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Isolated effects of footwear structure and cushioning on running mechanics in habitual mid/forefoot runners

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1 ABSTRACT

The true differences between barefoot and shod running are difficult to directly compare 2 because of the concomitant change to a mid/forefoot footfall pattern that typically occurs 3 4 during barefoot running. The purpose of this study was to compare isolated effects of footwear structure and cushioning on running mechanics in habitual mid/forefoot runners running shod 5 (SHOD), barefoot (BF), and barefoot on a foam surface (BF+FOAM). Ten habitually shod 6 7 mid/forefoot runners were recruited (male=8, female=2). Repeated measures ANOVA $(\alpha=0.05)$ revealed differences between conditions for only vertical peak active force, contact 8 time, negative and total ankle joint work, and peak dorsiflexion angle. Post hoc tests revealed 9 that BF+FOAM resulted in smaller vertical active peak magnitude and instantaneous vertical 10 11 loading rate than SHOD. SHOD resulted in lower total ankle joint work than BF and BF+FOAM. BF+FOAM resulted in lower negative ankle joint work than either BF or SHOD. 12 Contact time was shorter with BF than BF+FOAM or SHOD. Peak dorsiflexion angle was 13 smaller in SHOD than BF. No other differences in sagittal joint kinematics, kinetics, or ground 14 reaction forces were observed. These overall similarities in running mechanics between SHOD 15 and BF+FOAM question the effects of footwear structure on habituated mid/forefoot running 16 described previously. 17

19 Introduction

Barefoot running has been proposed to potentially lower the risk of running related injury because it results in a shorter stride length, reduced collision force, greater somatosensory information, and greater foot muscle strength compared with shod running (refer to (Hall et al., 2013; Jenkins & Cauthon, 2011; Tam et al., 2014) for comprehensive reviews). However, it is unclear how barefoot running directly compares with shod running because of the concomitant change to a mid/forefoot footfall pattern (Divert, Mornieux, et al., 2005; Gruber, Silvernail, et al., 2013).

27 A change from a rearfoot to a mid/forefoot pattern is suggested to be a kinematically mediated effect of running barefoot on a hard surface without cushioning to protect the heel 28 (Frederick, 1986; Gruber, Silvernail, et al., 2013) and may be the primary mechanism for the 29 mechanical differences between shod and barefoot running (De Wit et al., 2000; Lieberman et 30 al., 2010). Further, removing the cushioning from the foot-ground interface will result in altered 31 joint stiffness (e.g. (Ferris et al., 1998; Hardin et al., 2004; Nigg et al., 1987; Sinclair et al., 32 2016)), which is also affected by footfall pattern (Hamill, Gruber, et al., 2014; Lussiana et al., 33 2017). Changing the total stiffness of the system (individual-footwear-surface) will thus 34 introduce changes in running mechanics that cannot be separated from the effects of simply 35 removing the shoe structure because the cushioning is also removed. 36

Features of traditional running shoes, such as heel flare, heel-toe drop, and heel lift, may not be important when initial contact is anterior on the foot, or may have different effects on mid/forefoot running mechanics than were intended for rearfoot running. Given the high interaction of footfall pattern on the mechanical differences between barefoot versus shod running, it is unclear if the potential benefits, or detriments, of barefoot running are a result of being unshod alone, the subsequent change in footfall pattern, or the cushioning properties of the foot-ground interface.

A previous study comparing barefoot versus shod running while controlling for footfall 44 pattern used habitually shod rearfoot runners (Shih et al., 2013). Having participants perform 45 rearfoot and mid/forefoot patterns under both barefoot and shod conditions using a within-46 participants design is an excellent method to isolate the effects of footwear while removing the 47 influence of footfall pattern. Although runners in both habitual footfall pattern groups seem to 48 replicate the alternate pattern successfully in studies comparing footfall patterns while shod 49 50 (Boyer et al., 2014; Williams et al., 2000), introducing two sources of task novelty -alternate footfall pattern and running barefoot- may cause altered running mechanics than those who are 51 52 habituated. This altered movement may result in running mechanics that are either too variable to uncover meaningful relationships between outcomes or do not represent the running 53 mechanics of a habitual barefoot runner. For example, habitual minimalist and barefoot runners 54 tend to land with a mid/forefoot pattern (Goss & Gross, 2012; Hollander et al., 2017; 55 Lieberman et al., 2010), but this footfall pattern is not universally adopted by habitually shod 56 rearfoot runners during acute exposure to barefoot or minimalist shoe running (Gruber, 57 Silvernail, et al., 2013; Hollander et al., 2015; Paquette et al., 2013; Williams et al., 2012). 58 Therefore, error in running mechanics or increased variability may lead to inappropriate 59 conclusions regarding the characterization of a barefoot gait pattern and the potential benefits 60 of barefoot running. Examining the differences in running mechanics between shod and 61 barefoot running in habitual mid/forefoot runners would identify the direct influence of the 62 shoe without introducing error from task novelty. 63

The complex interaction of footfall pattern with shod versus barefoot running make it difficult to understand if the shoe properties, shoe cushioning, or the change in footfall pattern cause the well-documented changes in gait mechanics with barefoot running (e.g., (Hall et al., 2013; Jenkins & Cauthon, 2011; Tam et al., 2014)). Only by controlling for both cushioning and task-specific movement control (i.e., habitual footfall pattern), can the effects of running

barefoot/unshod be understood. The effects of being unshod can be isolated from the effect of 69 cushioning by comparing the change in gait mechanics within habitual mid/forefoot runners 70 while running shod verses barefoot on a foam surface constructed out of a common footwear 71 72 material, ethyl-vinyl acetate (EVA). The effects of cushioning the foot-ground interface can be isolated from the effects of being unshod by comparing barefoot running on a bare, laboratory 73 floor with barefoot running on EVA foam. Therefore, the aim of the present study was to 74 examine the differences in strike index, impact forces, and joint kinetics as well as relevant 75 frontal and sagittal joint angles between running shod, barefoot on concrete, and barefoot on 76 77 EVA foam in habitual mid/forefoot runners using a within-subjects design. We consider this study descriptive and preliminary and so we present the null hypothesis: there will be no 78 significant differences in gait mechanics between conditions in habitually shod, mid/forefoot 79 80 runners.

81

82 Materials and Methods

83 **Participants**

Runners were recruited as part of a larger study involving rearfoot and non-rearfoot 84 runners via flyers posted on the university campus and surrounding community. All 85 participants were healthy and free of musculoskeletal pain or injury within at least the previous 86 87 12 months. Ten habitually shod mid/forefoot runners (8 midfoot strikers, 2 forefoot strikers) were enrolled for the present study following footfall pattern screening (8 male, 2 female; Mean 88 \pm SD; Age (years): 25 \pm 7; Stature (cm) 177 \pm 0.1; Mass (kg) 71.32 \pm 6.54, current running 89 volume (km·week⁻¹) 46.5 ± 25.9). Habitual footfall pattern was assessed while participants ran 90 91 overground at their preferred pace while wearing the allocated footwear for the shod running condition (RC 550, New Balance, Brighton, MA, USA). Participant footfall pattern was 92 confirmed using the strike index (Cavanagh & Lafortune, 1980), sagittal plane ankle angle 93

measurements, and a blunted or absent vertical impact peak (Gruber, Boyer, et al., 2013).
Participants gave written informed consent before participating. Ethical approval was granted
by the University of Massachusetts institutional review board.

97

98 Equipment

Participants were brought to an indoor biomechanics lab and were asked to run over 99 ground at 3.5 m·s⁻¹ (\pm 5%) under three conditions: barefoot ("BF"); barefoot with foam mats 100 ("BF+FOAM", EVA 2.0cm depth, 55 Shore C durometer foam); and traditional, neutral 101 102 running shoes ("SHOD", RC 550, New Balance, Brighton, MA, USA, 215.7 g). Testing took place over a 25 m runway embedded with a force platform (OR6-5, AMTI, Watertown, MA, 103 USA) measuring 120 x 60 cm. Ground reaction force (GRF) and centre of pressure data were 104 collected at 1200 Hz. During the BF+FOAM condition, the foam mats were laid over the length 105 of the runway continuously. The mat in the centre of the collection volume included a cut-out 106 that matched the dimensions of the force platform. The height of the contact surface above the 107 force platform was addressed in the data processing (see below). Running speed was monitored 108 by photoelectric sensors (Lafayette Instruments, Lafayette, IN, USA) positioned 3m before and 109 after the centre of the force platform. Kinematic data were captured at 240 Hz using an eight-110 camera optical motion capture system (Oqus 300, Qualisys AB, Göthenburg, SWE). Retro-111 reflective spherical markers were placed on the pelvis and right lower extremity using an 112 established marker set (Hamill, Selbie, et al., 2014) and secured with tape and textile foam 113 wraps. Markers placed on the foot were secured with tape on the shoe over the heel, 1st and 5th 114 metatarsal heads, and distal end of the great toe for the shod condition. Markers were secured 115 on the skin with tape over the same anatomical landmarks for both barefoot conditions (BF, 116 BF+FOAM). 117

119 *Testing Procedure*

A standing calibration was collected before the shod and first barefoot condition in 120 order to calculate segment lengths and joint centre positions (Hamill, Selbie, et al., 2014). 121 Participants were instructed to "run normally" and practiced running under each condition until 122 they felt comfortable and found a starting point that allowed them to contact the force platform 123 with the whole foot (≥ 8 m). Ten acceptable trials were completed for each participant in each 124 of the three conditions (BF, BF+FOAM, SHOD). Trials were considered acceptable if the 125 participant ran within the speed threshold ($3.5 \text{ m}\cdot\text{s}^{-1}\pm5\%$), did not change running speed within 126 127 the collection volume, landed on the force plate with the whole foot of the right limb, and did not target or alter stride to land on the force platform completely. The order of the conditions 128 was semi-randomised determined using a random number generator; barefoot conditions were 129 presented together (but in a random order) to avoid differences in marker placement between 130 BF and BF+FOAM. Therefore, SHOD was presented randomly but constrained to be either 131 first or last. 132

133

134 Data Processing

Marker position data were tracked using Qualisys Track Manager software (Qualisys 135 AB, Göthenburg, SWE) and exported to Visual3D software for signal processing (C-Motion, 136 Rockville, MD, USA). Marker positions and force platform data were filtered using a 4th order 137 low-pass Butterworth filter using cut-off frequencies of 15 Hz and 50 Hz, respectively. Raw 138 GRF data were filtered at 15 Hz before the joint moments were calculated (Kristianslund et al., 139 2012). The minimum force threshold was 20 N. Prior to any filtering or data processing, the 140 "FORCE STRUCTURES" command in Visual3D was used for the BF+FOAM condition to 141 account for the contact surface of the foam being offset from the surface of the force platform 142 (refer to C-Motion, Inc. online documentation). 143

Contact time was the time between initial contact with the force platform and toe-off. 144 Strike index (SI) was calculated to assess footfall pattern as a continuous variable (Cavanagh 145 & Lafortune, 1980). Vertical active peak (VActP) was the magnitude of the global maximum 146 of the vertical ground reaction force. Maximum instantaneous vertical loading rate (VLR) was 147 calculated by first identifying the time of peak vertical impact force using the method of 148 Blackmore et al. (Blackmore et al., 2016) for all trials. Next, the first derivative of the filtered 149 150 (50 Hz cut-off) vertical force platform data was calculated using the central difference method to find the largest instantaneous slope magnitude between 20%-80% of the time to peak vertical 151 152 impact force. The method by Blackmore et al. (Blackmore et al., 2016) was used to ensure a data-driven method for identifying the time to peak vertical impact force. The instantaneous 153 VLR calculation method was selected because it follows the method used in previous research 154 examining the association of VLR to running injuries (Zadpoor & Nikooyan, 2011) and many 155 papers comparing footfall patterns and barefoot running (e.g. (Au et al., 2018; Boyer et al., 156 2014; Rice & Patel, 2017; Samaan et al., 2014; Shih et al., 2013)). Anterior-posterior loading 157 rate (APLR) was calculated as the largest instantaneous slope magnitude between 20%-80% of 158 the time to the first visible local maximum in the breaking phase. 159

Three-dimensional joint angles and joint kinetics were calculated using established 160 procedures (Hamill, Selbie, et al., 2014; Selbie et al., 2014). Specifically, joint angles were 161 calculated using an X-Y-Z (mediolateral-anteroposterior-vertical axes) using Cardan rotation 162 sequence with the proximal segment as reference. Ankle joint angles were calculated using a 163 virtual foot segment coordinate system that was aligned with the lab coordinate system. Internal 164 joint moments were calculated using a Newton-Euler inverse dynamics procedure. Positive 165 angles indicated hip and knee flexion, ankle dorsiflexion, knee and hip adduction, and ankle 166 inversion. Positive joint moments followed the same convention except for knee flexion, which 167 was negative. 168

Ankle, knee, and hip joint work in the sagittal plane was determined by first calculating joint power as the product of the joint moments and joint angular velocity then integrating the area under the joint power-time curve. Total joint work was the cumulative area under positive and negative portions of the power-time curve. Positive and negative work was the sum of the positive and negative areas under the power-time curve, respectively.

Peak values for specific sagittal and frontal plane joint angles and moments were used 174 175 in the examination of differences between conditions. Angles at initial ground contact were also examined to aid in the assessment of dynamics at the foot-ground interface. For this 176 177 descriptive study, variables were selected in consideration of previous studies comparing barefoot, minimalist, and shod running and comparing rearfoot and mid/forefoot patterns (e.g., 178 (Anderson et al., 2020; Hall et al., 2013; Jenkins & Cauthon, 2011; Tam et al., 2014; Xu et al., 179 2021)). Select frontal plane joint angle variables were also included given their potential 180 relevance to running injury development (e.g., (Ceyssens et al., 2019; Dudley et al., 2017; 181 Kuhman et al., 2016)). Peak ankle inversion moment was included because it is a suggested 182 key variable for recommending habitual mid/forefoot runners avoid traditional footwear (Davis 183 et al., 2017; Rice et al., 2016). Refer to Tables 1 and 2 for a complete list of variables. 184

185

186 Statistical Analysis

187 Differences between conditions (BF, BF+FOAM, SHOD) were examined with a 188 repeated measures ANOVA. Statistical significance was accepted at $\alpha \le 0.05$. Specific mean 189 differences (Mean_{diff}) between conditions were examined using pairwise comparisons under an 190 adjusted Bonferroni correction given the three comparisons (SPSS V20.0, SPSS Inc., Chicago, 191 Illinois, USA). Additionally, 95% confidence intervals (CI_{diff}) are reported and considered in 192 the interpretation of the likelihood of the difference. Data were verified for normality using a 193 Shapiro-Wilk test. A Huynh-Feldt correction was used where data failed Mauchly's test of 194 Sphericity. Effect sizes are reported as partial eta squared (ηp^2) for main effects. Given the 195 small sample size and multiple comparisons, we will only consider a main effect as meaningful 196 if the main effect is both significant and ηp^2 is a large effect (>0.14) (Cohen, 1988).

197

198 Results

199 Contact Time, Strike Index, & Ground Reaction Force Variables

200 Descriptive statistics for all ground reaction force variables are listed in Table 1. Vertical and anteroposterior force curves are presented in Figure 1. There was a significant 201 main effect of condition for VActP ($F_{(2,18)} = 6.169$; P = 0.009; $\eta p^2 = 0.41$). Pairwise 202 comparisons identified that VActP was significantly greater in SHOD versus BF+FOAM 203 (Mean_{diff} 118.8N; 95% CI_{diff} [5.8 to 231.8N]; P = 0.039), but VActP was similar between BF 204 and BF+FOAM conditions (Mean_{diff} 33.26; 95% CI_{diff} [-28.9 to 95.42N]; P = 0.453) and 205 between SHOD and BF conditions (Mean_{diff} 85.56N; 95% CI_{diff} [-36.13 to 207.25]; P = 0.208). 206 A significant main effect of condition was also observed for VLR ($F_{(2,18)} = 7.134$; P = 207 0.005; $\eta p^2 = 0.44$). Pairwise comparisons identified that VLR was significantly greater in the 208 BF versus SHOD condition (Mean_{diff} 42970 N/s; 95% CI_{diff} [2023 to 83981 N/s]; P = 0.040), 209 but no difference in VLR was observed between BF and BF+FOAM (Mean_{diff} 20879 N/s; 95% 210 CI_{diff} [-10307 to 52065 N/s]; P = 0.243) or between SHOD and BF+FOAM (Mean_{diff} 22091) 211 N/s; 95% CI_{diff} [-4215 to 48398 N/s]; P = 0.108). 212

213 There were no significant differences in APLR between conditions ($F_{(2,18)} = 0.556$; P = 214 0.583; $\eta p^2 = 0.058$).

215 Descriptive statistics for strike index and contact time are presented in Table 1. No main 216 effect of condition was observed for strike index ($F_{(2,18)} = 0.368$; P = 0.697; $\eta p^2 = 0.04$). A 217 significant main effect of condition was observed for contact time ($F_{(2,18)} = 13.579$; $P \le 0.001$; 218 $\eta p^2 = 0.60$). Pairwise comparisons identified a longer contact time during SHOD versus BF 219 (Mean_{diff} 0.009 s; 95% CI_{diff} [0.003 to 0.016 s]; P = 0.009) and a longer contact time during 220 BF+FOAM versus BF (Mean_{diff} 0.009 s; 95% CI_{diff} [0.004 to 0.013 s]; P = 0.001). No difference 221 in contact time between BF+FOAM vs SHOD was observed (Mean_{diff} 0.001 s; 95% CI_{diff} [-222 0.005 to 0.007 s]; P = 1.00).

223

224 Joint moments

Descriptive statistics for all joint moments can be observed in Table 1. Joint moment curves over stance are presented in Figure 2. No main effects of condition were observed for peak hip flexion moment ($F_{(2,18)} = 0.218$; P = 0.806; $\eta p^2 = 0.02$), peak knee extensor moment ($F_{(2,18)} = 0.497$; P = 0.617; $\eta p^2 = 0.05$), or peak ankle inversion moment ($F_{(2,18)} = 1.368$; P = 0.280; $\eta p^2 = 0.13$).

A main effect of condition was observed for peak plantarflexion moment ($F_{(2,18)} =$ 4.289; P = 0.030; $\eta p^2 = 0.32$). However, pairwise comparisons identified no significant specific differences between SHOD versus BF (Mean_{diff} 13.67 N*m; 95% CI_{diff} [-7.93 to 35.27 N*m]; P = 0.289), and SHOD versus BF+ FOAM (Mean_{diff} 18.77 N*m; 95% CI_{diff} [-3.35 to 40.89 N*m]; P = 0.103).

235

236 Joint work

Descriptive statistics for all joint work variables are listed in Table 1. Joint power curves are presented in Figure 3. No significant main effect of condition was observed at the hip joint for positive work ($F_{(2,18)} = 0.555$; P = 0.584; $\eta p^2 = 0.06$), negative work ($F_{(2,18)} = 2.886$; P =0.082; $\eta p^2 = 0.24$), or total work ($F_{(2,18)} = 2.521$; P = 0.108; $\eta p^2 = 0.22$). For the knee joint, no significant main effect of condition was observed for positive work ($F_{(2,18)} = 0.245$; P = 0.785; $\eta p^2 = 0.03$), negative work ($F_{(2,18)} = 0.259$; P = 0.774; $\eta p^2 = 0.03$), or total work ($F_{(2,18)} = 0.546$; P = 0.589; $\eta p^2 = 0.06$).

There was no significant main effect of condition for ankle positive work ($F_{(2,18)} =$ 244 0.647; P = 0.458; $\eta p^2 = 0.07$). Significant main effects of condition were observed for both 245 negative work ($F_{(2,18)} = 11.956$; P = 0.003; $\eta p^2 = 0.57$) and total work ($F_{(2,18)} = 26.217$; P \leq 246 0.001; $\eta p^2 = 0.74$). With respect to negative ankle joint work, pairwise comparisons identified 247 significantly more negative work during BF versus BF+FOAM (Mean_{diff} 6.23 J; 95% CI_{diff} [-248 0.35 to 12.12 J]; P = 0.038), as well as more negative ankle work during SHOD versus 249 BF+FOAM (Mean_{diff} 20.56 J; 95% CI_{diff} [6.76 to 34.38 J]; P = 0.005). However, there was no 250 difference in negative ankle work between BF and SHOD (Mean_{diff} 14.33 J; 95% CI_{diff} [-1.63 251 252 to 30.3 J; P = 0.082). Total ankle joint work was significantly less during SHOD than both BF (Mean_{diff} 12.49 J; 95% CI_{diff} [3.82 to 21.15 J]; P = 0.007) and BF+FOAM (Mean_{diff} 16.97 J; 253 95% CI_{diff} [10.15 to 23.79 J]; $P \le 0.001$). There was no difference in total ankle work comparing 254 BF versus BF+FOAM (Mean_{diff} 4.48 J; 95% CI_{diff} [-1.06 to 10.03 J]; P = 0.125). 255

256

257 Joint Angles

258 Descriptive statistics and differences in sagittal and frontal plane joint angles for the 259 hip, knee, and ankle are summarized in Table 2 and presented in Figure 4. No significant main 260 effects were observed for any hip or knee angle variable and three ankle angle variables (P >261 0.121).

At the ankle, a significant main effect of condition was observed for the peak dorsiflexion angle ($F_{(2,18)} = 9.480$; P = 0.006; $\eta p^2 = 0.51$). Pairwise comparisons identified SHOD resulted in a greater peak dorsiflexion angle than BF (Mean_{diff} 3.15 deg; 95% CI_{diff} [1.13 to 5.03 deg]; P = 0.003). However, no significant difference in peak dorsiflexion angle wase observed between SHOD versus BF+FOAM (Mean_{diff} 2.86 deg; 95% CI_{diff} [-0.23 to 5.94 deg]; P = 0.072) or between BF+FOAM versus BF (Mean_{diff} 0.27 deg; 95% CI_{diff} [-1.52 to 2.06 deg]; P = 1.00). There was a significant main effect of conditions for frontal plane ankle angle at touch down ($F_{(2,18)} = 4.650$; P = 0.024; $\eta p^2 = 0.34$). However, pairwise comparisons did not identify significant differences between SHOD versus BF (Mean_{diff} 3.12 deg; 95% CI_{diff} [-0.35 to 6.59 deg]; P = 0.081), SHOD versus BF+FOAM (Mean_{diff} 2.93 deg; 95% CI_{diff} [-0.82 to 6.67 deg]; P = 0.143), or between BF+FOAM versus BF (Mean_{diff} 0.20 deg; 95% CI_{diff} [-2.61to 3.01 deg]; P = 1.00).

275

276 Discussion and Implications

277 The purpose of this study was to characterize the specific effects of being barefoot on running mechanics by eliminating any potential effects of habitual footfall pattern and isolating 278 effects of cushioning by including a condition of running barefoot on an EVA foam surface. 279 Comparing the SHOD and BF+FOAM conditions isolated the effects of being unshod while 280 cushioning between the foot-ground interface was maintained whereas comparing BF and 281 BF+FOAM conditions isolated the effects of cushioning alone. Our null hypothesis was not 282 supported. When cushioning of the foot-ground interface was maintained (SHOD vs. 283 BF+FOAM), being unshod resulted in reduced peak vertical active force and negative ankle 284 joint work but increased total ankle joint work. Remaining unshod but removing cushioning 285 from the foot-ground interface (BF vs. BF+FOAM) resulted in a shorter contact time and 286 increased negative ankle joint work. Compared with shod running, running barefoot with no 287 external cushioning (SHOD vs. BF) resulted in a shorter contact time, greater vertical loading 288 rate, and greater total ankle joint work. No differences in peak joint angles, peak joint moments, 289 or joint work were observed at the hip and knee and no variable was significantly different 290 between all three conditions. The differences in joint mechanics were isolated at the ankle 291 which supports previous conclusions that shod forefoot running was controlled at the ankle 292 whereas shod rearfoot running was controlled at the knee (Davis et al., 2017; Hamill, Gruber, 293

et al., 2014). Few studies have directly examined the differences in barefoot and shod running
in habitual mid/forefoot runners, making direct comparison of our findings to current literature
limited. Given that this was a descriptive study, the mechanisms for the observed differences
between conditions need further investigation.

Barefoot running is often advocated to prevent running injuries, in part, by reducing the 298 VLR (Divert, Baur, et al., 2005; Divert, Mornieux, et al., 2005; Samaan et al.; Utz-Meagher et 299 300 al., 2011), but this effect had limited evidence in a recent systematic review and was dependent on footfall pattern (Hall et al., 2013). Our results suggest that the effects of barefoot running 301 302 on VLR may be dependent on habituation to a mid/forefoot pattern and surface conditions given that strike index did not change between SHOD, BF, and BF+FOAM. Some previous 303 studies comparing barefoot and shod running found no differences in VLR when footfall 304 pattern was maintained by either including habitual mid/forefoot runners (Paquette et al., 2013) 305 or by asking habitual rearfoot runners to run with a mid/forefoot pattern (Shih et al., 2013). 306 Those findings contrast with Rice et al. (Rice & Patel, 2017) who concluded that both, 307 minimalist footwear and a forefoot pattern, were required together to reduce VLR compared 308 with either rearfoot or forefoot running in traditional footwear. However, minimalist and 309 barefoot running are not equivalent (Bonacci et al., 2013; Sinclair et al., 2013; Squadrone et 310 al., 2015). Our findings suggest that habitual mid/forefoot runners reduce VLR when shod 311 compared with barefoot running on a hard surface, but this difference disappears when running 312 313 barefoot whilst cushioning is maintained.

Caution is needed when comparing our VLR results with previous studies. Researchers have used different methods when identifying peak impact force for VLR calculations during mid/forefoot running including: identifying peak impact force at the same, specific point within stance for all trials (Boyer et al., 2014; Rice & Patel, 2017; Samaan et al.; Willy et al., 2008), using the time to peak impact force from other trials in which a peak impact force was visible

(Lieberman et al., 2010), or did not report the complete details of the calculation (Paquette et 319 al., 2013). Like others (e.g. (Au et al., 2018; Warne et al., 2016; Yang et al., 2020)), we used 320 the method of Blackmore et al. (Blackmore et al., 2016) to determine the time of peak vertical 321 impact force from which our VLR was calculated from the original, filtered force platform 322 signal. This method isolates the impact force from the summated vertical GRF waveform, 323 which has been recommended to remove effects of upper body motion on VLR (Gruber et al., 324 325 2017) and is argued to be a robust, data driven method to isolate the impact force when a distinctive peak is not visible. Recent studies found that VLR was not a significant factor 326 327 associated with running injury in collegiate runners regardless of calculation method (Schmida et al., 2021) and three instantaneous VLR calculation methods were statistically similar in 328 rearfoot runners (Ueda et al., 2016). However, the sensitivity of various calculation methods 329 for comparing impact force variables between footfall patterns should be considered in future 330 footfall pattern and barefoot running research. 331

Barefoot running has the greatest effect on ankle joint mechanics, findings which are 332 largely consistent across studies (Hall et al., 2013; Jenkins & Cauthon, 2011; Tam et al., 2014) 333 and generally attributed to changing to a mid/forefoot pattern when barefoot (De Wit et al., 334 2000; Kurz & Stergiou, 2004; Lieberman et al., 2010; Squadrone et al., 2015). In the present 335 study, pairwise differences were only observed for peak dorsiflexion angle, total ankle joint 336 work, and negative ankle joint work. Previous researchers found similar changes with ankle 337 work but, unlike the present study, they found knee and hip work differences between shod and 338 barefoot possibly related to differences in ankle angle at contact (Bonacci et al., 2013; Williams 339 et al., 2012). Greater peak dorsiflexion angle in SHOD versus BF conditions could be related 340 to the shoe elevation and structure (Kerr et al., 2009). Similarly, the smaller lateral heel flare 341 is suggested to minimize frontal plane ankle joint moments, which is a key factor 342 recommending that mid/forefoot runners run in minimalist footwear or barefoot (Davis et al., 343

2017; Rice et al., 2016). However, non-significant differences in joint angles and joint moments
between SHOD and BF+FOAM condition questions the effects of stack height, heel-toe drop,
heel flare, and other footwear features on habituated mid/forefoot running mechanics described
elsewhere (Davis et al., 2017; Lieberman et al., 2010; Rice et al., 2016).

Similarly, footwear structure and cushioning had no effect on frontal plane joint angles. 348 Hall et al. (Hall et al., 2013) in a systematic review identified limited evidence that ankle 349 350 eversion was lower during barefoot running when compared with shod, as did De Witt et al. (De Wit et al., 2000). The role of ankle eversion in injury is poorly understood as this 351 352 mechanism may increase some injuries (Chuter & Janse de Jonge, 2012; Ness et al., 2008), aid in impact absorption and hence reduce the risk of bony injuries (Chuter & Janse de Jonge, 353 2012; Hall et al., 2013; Hreljac et al., 2000), or have no influence (Kuhman et al., 2016; Nielsen 354 et al., 2014). This variable is important because of the proliferation of gait measurement in the 355 prescription of pronation control running shoes. Given that no differences in frontal plane ankle 356 joint angles were observed in the present study, it appears that the difference in cushioning and 357 footwear structure (and subsequent neuromuscular adjustments) may not influence the eversion 358 angle in habituated mid/forefoot runners. 359

The reduced contact time when BF compared with both BF+FOAM and SHOD in this 360 study was consistent with many observations of shorter ground contact times when comparing 361 barefoot and shod running regardless of whether the footfall pattern was controlled (Divert, 362 Baur, et al., 2005; Divert, Mornieux, et al., 2005; Lussiana et al., 2015; McCallion et al., 2014; 363 Paquette et al., 2013; Shih et al., 2013; Squadrone & Gallozzi, 2009). Inconsistent with our 364 findings, two previous studies found contact time to be similar between shod and barefoot 365 running in in habitual mid/forefoot runners (Paquette et al., 2013) and habitual rearfoot runners 366 performing a mid/forefoot pattern (Shih et al., 2013). Our findings suggest that removal of both 367

368 cushioning and footwear structure are required to elicit changes in contact time given that369 contact time was similar between SHOD and BF+FOAM conditions.

A strength of the present study is that we included participants who were already 370 accustomed to a mid/forefoot footfall pattern. Previous studies have examined the effect of 371 acute changes to footwear both with and without instructing footfall pattern, but this method 372 does not account for the complex neuromuscular adaptations that may occur with footfall 373 pattern habituation. For example, making a deliberate, acute switch from a rearfoot to a 374 mid/forefoot pattern or from shod to barefoot may not allow for gradual, more sensitive 375 376 changes to leg stiffness and joint geometry that may be present after long-term habituation. It is also important to note that since the present study controls for footfall pattern, we eliminate 377 the complex interaction of footfall pattern on barefoot versus shod running, and therefore 378 comparisons of the shod and barefoot conditions in the present study must only be considered 379 in those who mid/forefoot strike (who represent a minority of the population (Bertelsen et al., 380 2013; Hanley et al., 2019; Hasegawa et al., 2007; Hébert-Losier et al., 2021; Larson et al., 381 2011)). 382

Another strength of the present study is that a foam EVA running surface was included to minimize any kinematic or kinetic mediated effects of cushioning to isolate the mechanical differences resulting from shoe structure. More studies are needed in this area.

386

387 *Limitations*

A potential limitation of the present study is that participants only had a short time to practice and become accustomed to each condition. However, experienced runners have been observed to adjust leg stiffness in the first step onto different surface conditions (Ferris et al., 1999); thus, the potential influence of the short practice time likely did not have a strong effect on these within-subjects comparisons.

An additional limitation was that the participants were not experienced barefoot runners 393 and only one participant anecdotally reported previous experience with barefoot running. 394 Experienced barefoot runners may have an alternate neuromuscular strategy, although the 395 differences in neuromuscular strategies between experienced and inexperienced barefoot 396 habitual mid/forefoot runners has yet to be catalogued to our knowledge. Indeed, some of our 397 results contrast with previous studies comparing barefoot and shod running in experienced 398 399 barefoot runners (Squadrone & Gallozzi, 2009; Willwacher et al., 2015). However, those previous studies observed changes in ankle angles that could reflect a change in footfall pattern 400 401 or a significant change in strike index that were not observed in the present study. Although all participants were habitual mid/forefoot runners when shod, and the mid/forefoot pattern is 402 frequently observed with barefoot and minimalist footwear running (De Wit et al., 2000; 403 404 Hollander et al., 2017; Kurz & Stergiou, 2004; Lieberman et al., 2010; Squadrone et al., 2015), experience with barefoot or minimalist running does not necessarily equate to also being a 405 mid/forefoot runner when shod (e.g. (Au et al., 2018; Lieberman et al., 2010)). 406

Care should be taken in the inference of this data, given that only mid/forefoot runners were included, and the vast majority of runners are rearfoot across recreational and elite endurance runners (Bertelsen et al., 2013; Hanley et al., 2019; Hasegawa et al., 2007; Hébert-Losier et al., 2021; Larson et al., 2011). Although participants were asked if they have always run with a mid/forefoot pattern versus switching from rearfoot, this information was anecdotal as it was not collected in a formal survey. Those who reported switching from a rearfoot to mid/forefoot had done so at least 12-months prior to data collection.

Due to the more descriptive rather than mechanistic nature of the present study, leg and joint stiffness were not calculated thus the complex interaction of surface/footwear and footfall pattern on stiffness is an area for future research. The lack of significant post hoc differences for frontal plane ankle angle at touch down and peak plantarflexion moment were likely a result of either type 1 error of the main effect or otherwise the conversative Bonferroni correction applied to the analysis. It is important to note that the p-value from an omnibus versus a post-hoc test reflect different questions. Regardless of the reason, given the sample size of N=10 in the present experimental study, we suggest this effect should be explored further in replicated studies for further clarification.

Finally, the present study included a sample size of N=10 because it was exploratory, and no comparable publications were available at the time of study planning for which to base the sample size calculation. The present study provides data that can be used to calculate appropriate sample sizes for future studies.

427

428 Conclusion

The present study is one of the first attempts at elucidating the specific effects of shoe 429 structure and shoe cushioning on barefoot running. Our findings suggest that removal of both 430 cushioning and footwear structure were required to elicit changes in running mechanics when 431 habitually mid/forefoot runners ran barefoot. Conflicting findings with previous research may 432 be related to changes in ankle angle at contact or strike index between barefoot and shod 433 conditions. The few significant differences in ankle mechanics between SHOD and BF+FOAM 434 running conditions and the lack of significant findings for the hip, knee, and other ankle 435 436 variables in habituated mid/forefoot runners questions the effects of footwear structure on running mechanics suggested previously. 437

438

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Figure 1. Vertical (top) and anteroposterior (bottom) ground reaction forces during
running barefoot on the concrete lab floor (BF, black), barefoot on a foam surface
(BF+FOAM, blue), and shod on the concrete lab floor (SHOD, yellow).



662	Figure 2. Sagittal and frontal plane joint moments during running barefoot on the
663	concrete lab floor (BF, black), barefoot on a foam surface (BF+FOAM, blue), and
664	shod on the concrete lab floor (SHOD, yellow). Data includes sagittal hip (1 st row),
665	sagittal knee (2 nd row), sagittal ankle (3 rd row), and frontal ankle (4 th row) internal
666	joint moments. Positive moments indicate hip flexion (FL), knee extension (EX),
667	ankle dorsiflexion (not observed), and ankle inversion (INV). Negative moments
668	indicate hip extension (EXT), knee flexion (FLX), ankle plantarflexion (PF), and
669	ankle eversion (peak eversion magnitudes across subjects were less than < 8 Nm).



Figure 3. Sagittal plane joint power for the hip (top), knee (middle), and ankle
(bottom) during running barefoot on the concrete lab floor (BF, black), barefoot on
a foam surface (BF+FOAM, blue), and shod on the concrete lab floor (SHOD,
yellow). Positive power indicates energy generation and negative power indicates
energy absorption.





Table 1. Descriptive statistics (Mean \pm SD) for contact time, strike index, force platform

692 variables, and joint kinetics for the barefoot (BF), barefoot with foam mats (BF+FOAM), and

693 sl	hod (SHOD)	running c	onditions	(N =	10).
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		BF	BF+FOAM	SHOD		
Ground	Peak active force (N)*,c	1819.45±186.86	1786.19±194.72	1905.01±218.31		
Reaction	Max. instantaneous loading rate $(N \cdot s^{-1})^{*,a}$	91489.20±50538.31	70610.10±30806.01	48518.50±15473.24		
Force, Strike	A-P Max. instantaneous loading rate (N·s ⁻¹)	19946.70±5532.78	20291.50±4496.96	21290.10±3237.45		
Index, Contact	Strike Index (%)	58.95±14.57	54.92±15.57	59.52±11.14		
Time	Contact time (s) ^{*,a,b}	0.215±0.011	$0.224{\pm}0.014$	$0.225 {\pm} 0.013$		
Joint Moments	Hip: peak flexion moment (Nm)	48.14±16.71	45.40±20.32	46.10±23.24		
	Knee: peak extensor moment (Nm)	154.26±47.36	154.79±42.35	160.12±41.58		
	Ankle: peak plantar flexor moment (Nm)*,ns	-213.54±42.45	-208.45 ± 40.43	-227.22±51.24		
	Ankle: peak inversion moment (Nm)	51.74±18.99	57.44±21.14	53.42±18.67		
Joint Work	Hip: positive work (J)	5.24±240	5.96±3.18	5.85±2.46		
	Hip: negative work (J)	-19.40 ± 6.90	-18.26 ± 7.94	-15.23±7.81		
	Hip: total work (J)	-14.15 ± 7.92	-12.30±9.75	-9.38 ± 9.09		
	Knee: positive work (J)	18.75±4.96	18.21±3.78	18.73 ± 6.07		
	Knee: negative work (J)	-27.64±10.99	-28.92 ± 9.67	-27.91 ± 8.89		
	Knee: total work (J)	-8.89 ± 7.62	-10.71±7.47	-9.18±4.10		
	Ankle: positive work (J)	65.87±14.47	64.12±14.33	67.72±21.0		
	Ankle: negative work (J)*,b,c	-44.64±15.21	-38.41±10.18	-58.98 ± 16.92		
	Ankle: total work (J)* ^{a,c}	21.23±10.35	25.71±10.41	8.74±9.34		
694 *: sign	ificant main effect of condition ($P \le 0.05$)					
695 a: sign	a: significant pairwise comparison, SHOD vs. BF ($P \le 0.05$)					
696 b: sign	b: significant pairwise comparison, BF vs. BF+FOAM ($P \le 0.05$)					
697 c: sign	c: significant pairwise comparison, SHOD vs. BF+FOAM ($P \le 0.05$)					
698 ns: no	ns: no significant pairwise comparisons between conditions					
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721	Table 2. The reported main	effect of the repeated measures	ANOVA and descriptive
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statistics for the differences in sagittal and frontal plane kinematics of the ankle, knee, and

hip between barefoot (BF), barefoot with foam mats (BF+FOAM), and shod (SHOD) running

conditions (N = 10). Descriptive statistics are presented in degrees as mean \pm 1 standard

725 deviation. IC = initial contact.

Joint	Variable	Main Effect for Condition	BF	BF+FOAM	SHOD
Hip	peak flexion angle	$F_{(2,18)} = 0.607; P = 0.487; \eta p^2 = 0.06$	27.22±9.33	28.32±7.82	26.87±11.49
	peak adduction angle	$F_{(2,18)} = 1.384; P = 0.276; \eta p^2 = 0.13$	10.23±2.72	10.38±3.30	9.39±3.36
Knee	peak flexion angle	$F_{(2,18)} = 2.385; P = 0.121; \eta p^2 = 0.21$	34.38±5.50	34.58±5.68	35.71±5.95
	peak adduction angle	$F_{(2,18)} = 0.600; P = 0.508; \eta p^2 = 0.06$	1.92±2.62	2.57±2.95	2.31±3.53
	peak abduction angle	$F_{(2,18)} = 0.870; P = 0.393; \eta p^2 = 0.09$	2.18±3.46	1.70±3.64	2.52±4.37
	flexion angle at IC	$F_{(2,18)} = 0.003; P = 0.997; \eta p^2 = 0.00$	8.98±4.41	8.89±3.90	8.94±5.42
Ankle	peak dorsiflexion angle*, ^a	$F_{(2,18)} = 9.480; P = 0.006; \eta p^2 = 0.51$	19.07±4.98	19.34±4.93	22.2±4.08
	peak plantarflexion angle	$F_{(2,18)} = 0.160; P = 0.853; \eta p^2 = 0.02$	23.24±5.31	22.92±4.48	23.43±4.83
	peak eversion	$F_{(2,18)} = 0.534; P = 0.537; \eta p^2 = 0.06$	5.87±2.95	6.59±3.12	6.87±2.10
	sagittal plane plantarflexion angle at IC	$F_{(2,18)} = 0.714; P = 0.450; \eta p^2 = 0.07$	8.48±6.39	6.97±7.39	9.80±9.21
	frontal plane inversion angle at IC*,ns	$F_{(2,18)} = 4.650; P = 0.024; \eta p^2 = 0.34$	8.32±3.42	8.52±4.28	11.44±2.14

727 *: significant main effect of condition ($P \le 0.05$)

728 a: significant pairwise comparison, SHOD vs. BF ($P \le 0.05$)

ns: no significant pairwise comparisons between conditions

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