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Xiulong Bao

Technological University Dublin, xiulong.bao@tudublin.ie

Max Ammann

Technological University Dublin, max.ammann@tudublin.ie

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A Cavity-Backed Spiral Slot Antenna with Wide Axial Ratio Beamwidth for GPS System

X. L. Bao and M. J. Ammann

Abstract—A monofilar spiral slot antenna with a cavity-backed reflector is described. presented, which can achieve the performance of the wide Axial Ratio beamwave for Global Positioning System GPS system. It comprises an arrangement of a single printed spiral slots fed by a 50 Ω microstrip line. By using cavity-backed covering the slot structure, a wide axial ratio beamwidth performance is achieved in the GPS L1 frequency. The angle with less than 3 dB axial ratio at 1.575 GHz in the YoZ plane is about 215 degree. The measured results show that the HPWB beamwidths at 1.575 GHz are 100 degree in the YoZ plane, respectively. The peak gain is 5.5 dBic.

Index Terms—Spiral slot antenna, circular polarization, GPS system, wide beamwidth,

I. INTRODUCTION

In recent decades, circularly-polarized antennas have become more attractive for wireless communication and sensor system applications due to the mitigation of multipath propagation effects as well as reduced antenna orientation constraints. In GPS applications, it is important to have a wide beamwidth in the circularly polarized radiation pattern, in order to achieve a full sky view. To improve the beamwidth for printed patch antennas, some technologies have been reported in the literature [1-6]. One method is to shape the groundplane to improve beamwidth, such as a 3D square ground plane which obtained over 113° [1], a pyramidal groundplane and the partially enclosed flat conducting wall [2] were employed to provide a 130° axial ratio beamwidth, and a folded and drooped groundplane was used to realize over 110° beamwidth [3]. Another method is to extend the substrate to achieve wide dual band beamwidth [4]. Additionally, a combined structure of horizontal bow-tie patches and vertical dipoles was also shown to widen the beamwidth [5]. Furthermore, in order to achieve directional radiation patterns and enhance the antenna gain, microstrip-fed slot antennas with a cavity reflector were reported [6]. But there is no report of wide beamwidth circularly polarized cavity-backed slot antenna the open literature.

In this paper, a monofilar spiral slot antenna is proposed, which has a cavity-backed reflector to suppress the rearward radiation, providing wide 3dB axial ratio beamwidths in both principle planes.

II. ANTENNA GEOMETRY AND CIRCULAR POLARIZATION MECHANISMS

A single spiral slot antenna with a cavity-backed reflector is shown in Figure 1 with the coordinate system and dimensional parameters. The outer and inner radius sequentially increases with movement of the origin point each quarter turn. The starting values are outer radius R_1 and origin O_1 . The second

quadrant has outer radius R_2 and origin O_2 . The 3rd, 4th and 5th quadrants have radii R_3 , R_4 and R_5 with origins O_3 , O_4 and O_1 , respectively. The slot maintains the same width W_1 . The two endpoints of the spiral slot have extended lengths L_1 and L_2 . In order to improve matching for both bands, the microstrip feedline width is stepped using lengths L_{s1} , L_{s2} and widths W_{s1} and W_{s2} as shown in Figure 1. The slot perimeter length corresponds approximately to one guided wavelengths for the operation frequency.

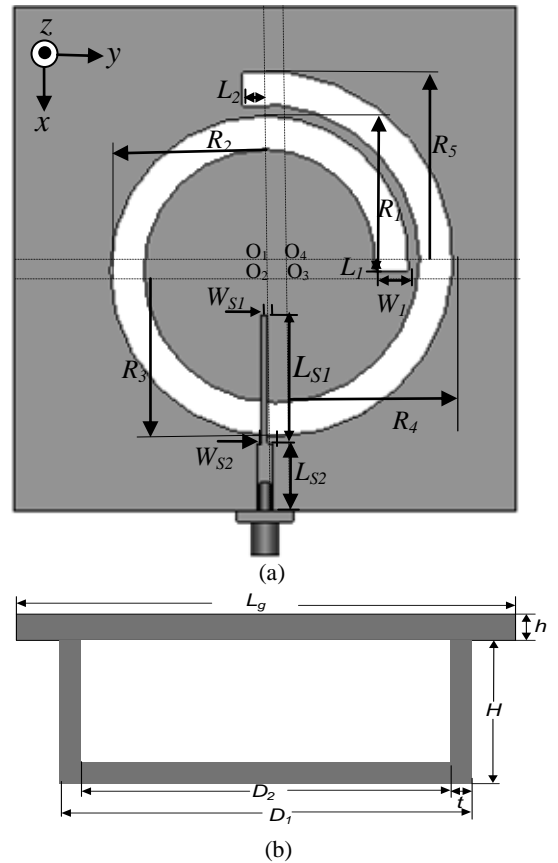


Figure 1 (a) Configuration of the antenna showing spiral slot on the rear of the board and fed by microstrip line on the near side, (b) The profile of the proposed antenna with cavity-backed reflector

In order to investigate the circular-polarization mechanism, the current distributions at 1.575 GHz for four phase values of 0°, 45°, 90° and 135° are shown in Figure 2. It is found that the magnetic current wave travels in an anti-clockwise fashion when viewed from the +Z direction leading to the radiation of a right-hand circularly polarized wave. Thus the polarization sense for the low frequency range is RHCP.

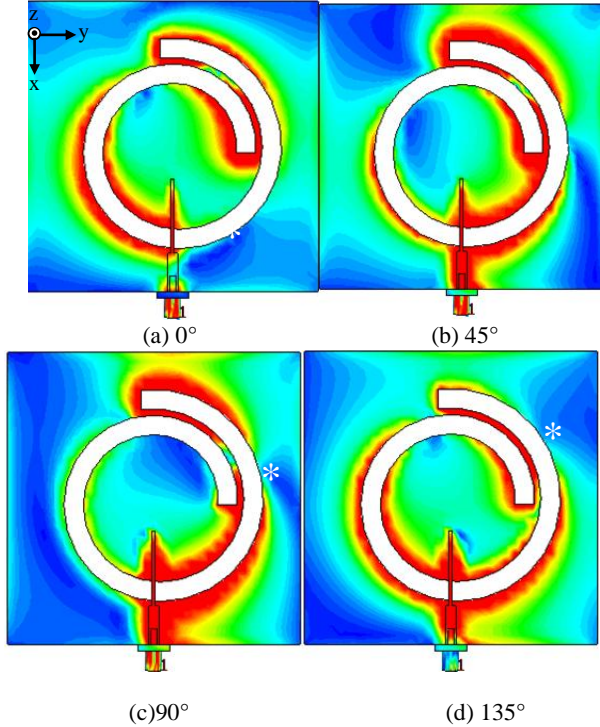


Figure 2. Surface current distributions at 1.575 GHz showing RHCP when viewed from the +Z direction

III. ANALYSIS AND DESIGN OF THE PROPOSED ANTENNA

The single spiral slot is printed on the substrate with $\epsilon_r = 3.5$, $\tan\delta = 0.0018$ and of thickness = 1.57 mm. The groundplane size was chosen to be 90 mm \times 90 mm which is approximately a half of a free space wavelength at the lowest operating frequency. The 50 Ω microstrip feedline ($W_{s2} = 3.0$ mm) is stepped to $W_{s1} = 1$ mm (95 Ω) for good matching to the higher impedance slot. In order to obtain circular polarization, the slot radius is increased to provide the spiral geometry. The origin O_1 is positioned centrally in the board and an origin offset of $O_1O_2 = O_3O_4 = 2$ mm is used. The starting slot radius R_1 is chosen to be approximately 1/8 of a guided wavelength for the lowest frequency. Subsequent radii increase by 2 mm per quarter-circle which was found to provide best axial-ratio and matching.

For the spiral slot antenna, the radiation patterns are dependent on the length of the slot perimeter [7]. Usually, spiral slot antennas radiate axially when the length of the perimeter is between the one and two guided wavelengths. However, it will radiate a tilted beam when the perimeters are greater than two guided wavelengths. In this case, the slot perimeter length approximates one guided wavelength to provide an axial beam. In order to adjust the centre frequency and get the appropriate frequency bands for GPS system, some parameters of antenna, such as the height and diameter of the cavity-backed reflector and the microstrip feedline length L_{s1} are discussed in details.

The parametric study is made using the time domain solver in CST MWS. Other parameters are fixed as follows: $W_{s1} = 1.0$ mm, $W_{s2} = 3.0$ mm, $L_{s2} = 12.0$ mm, $R_1 = 26.0$ mm, $R_2 = 28.0$ mm, $R_3 = 30.0$ mm, $R_4 = 32.0$ mm, $R_5 = 34.0$ mm, $O_1O_2 = O_2O_3 = O_3O_4 = O_1O_4 = 2.0$ mm, $L_1 = 2$ mm, $L_2 = 4$ mm, $W_l = 6$ mm, $L_g = 90$ mm, $h = 1.57$ mm, $t = 3$ mm.

The height of the cavity-backed reflector have affected on the S_{11} and axial ratio curves. Figure 3 and Figure 4 show the centre frequency to increase as the height of the cavity-backed reflector decreases.

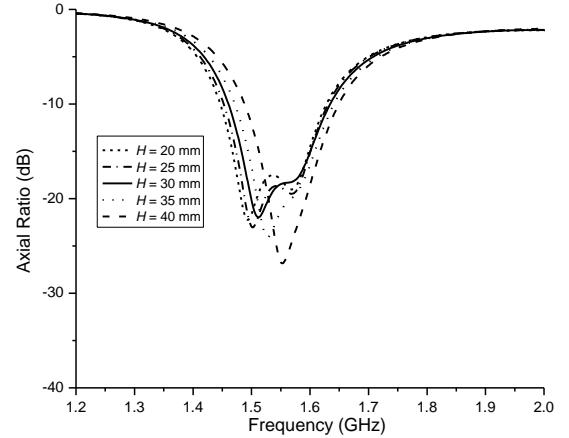


Figure 3. The simulated S_{11} for different heights of the cavity-backed reflector ($L_{s1} = 21$ mm, $D_l = 38$ mm)

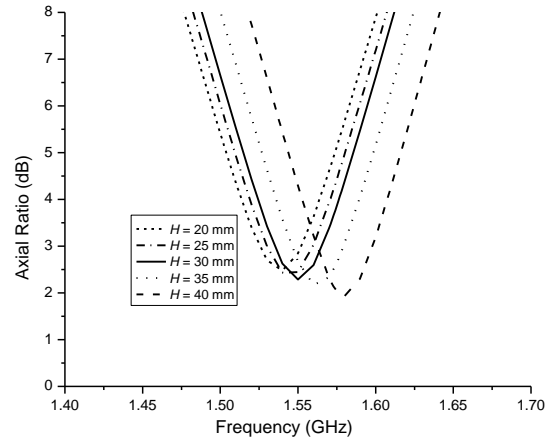


Figure 4. The simulated axial ratio for different heights of the cavity-backed reflector ($L_{s1} = 21$ mm, $D_l = 38$ mm)

Figure 5 illustrates the S_{11} for different values of microstrip feedline coupling length L_{s1} . By increasing the coupling length, the frequency of the lower band is shifted downwards. The sensitivity of matching to the line length is seen in Figure 5. But for axial ratio curves, there is little effect with different microstrip feedline length L_{s1} , as shown in Figure 6.

Figure 7 and Figure 8 display the S_{11} and axial ratio for different diameters of cavity-backed reflector, respectively. It is found that the working frequencies is shifted downwards as the diameter of the cavity-backed reflector is increased.

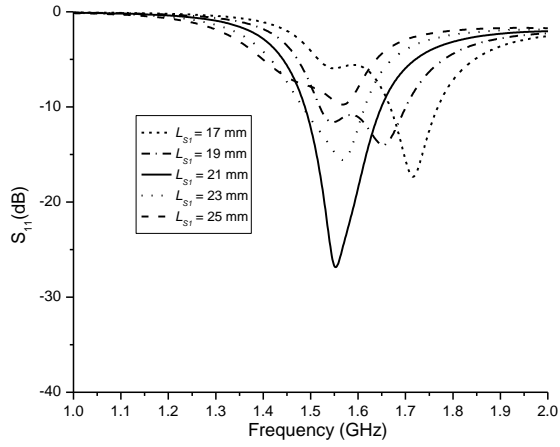


Figure 5. The simulated S_{11} for different L_{SI} ($H=30$ mm, $D_I=38$ mm)

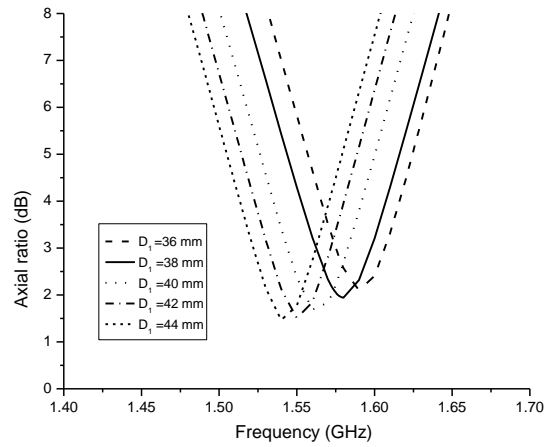


Figure 8. The simulated axial ratio for different diameters of the cavity-backed reflector ($H=30$ mm, $L_{SI}=21$ mm)

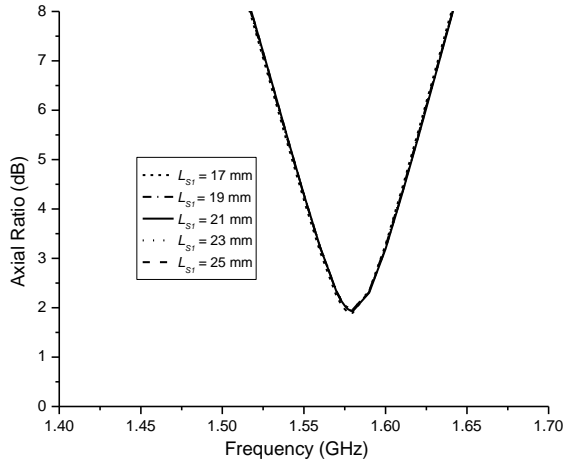


Figure 6. The simulated axial ratio for different L_{SI} ($H=30$ mm, $D_I=38$ mm)

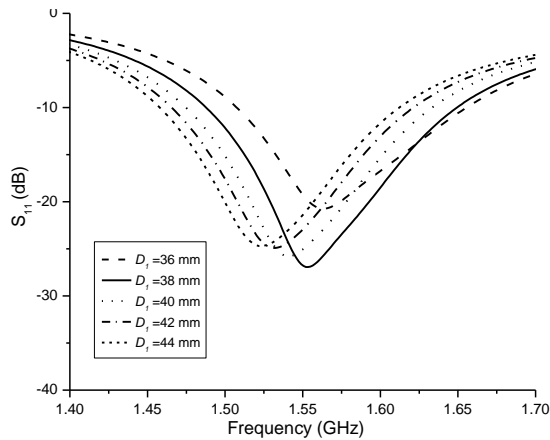


Figure 7. The simulated S_{11} for different diameters of the cavity-backed reflector ($L_{SI}=21$ mm, $H=30$ mm)

IV. NUMERICAL RESULTS

The proposed spiral slot antenna was prototyped and tested. The selected dimensions of the antenna parameters are listed as: $W_{S1}=1.0$ mm, $W_{S2}=3.0$ mm, $L_{S1}=21.0$ mm, $L_{S2}=12.0$ mm, $R_1=26.0$ mm, $R_2=28.0$ mm, $R_3=30.0$ mm, $R_4=32.0$ mm, $R_5=34.0$ mm, $O_1O_2=O_2O_3=O_3O_4=O_1O_4=2.0$ mm, $L_1=2$ mm, $L_2=4$ mm, $W_l=6$ mm, $L_g=90$ mm, $H=30$ mm, $h=1.57$ mm, $t=3$ mm, $D_I=38$ mm. Figure 9 and Figure 10 show the simulated and measured S_{11} and axial ratio, respectively. The measured results show the S_{11} to be less than -10 dB for approx. 120 MHz from 1.50 GHz to 1.62 GHz. The 3 dB axial ratio bandwidth is 68MHz (4.3%) (1.541 GHz to 1.609 GHz). The 3dB axial ratio beamwidths are shown in Figure 11 at 1.570 GHz, 1.575 GHz, 1.580 GHz, respectively. It is noted that axial ratio is less than 3 dB for 215° in the YoZ plane and 100° in the XoZ plane at 1.575 GHz, as shown in Figure 12.

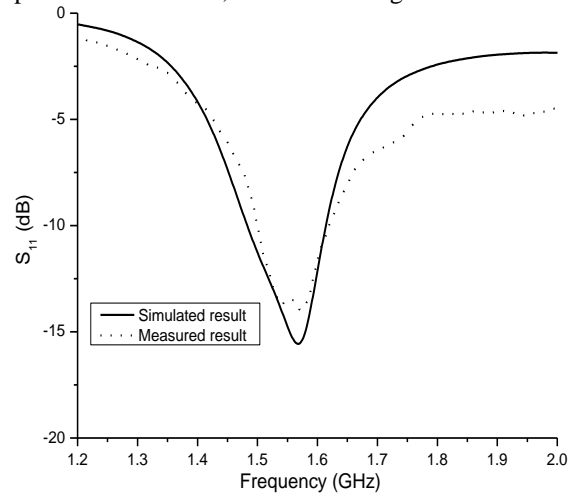


Figure 9. Comparison of the simulated and measured S_{11}

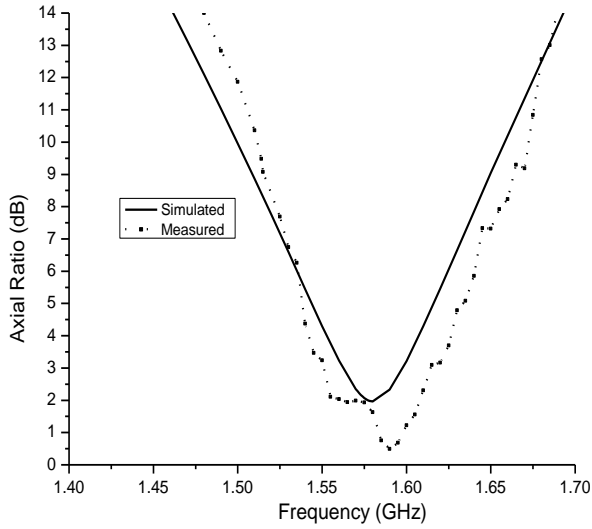


Figure 10. Comparison of the simulated and measured axial ratio

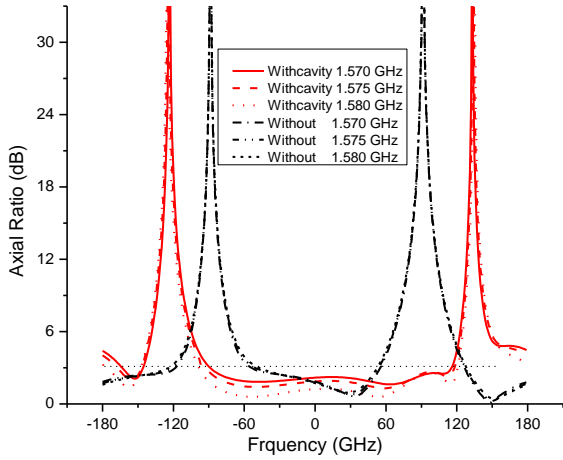


Figure 11. Simulated axial ratio in the YoZ plane with cavity reflector and without cavity reflector

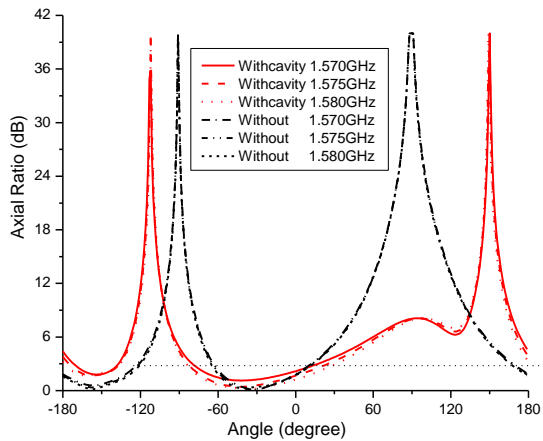


Figure 12. Simulated axial ratio in the XoZ plane with cavity reflector and without cavity reflector

Figure 13 and Figure 14 show the measured and simulated radiation patterns at 1.575 GHz. It is found that there are about

215° and 100° half power beamwidth (HPBW) in the YoZ plane and XoZ plane, respectively. The measured peak gain at 1.575 GHz is 5.5 dBic.

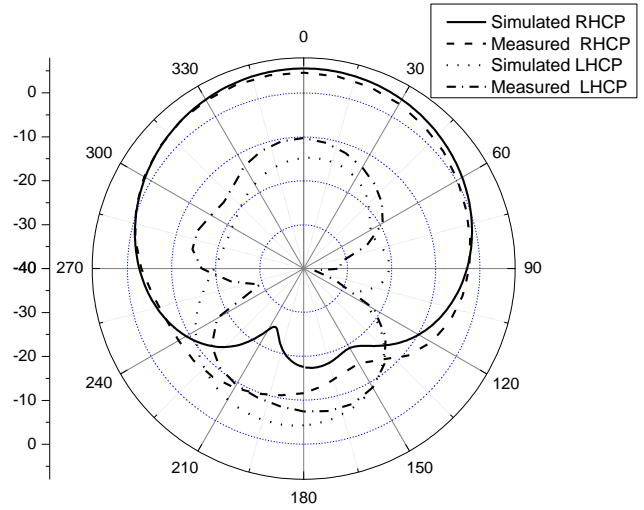


Figure 13. Simulated and measured radiation patterns at 1.575 GHz in the YoZ plane

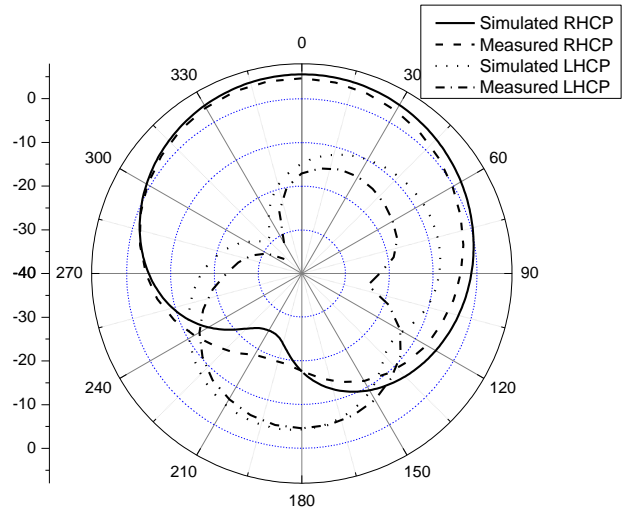


Figure 14. Simulated and measured radiation patterns at 1.575 GHz in the XoZ plane

V. CONCLUSION

A novel circularly-polarized spiral slot antenna for GPS system was modeled, fabricated and tested. The proposed antenna is composed of a spiral slot cavity-backed a reflector and fed by a 50 Ω microstrip line. The proposed antenna can achieve right-hand circular polarization with an axial ratio beamwidth of 215°. Its peak gain is 5.5 dBic at 1.575GHz.

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