network model illustrated in Figure 1 and the means of harmonic load profile inclusion, is summarised in Figure 2. The flow chart explains the steps involved in the harmonic analysis presented in this paper. The Simulink based harmonic analysis is conducted initially and used for OpenDSS based analysis.

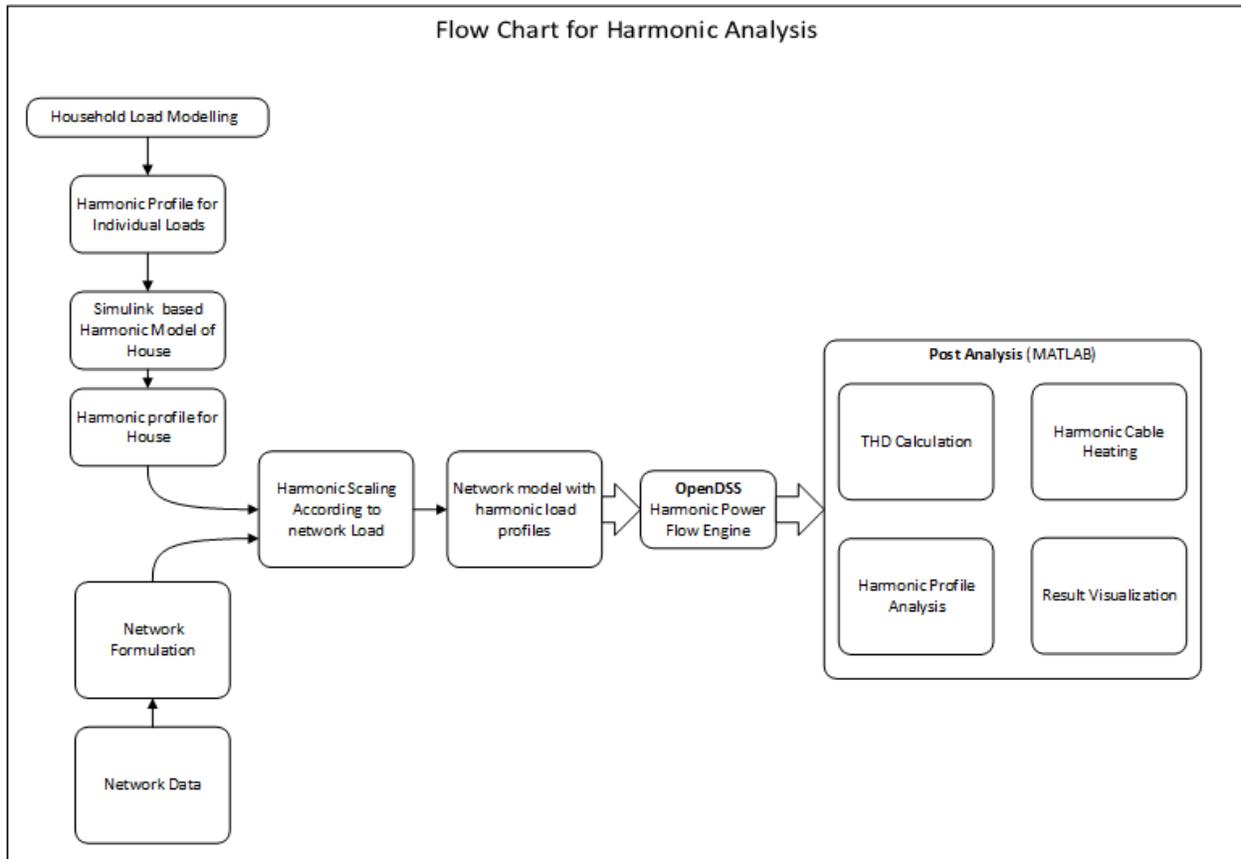


Figure 2 Flow chart of Harmonic Analysis Conducted

Harmonics and Loss(es) due to harmonic manifested heat in Household system

The analysis is conducted in two parts. In the first part, the focus is on the household network and analysis of the thermal heating effect of harmonics. In the second part, the focus is on the propagation of harmonics and harmonic heating on the network cables in a distribution network which encompasses houses similar to the one in the first section. An additional objective of this consideration is to introduce the effect of distributed (domestic) PV generation.

In order to analyse the effect of harmonics in a building energy systems (BES), simple methods are utilised to represent the harmonic heating. The BES implies to all the circuit in the building environment, which is a household environment referring to this paper. In any conductor when sinusoidal currents are introduced the geometry associated with the conductors introduces a complex electromagnetics problem. The sinusoidal varying magnetic flux induces a time varying magnetic flux density which induces eddy currents and as a consequence of the skin effect, higher losses relatively, in comparison to a DC context, are created. The ratio of AC to DC resistance is the parameter that varies for each harmonic frequency. The inductive element of the cable is not considered here as the associated value is sufficiently small and it does not cause an active power loss contribution to heat. However, the same is not true if the voltage waveform is considered, but this does not feature in this study. The ratio of AC to DC resistance is described generally in (3),

$$\frac{R_{AC}}{R_{DC}} = \frac{\int \frac{(i(x,y))^2}{\sigma} ds}{i^2 r_{DC}} \quad (3)$$

The integral is in respect to the cross-sectional area of all conductors in the system (cognisant of conductivity, σ). The $i(x,y)$ is the RMS current density which is a function of position ((x,y) is position). This inclusion of $i(x,y)$ helps to account for the conductor geometry to the current propagation. Only usage of symbol 'i' represents the RMS current flowing through the conductor irrespective of the position. The effective resistance ratio is weighted sum of resistance ratios calculated at each frequency and provided by [10]

$$\left(\frac{r_{AC}}{r_{DC}}\right)_{eff} = \sum_{n=1}^{\infty} \gamma_n^2 \left(\frac{r_{AC}}{r_{DC}}\right)_n \quad (4)$$

where γ_n is the ratio of n^{th} harmonic to the magnitude of total harmonic current. Considering only non-sinusoidal load current, and in consideration of a Fourier transform application, multiples of fundamental frequency, which themselves are sinusoidal, can be determined. The total heating caused by each component and in the context of a low voltage distribution network, the ratio of AC/DC resistance approximately equals 1.02 [28], the total power loss can be obtained as follows:

$$P_L = I^2 r_{AC}$$

$$P_L = 1.02 \cdot r_{DC} \cdot i^2 (1 + THD_i^2) \quad (5)$$

where I is the total current consumed by the harmonic load, including the THD_i (i.e. the current THD) factor in the equation to quantify the harmonics as

$$THD_i = \frac{\sqrt{\sum_{n=2}^{\infty} I_n^2}}{I_1} \quad (6)$$

where, I_1 is the fundamental current, I_n is the harmonic current component for each harmonic order and n is the order of harmonics. Power loss without harmonics or AC resistance considered is:

$$P_{L_normal} = I^2 r_{DC} \quad (7)$$

In the household network the wiring on the main circuit is considered for the thermal analysis. However, the methodology can also be applied to the sub circuit and to the cable of an extension cord through which multiple consumer devices may be simultaneously connected. Equation (3) calculates the loss without considering the harmonics and loss taking harmonics into account. Thus, this paper will offer a comparison of the mismatch between the normal power loss and the loss incurred through THD (considering harmonics) to understand the amount of harmonic rating factor that may be required for the sub-circuit cable rating. The authors acknowledge that harmonic power factor, displacement power factor, etc. play an important role in the heating manifestations of harmonics. These characteristics however, are not considered in this study as their respective contributions are almost insignificant in terms of the building environment. To understand the relationship between the THD and heating effect a THD vs P_{loss} curve is plotted in Figure 3 which illustrates how power loss increases with an increase in THD . This is apparent when equation (2) is employed to calculate the power loss in terms of THD . As the harmonic pollution increases in an electrical network, the heating in the cable increases and may eventually be higher than the

rated value for a particular conductor. This situation may not be recognised by standard protection equipment as it relies on the root mean square (RMS) value of current. However, modern protection circuits with thermal overhear protection may detect if the increase in temperature is in the same circuit as of the protection unit. To understand the adversity of the situation, the initial point depicted in Figure 3 at *THD* of 1% represents a loss of only 3.83×10^{-5} pu, whereas at 100 % *THD* it reaches close to 0.4 pu and it reaches 1pu when *THD* is 160 %. The temperature rise on the conductor due to the increased heat will depend on various factors such as the installation method, ambient temperature, rate of cooling, etc. The modelling of temperature rise hence would be dependent on various dynamic factors and hence not considered here. Therefore, the relative error of loss (W) as effected (proportionally) by the temperature rise is the preferred consideration in this analysis.

The network based analysis will also use the same equations (5 & 7) to calculate the cable ohmic loss with and without harmonics in the network feeder. It also shows the propagation of harmonics through the network feeders. The network considers solar PV installation and in the domestic building environment to understand the variation in harmonic profile due to it. The methodology is further utilized to understand the harmonic propagation and behaviour under different load and PV penetration scenarios. The network based analysis will provide an insight to the planning and operation engineers on the actual effect of harmonics in distribution network and facilitate them to plan and implement the regulations where ever necessary.

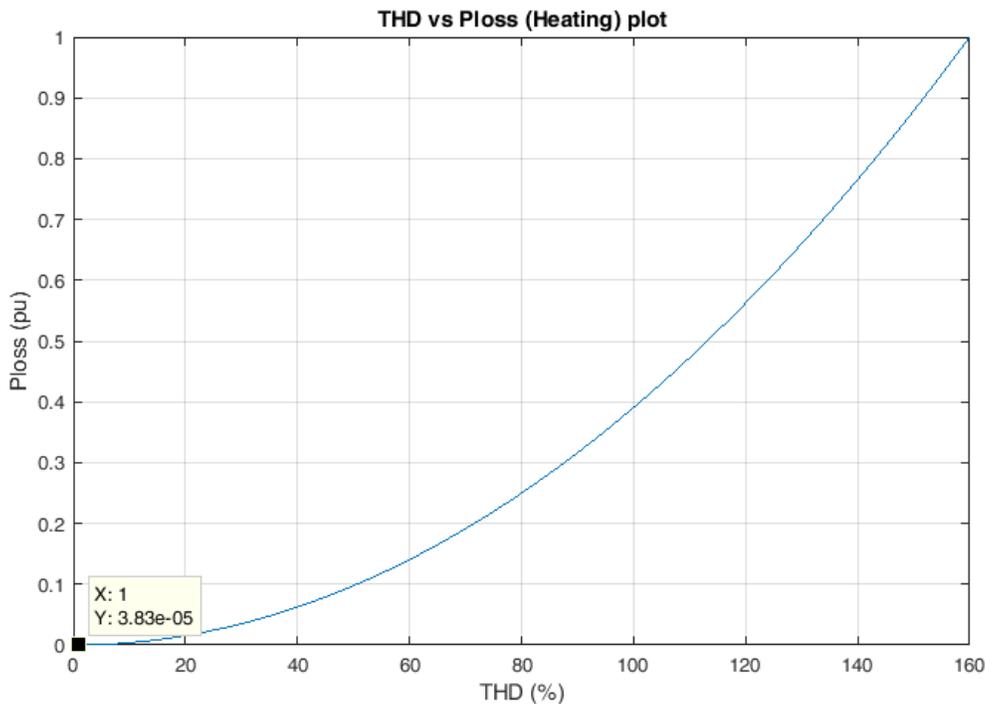


Figure 3 *THD vs P_{loss}* Plot

Results and Discussion

The results of the analysis are presented in two parts. The harmonic heating in a household circuit is initially considered and thereafter extrapolated for a distribution network analysis; as presented in Figure 1.

To analyse the combined effect of the harmonic loads (devices), a household network wiring is considered which is in accordance with the British wiring standards, BS7671 (IEE/BSI. 2008), Power is distributed through radial circuits, with varying current carrying capacities (I_z). In a domestic context, lighting circuits are facilitated through a 1.5 mm² ($I_z = 6A$ capacity) wiring system with general services (socket) circuits are facilitated through a 2.5 mm² wiring system ($I_z = 20A$ capacity). The daily power consumption of lighting/general service load may vary depending on various factors. In this study, the power quality analysis of the appliances during their operation mode is considered and hence does not relay on the manufacture pre-specified values of power quality.

The worst case harmonic scenarios in a domestic environment occur when multiple harmonic loads are connected to a single sub circuit as the harmonics are generally cumulative in nature. Hence to understand this environment, various probable combinations of harmonic loads are combined together to form different case studies. A total of six harmonic loads were considered along with two linear heating loads forming 255 combinations the details of these loads are given in Table 1. Exemplar cases are provided in Table 2 with their corresponding current *THD* calculated. While the harmonics are generally cumulative, in some cases, they tend to cancel out depending upon the harmonic phase angle and hence in the practical consideration the *THD* may reduce with certain combinations. But as discussed before the current study focuses on worst possible scenarios of harmonics, the harmonic phase angles are ignored and harmonic cancellation is not expected. Hence, to understand the worst possible scenario in a domestic environment, five combinations that accumulated the highest losses are considered and presented in Table 2 and Figure 4. In this regard, the exemplar scenarios are analysed for the harmonic power loss and then compared with standard power loss calculated by the RMS value of current. It is evident that the actual power loss occurring in the conductor is much more than the loss during the normal operating condition. To put it in perspective, a 2.5 mm² cable, with maximum rated current carrying capacity, the loss is 3.8 W/unit length but in case 2 the loss is close to 5 W/unit length even when the RMS current is much less than the rated current. This therefore implies, that relatively speaking, a circuit operating at near to its rated current would incur enhanced deterioration in the cable, which could eventually lead to cable failure or in the worst case a fire incident.

Table 2: Harmonic Devices different combinations and their resultant THD percentage

	Light	Microwave Oven	Fridge	Vacuum Cleaner	Washing Machine	Laptop	Current THD (%)
Ratings (in Watt)	40	1350	160	1400	1200	250	
CASE 1	ON	ON	OFF	OFF	ON	ON	44.64
CASE 2	ON	ON	ON	OFF	ON	ON	42.12
CASE 3	ON	ON	ON	OFF	ON	OFF	41.31
CASE 4	OFF	ON	ON	OFF	ON	ON	40.73
CASE 5	OFF	ON	ON	OFF	ON	OFF	39.74

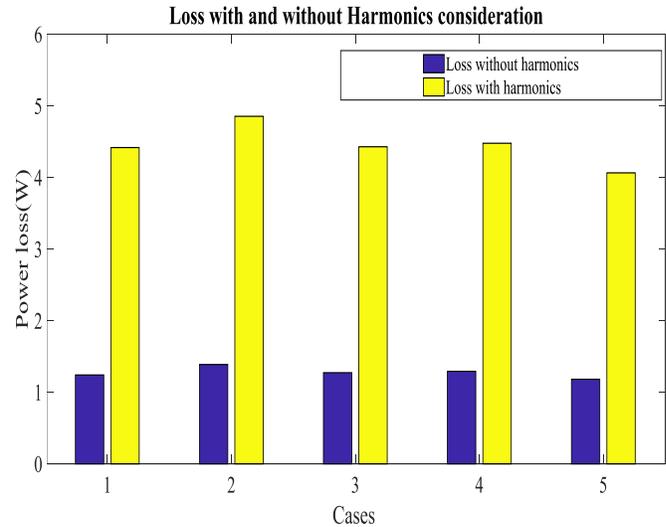


Figure 4 Loss with and without Harmonic consideration

It is normal practice in the domestic environment for consumers to employ extension cords to connect multiple devices and may not have such type of thermal protection locally. Such possibilities in the domestic environment are the primary motivation for this study with consumer awareness and best practice awareness in respect to harmonic loads as the goal.

Figure 5 illustrates that in consideration of the harmonic profile associated with compact fluorescent lamp (CFL) (Case A) and CFL with resistive load (Case B), that the *THD* is not always the optimal measure of harmonic content in the system, or to even understand the harmonic pollution in a system. Since the *THD* is a ratio of fundamental to the vector sum of harmonics, when a purely resistive load like a heater is connected to a circuit containing harmonic load, the *THD* may appear to be lower; even though the harmonic profile does not change. Hence the harmonic pollution will be still observed in the system, which is evident from the harmonic spectra illustrated in Case A and Case B of Figure 5. This scenario could be intolerable for many sensitive consumer equipment and could eventually lead to premature failure of such devices. This is because, sensitive consumer equipment containing electronic circuitry could form a lower impedance in the context of certain harmonic frequencies. Reliability studies such as mean time failure (MTF) studies need to be conducted to completely understand and quantify the direct effect of harmonics in the context of consumer equipment. Such study is not considered in the scope of this paper.

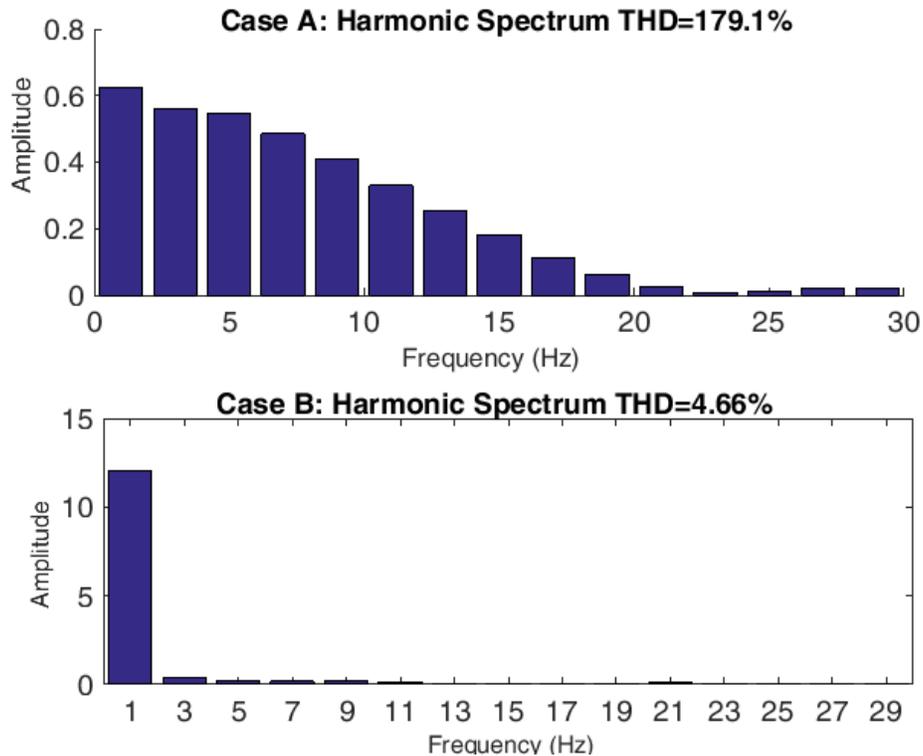


Figure 5 Harmonic spectrum of different cases considered

Solar PV penetration is increasing in a distribution network throughout the world. A grid connected solar PV system has an inverter at its front end that employs power electronic switches. Even though filters are employed at the connection point, the output power still contains harmonics and contributes to the associated non-linearity to the grid. Since the solar PV's are usually connected in conjunction to a building network, a harmonic analysis without considering PV would never do justice to the motive of this work. To understand the effect of non-linearity imposed by a grid connected solar PV, the household network consisting of harmonic load, facilitated by an independent PV source and the voltage THD_v is measured. Generally a stiff source such as the electrical grid, which may still provide a close to the sinusoidal voltage input even with significant harmonic pollution from a building energy system is found in the distribution network and was used to conduct the previous analysis. However, with a source like solar PV generator or a battery storage system, the situation is entirely different. The source voltage may not be exactly sinusoidal with the harmonics present and even with filters installed in the inverter system. This will further lead to distortion in the power quality and adversely impact on equipment operation in a building. With impure power, the performance and expected life time of equipment is further affected. Figure 6 illustrates a voltage waveform without a stiff source where the harmonic pollution causing voltage distortion is clearly visible. The voltage *THD* (THD_v) is approximately 12.74 percent in Figure 6. However, the regulation states of 8% [29] harmonic voltage connected to the electrical system depending on the power rating. Even though, the model was made in accordance with regulations, the increase in THD_v is due to high demand of harmonic current and hence the source voltage gets distorted to provide it. Practically, it is highly unlikely to operate all loads in the household simultaneously and hence the THD_v value would still be close to/less than the regulation(s) specified. That said however, a 2 % increase in the context of a high power

consuming piece of equipment (PV/EV) would itself represent a high value when compared to low power consuming equipment and could lead to consumer equipment damage. Furthermore, in the context of power loss in cables with non-linear loads connected to distorted voltage, the losses incurable due to harmonics will increase in this regard.

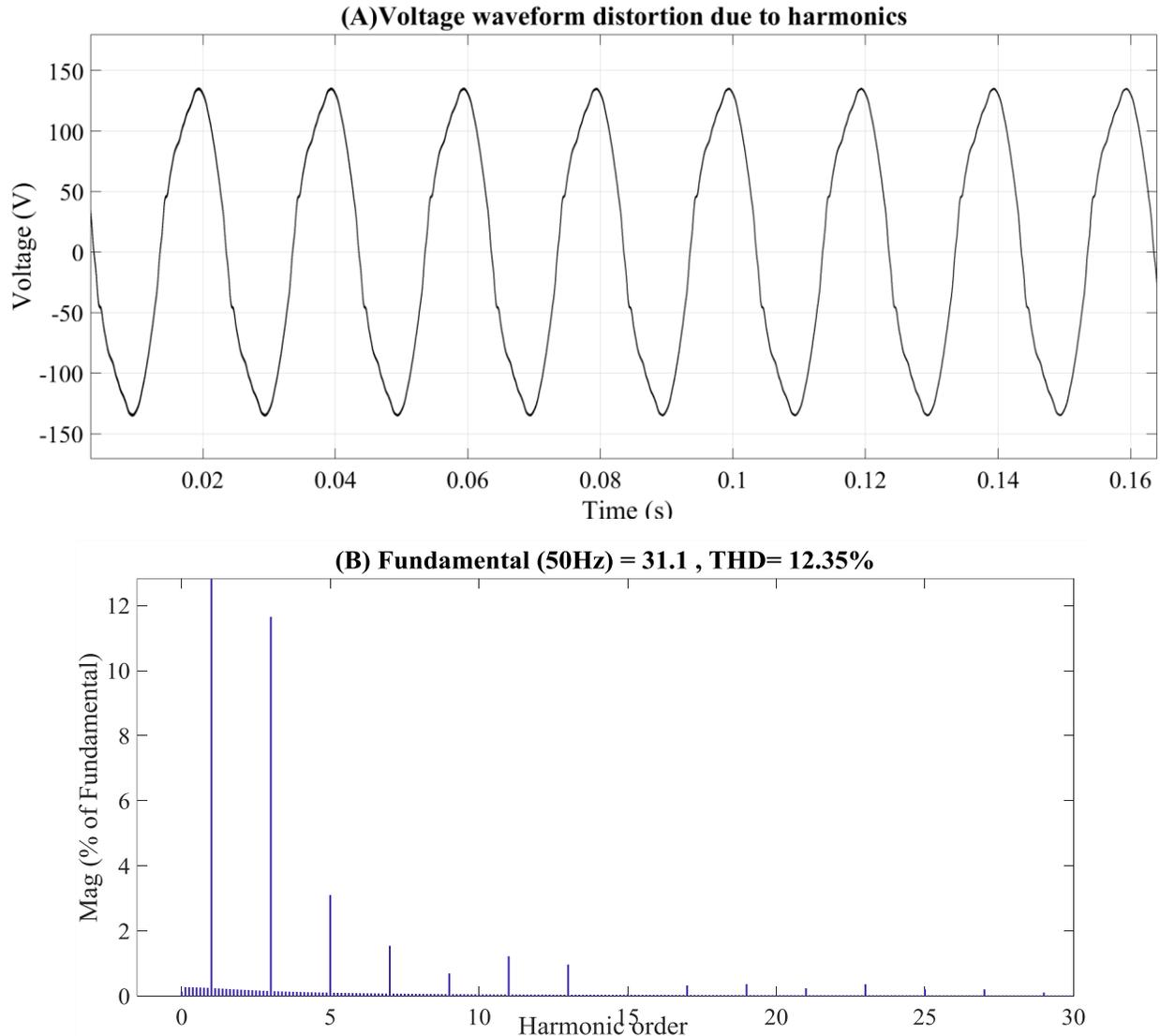


Figure 6 (A) Voltage waveform distortion due to harmonics with an isolated source and its (B) harmonic spectrum

Now, with the same methodology is applied on the distribution network. The total load on the distribution network is 196.9 kW from 74 individual household load distributed in at different section of network as given in figure 1. In the first scenario harmonic power flow analysis is conducted without any PV and linearly scaled harmonic profile from the previous analysis to match the power of individual loads. All loads in the network are assumed to be operating at a power factor of 0.9 which is reasonable owing to the low nature of inductive load in the domestic environment. The resistance of XLPE cable is taken as $0.2613 \times 10^{-3} \text{ Ohm/m}$. The values for individual harmonic current component is obtained for each node represented A, B, C etc. in Figure

1. The section numbering in the proceeding figures is consistently labelled with Figure 1. The harmonic heating on each phase conductor is calculated along with the heating caused due to the RMS component of the (phase) current and the error is depicted in the loss deviation plot in Figure 7. In this figure (7), the heating caused due to normal heating is illustrated via the data points connected by the trace line. The additional loss (per section) caused due to harmonics is subsequently illustrated in each data point for each section of the network. The normal heating loss is calculated by equation (7) and heating loss with harmonics by equation (5). The heating loss in all the figures is provided in watt per meter. The first observation from Figure 7 is that harmonic heating is much more in line 2 (L2) which is the result of high loading in L2 and a high THD in L2 as shown in Figure 8. Furthermore, it can be observed that the harmonic heating increases as it moves from last section to first due to cumulative effect of harmonic propagation at the main feeder. The difference in error at certain sections is almost twice the RMS heat calculated which forms the strong evidence to the proposed problem of major effect of harmonic heating on conductors. The load on line 3 (L3) is considerably lower and hence the difference in harmonic heating is much less, which leads to the conclusion that the harmonic heating issue not only depends on the harmonic content in the system but is also a major threat when the system is operating around its maximum loading limits. Interestingly, distribution systems seldom operate at maximum loading limits and hence the effects may not be obvious. However, power system engineers are increasingly being challenged to push system loading to higher levels day by day and hence the effects may soon become readily visible in the system.

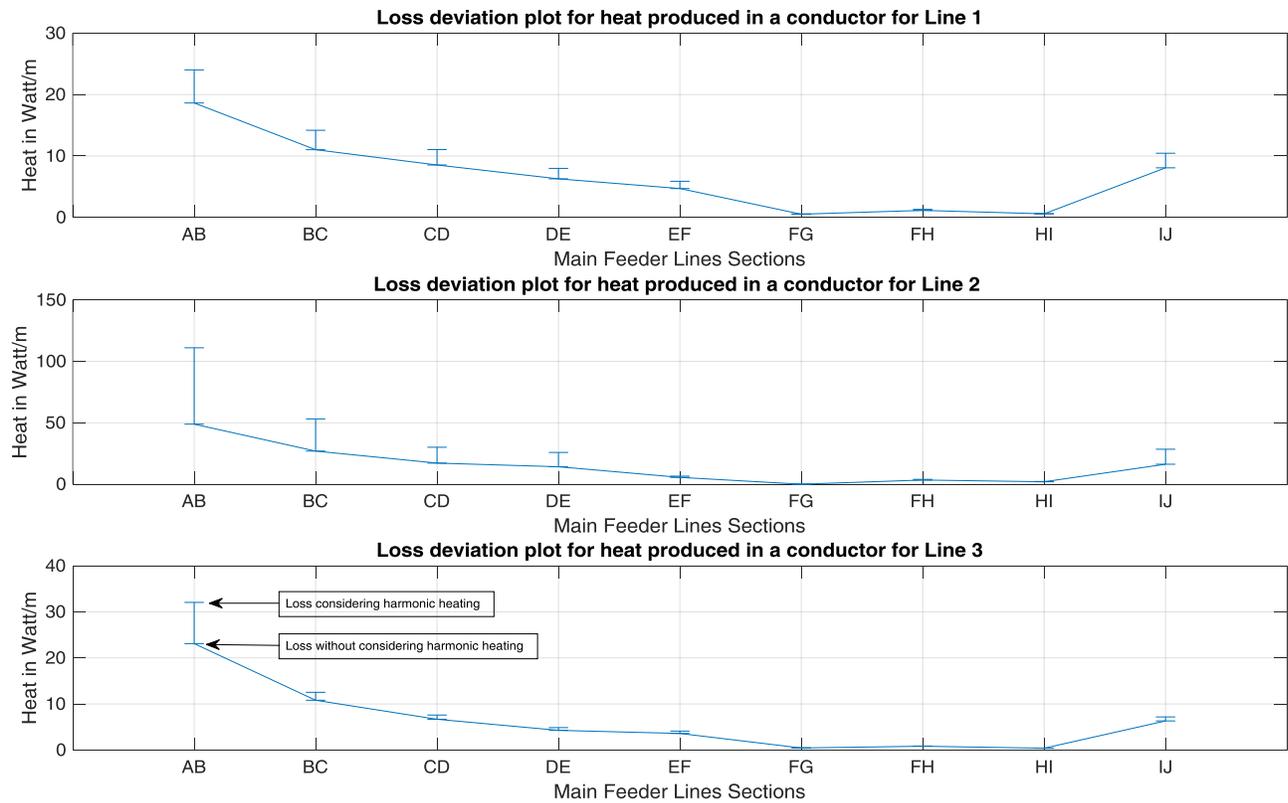


Figure 7 : Loss deviation plot for harmonic heating in individual phase without solar PV

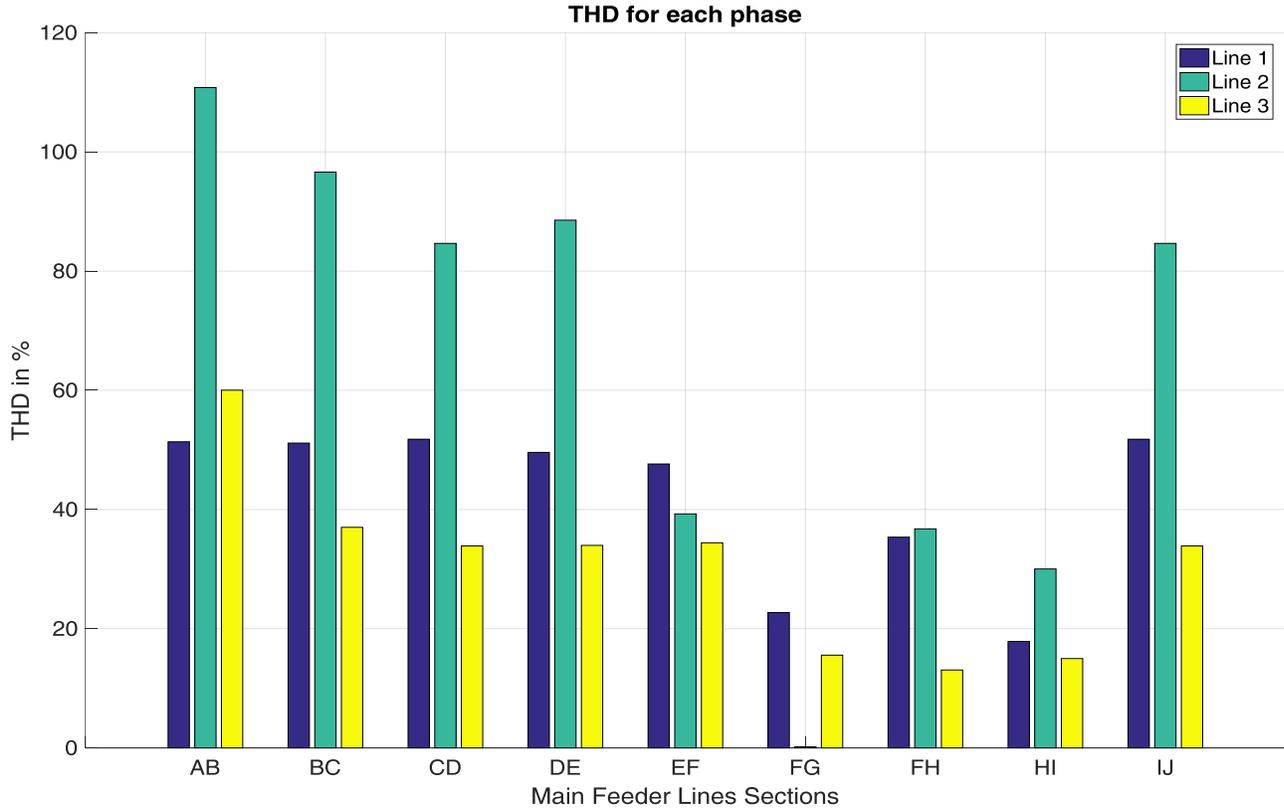


Figure 8 THD in each phase for every section without PV

The second part of analysis presented in this work considers the inclusion of solar PV generators. In this regard, the distribution network model supports a hosting capacity of 36.7%, where the contribution by PV to the total load is 184.5kW. This is in accordance with the work presented in [23] where the authors suggest the 36.7 % as an optimal hosting capacity for the network if network control mechanisms are to be avoided. With this scenario 98% of the total load connected to the network is supplied by solar PV. PV systems are arbitrarily placed throughout the network in such a way that the nodal voltage will not raise above the regulations (1.10 pu). Now, harmonic power flow is executed and harmonic heating calculations are conducted. Consideration of Figure 9 suggests that the heat produced in the individual sections of main feeder has reduced considerably owing to the fact that, at each node the majority of load is supplied by the local PV and hence the power transmitted through the main feeder is very small. However, it is apparent that while sufficiently smaller in magnitude, the associated loss deviation plot shows a considerable loss ratio when the loss due to harmonics are compared to the normal (RMS) heating loss. These facts conclude that, even though the PV is a harmonic source it helps to reduce the heating by reducing the line loading and in effect reduces the harmonic heating as well. Figure 10 however, shows significant THD values and especially at node 7. This occurs as the PV supplies on the fundamental component of loads and hence all harmonic current requirements are met by main grid which leads to low value of fundamental current in main feeder section and high value of THD in the same. Figure 11 shows a scatter plot of fundamental current in either scenario. The electrical losses, with

or with our PV, is proportional to current flow with and without harmonics (equations (5) and (7) respectively). In Figure 11 at section 1, the fundamental current before having PV in the network was just over 350 A and with introduction of PV the fundamental current has decreased to be close to 90 A. This is the cause for reduction in heat in Figure 9 and increase in THD in Figure 10. This scenario may not seem to be a problem as the heating in the cable is much less, but, the power factor at the substation transformer would be so low to have economic operation and may further cause saturation of transformer cores. This points to the need for a balance in PV penetration from a harmonic perspective to have a safe stable and economic operation of the distribution network. Different combinations of PV hosting capacity, loads and harmonic profiles could be considered for analysis. For example, preliminary analysis considering non-linear loads with varying THD at the end of this network (pillar J) indicated significant implications for percentage THDv manifestation at that part of the network; increasing by a factor of 4 when load THD increases from 17% to 35%. However, and in the context of serving as a reference, the emphasis in this work is to present extreme (practical) scenarios across the entirety of the network; as illustrated in Figures 9-11.

A set of recommendations and best practices in a building environment is followed which would help to create consumer awareness and help them to regulate the harmonics in their environment to protect and safeguard their equipment's and life.

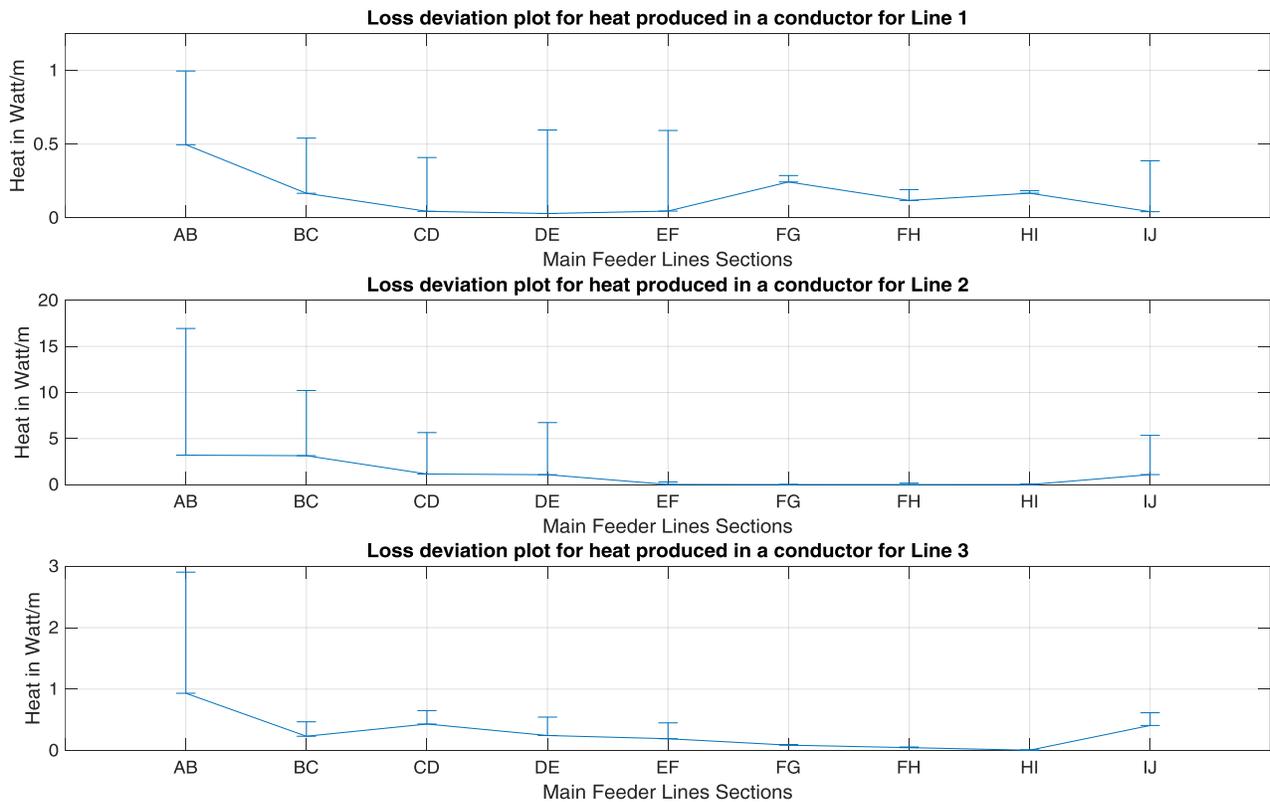


Figure 9 Error plot for harmonic heating in individual phase with solar PV

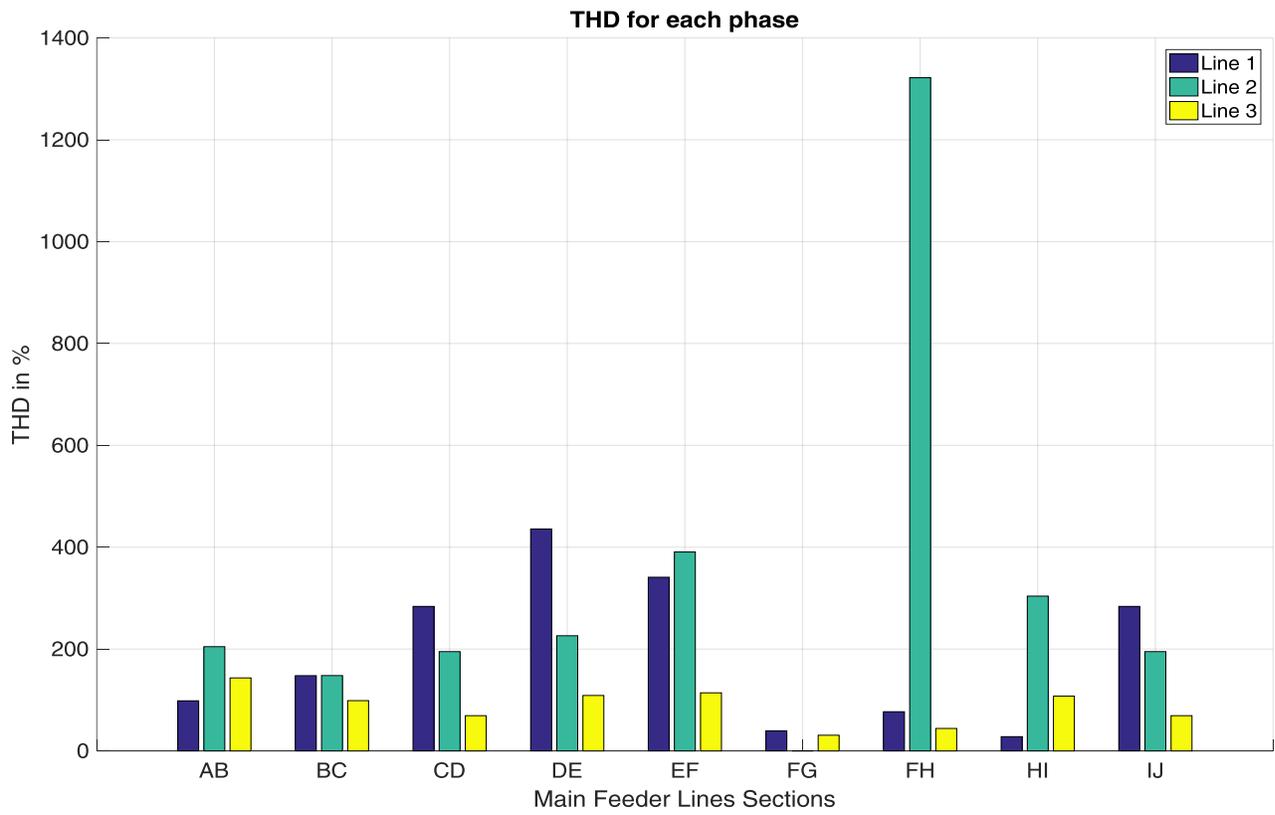


Figure 10 THD in each phase for every section with PV

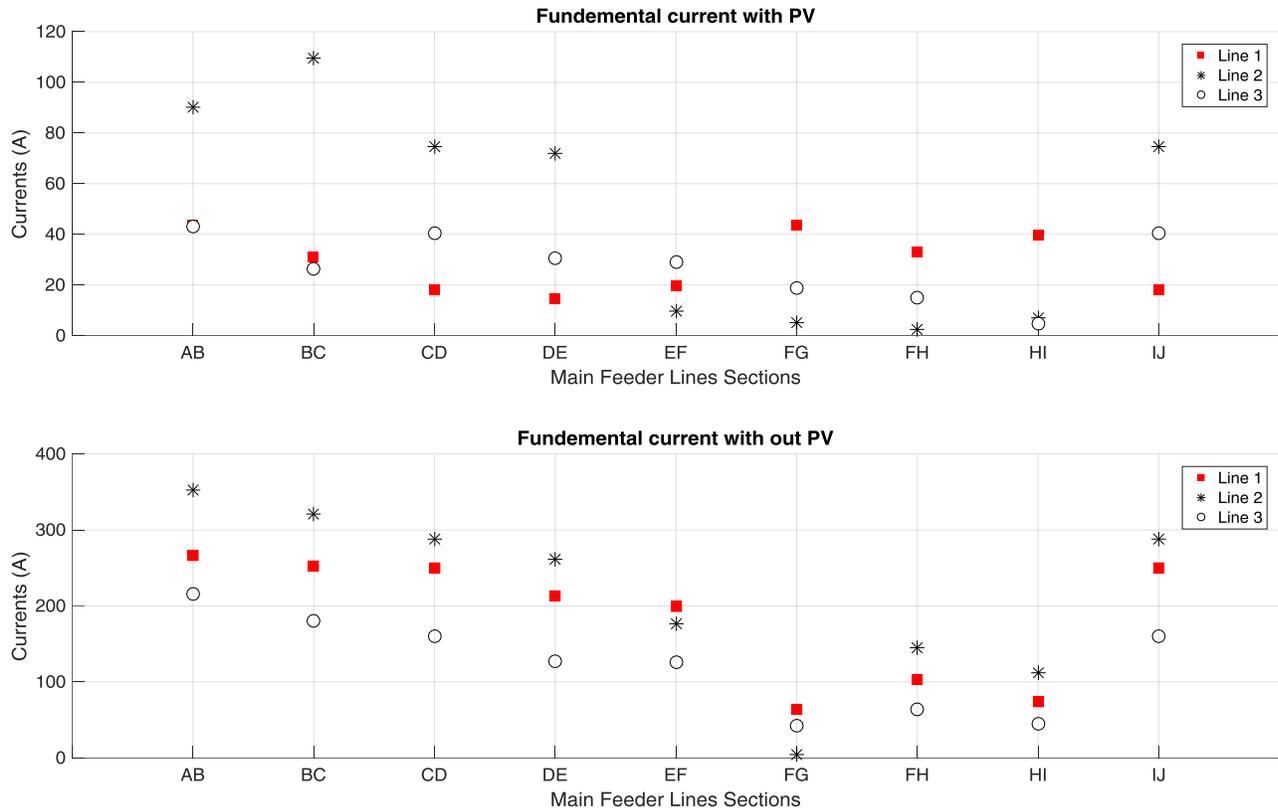


Figure 11 Scatter plot of fundamental current at all phase at each node with and without PV

Recommendations and Best Practices for reducing effect of harmonics in Domestic Envnt.

The following are the recommendations based on the analysis and observation in this work, which can be followed in domestic/building environments to safeguard the equipment involved and reduce the harmful effects of harmonics. These are only simple solutions to the much-understated problem and would need further detailed study and theoretical explanations based on field data to prepare for future penetration of harmonic load.

1. Separate circuit supplying harmonic loads based on the power rating
2. Anticipate for potential load growth during electrical circuit design phase
3. Consider a harmonic rating factor while deciding conductor size
4. Install a generous number of general service outlets,; mitigate against the use of extension cords/leads
5. Use loads with harmonic filters facilitated
6. Prioritize a DC supply, in the context of DG, for loads in the house would help to bypass the issues with harmonics
7. Implement strict regulation for limiting harmonics in the domestic environment.
8. Consider tariffs that incentivise consumers against higher harmonic pollutants
9. Create consumer awareness of the harmful effects of harmonics and sensitive equipment
10. Create a harmonic tolerance rating to understand the withstand capability of devices to a harmonic environment.

Conclusion

Harmonic distortion and its associated problems is not a new concept. However, the issue has heretofore not been afforded sufficient importance within the domestic environment. The analysis presented in this paper indicates the need to consider the same in a building system to preserve and maintain the stable long term operation of building electrical services in the context of modern smart environment scenario. The cable heating effect associated with harmonic current should be carried out during the design phase of the building itself. This calls for much more accurate anticipation of loads and consumer behaviour as well. The BS7671 wiring standards have provided a harmonic derating factor which should be considered at the design phase with 3 phase systems. However, in the context of single phase, the presented analysis may also be used to derate the associated conductors. While this could lead to a prevalence of potentially oversized cable, assurances in the context of enhanced safety provisions for equipment and human/appliance engagement are justifiable outcomes in this regard.

The initial analysis of a domestic wiring circuit, indicated that there is a significant deviation in respect to expected power loss and actual power loss in cables as a consequence of harmonic distortion. The impact of such deviation may pose a threat only when accumulation of harmonics occur at main circuits which is rare under present circumstance. But with increased penetration of non-linear loads and the use of extension/multipin leads may end up with scenarios which threaten the safety of consumer and equipment.

The harmonic heating analysis conducted on the distribution network reveals that the situation is much worse than anticipated previously and a worst case scenario consideration suggests catastrophic implications for the network. While such a 'worst case scenario' is highly unlikely, it offers better insight (as a reference) rather than a consideration of variable non-linear load integration and network connection positioning. That notwithstanding, more work is required to understand optimisation in the context of voltage regulation, harmonic heating effects and THDv with increasing non-linear load (and generation).

The results of the analyses presented with the renewable energy source integration (solar PV) suggest that with increases in PV penetration the active element of power may be reduced, but the THD can increase even though the harmonic content in the network may not have varied significantly. The increased THD may not cause dangerous level of heating, but the essence of this analysis is on the fact that THD may not be used as an implication of harmonic pollution in the network. Another interesting finding from this scenario was the increase in voltage distortion with utilization of PV generators. In a particular case it has been observed that when THD of the load increases from 17% to 35%, the harmonic voltage distortion increases by a factor of 4. This is however not a concern to harmonic heating as seen in the results but it could severely affect distribution transformers and economic operation of distribution network. The interesting fact in the presented study is that, the largest harmonic/non-linear load of distribution network for the modern era 'Electric Vehicle (EV)' is not considered. So with increased EV penetration the worst case scenario may not be as farfetched as it might seem.

The investigation and the insight obtained along with previous knowledge leads to the formulation of recommendations and best practice suggestions for consumers to safeguard themselves and their equipment from the ill effects of harmonics and harmonic heating.

Harmonics is like an inexorable demon in certain cases, however, by being aware of it, using best practices and by abiding to the regulations would allow us to keep the demon at bay.

REFERENCES

- [1] N. Watson and J. Arrillaga, *Power systems electromagnetic transients simulation*. 2003.
- [2] A. Kalair, N. Abas, A. R. Kalair, Z. Saleem, and N. Khan, “Review of harmonic analysis, modeling and mitigation techniques,” 2017.
- [3] M. Farhoodnea, A. Mohamed, H. Shareef, and H. Zayandehroodi, “Power quality impacts of high-penetration electric vehicle stations and renewable energy-based generators on power distribution systems,” 2013.
- [4] S. K. Khadem, M. Basu, and M. F. Conlon, “Power quality in grid connected renewable energy systems: role of custom power devices,” 2010.
- [5] A. Gil-de-Castro, S. K. Ronnberg, and M. H. J. Bollen, “A study about harmonic interaction between devices,” in *2014 16th International Conference on Harmonics and Quality of Power (ICHQP)*, 2014, pp. 728–732.
- [6] M. S. Munir, Y. W. Li, and H. Tian, “Improved Residential Distribution System Harmonic Compensation Scheme Using Power Electronics Interfaced DGs,” *IEEE Trans. Smart Grid*, vol. 7, no. 3, pp. 1191–1203, May 2016.
- [7] N. F. Guerrero-Rodríguez, A. B. Rey-Bou E, L. C. Herrero-De Lucas, and F. Martinez-Rodrigo, “Control and synchronization algorithms for a grid-connected photovoltaic system under harmonic distortions, frequency variations and unbalances,” 2015.
- [8] K. Fekete, Z. Klaic, and L. Majdandzic, “Expansion of the residential photovoltaic systems and its harmonic impact on the distribution grid,” *Renew. Energy*, 2012.
- [9] D. Sko, M. Tovilovi, and N. L. Rajakovi, “The simultaneous impact of photovoltaic systems and plug-in electric vehicles on the daily load and voltage profiles and the harmonic voltage distortions in urban distribution systems,” *Renew. Energy*, vol. 76, pp. 454–464, 2015.
- [10] J. A. Palmer, R. C. Degeneff, T. M. McKernan, and T. M. Halleran, “Determination of the effect of harmonics on pipe-type power cable AC/DC resistance ratios,” *IEEE Trans. Magn.*, vol. 29, no. 2, pp. 1427–1433, Mar. 1993.
- [11] J. Blackledge, K. O ’connell, M. Barrett, and A. Sung, “Cable Heating Effects due to Harmonic Distortion in Electrical Installations,” 2012.
- [12] I. Regulations and S. Edition, “Requirements for Electrical Installations,” *BS7671-2008*, 2008.
- [13] J. Yong, L. Chen, and S. Chen, “Modeling of Home Appliances for Power Distribution System Harmonic Analysis,” *IEEE Trans. Power Deliv.*, vol. 25, no. 4, pp. 3147–3155, Oct. 2010.
- [14] F. Waite, D. Payne, J. Pilgrim, P. Lewin, and A. Gorwadia, “Quantifying possible transmission network benefits from higher cable conductor temperatures,” *IET Gener.*

- Transm. Distrib.*, vol. 7, no. 6, pp. 636–644, Jun. 2013.
- [15] E. 2004- ETCI, “NATIONAL RULES FOR ELECTRICAL INSTALLATIONS,” 2004.
- [16] H. E. Mazin, E. E. Nino, W. Xu, and J. Yong, “A Study on the Harmonic Contributions of Residential Loads,” *IEEE Trans. Power Deliv.*, vol. 26, no. 3, pp. 1592–1599, Jul. 2011.
- [17] D. Salles, C. Jiang, W. Xu, W. Freitas, and H. E. Mazin, “Assessing the Collective Harmonic Impact of Modern Residential Loads—Part I: Methodology,” *IEEE Trans. Power Deliv.*, vol. 27, no. 4, pp. 1937–1946, Oct. 2012.
- [18] S. Khadem, R. Kerrigan, M. Basu, and B. Basu, “A Study on the Power Quality of DG Integrated Building Energy System in Virtual Environment,” *Conf. Pap.*, Jan. 2013.
- [19] Chauvin-Arnoux, “Single phase power quality analyser, C.A 8230.” [Online]. Available: http://www.chauvin-arnoux.com/sites/default/files/D00QPA50_4.PDF. [Accessed: 24-Jul-2017].
- [20] SEAI, “Your Guide to Electricity in the Home,” Wilton place, Dublin, Ireland, , 2008.
- [21] S. K. Khadem, R. Kerrigan, M. Basu, B. Basu, S. K. Khadem Member IEEE, M. Basu Member IEEE, and B. Basu Member IEEE, “A Study on the Power Quality of DG Integrated Building Energy System in Virtual Environment Recommended Citation "A study on the power quality of DG integrated building energy system in Virtual Environment A Study on the Power Quality of DG Integrated Building Energy System in Virtual Environment,” vol. 15, pp. 2–5, 2013.
- [22] K. Sunderland, M. Coppo, M. Conlon, and R. Turri, “A correction current injection method for power flow analysis of unbalanced multiple-grounded 4-wire distribution networks,” *Electr. Power Syst. Res.*, vol. 132, pp. 30–38, 2016.
- [23] S. Pukhrem, M. Basu, M. F. Conlon, and K. Sunderland, “Enhanced Network Voltage Management Techniques Under the Proliferation of Rooftop Solar PV Installation in Low-Voltage Distribution Network,” *IEEE J. Emerg. Sel. Top. Power Electron.*, vol. 5, no. 2, pp. 681–694, Jun. 2017.
- [24] R. C. Dugan, “Reference Guide The Open Distribution System Simulator(OpenDSS),” 2016.
- [25] A. Mansoor, “Lower order harmonic cancellation: impact of low-voltage network topology,” in *IEEE Power Engineering Society. 1999 Winter Meeting (Cat. No.99CH36233)*, 1999, pp. 1106–1109 vol.2.
- [26] M. Rylander and J. Smith, “Stochastic Analysis to Determine Feeder Hosting Capacity for Distributed Solar PV,” *EPRI Tech. Updat. 1026640*, 2012.
- [27] T. M. Gruz, “A Survey of Neutral Currents in Three-Phase Computer Power Systems,” *IEEE Trans. Ind. Appl.*, vol. 26, no. 4, pp. 719–725, 1990.
- [28] anexo 2 Gobeirna De Espana, Guía técnica de aplicación en BT, “Cálculo DE Caídas De

Tensión, (Technical Guide for application to the Low Voltage Electrotechnical Regulation),” 2003.

- [29] I. E. C. "61000-3-6. . Standard, “IEC TR 61000-3-6:2008 Electromagnetic compatibility (EMC) - Part 3-6: Limits - Assessment of emission limits for the connection of distorting installations to MV, HV and EHV power systems.”