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## Breaking the Mould 2 : An analysis of single-leaf insulation upgrades

Joseph Little

Technological University Dublin, joseph.little@tudublin.ie

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# Breaki ng the Moul d 2



## An analysis of Single-Leaf Insulation Upgrades

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By

**[Author name]**

BArch, MRIA, MÉASCA, MSc Archit.

Advanced Environmental + Energy Studies  
(Hons)



### Introduction

This article is the second in a series looking at thermal upgrades to single-leaf walls of existing houses. It compares a range of ways of upgrading masonry single-leaf walls, particularly the ubiquitous hollow block wall, and the impact of those decisions on moisture content, wind- and airtightness, cost and heating. Future articles will look at various dry-lining approaches for a range of walls including brick walls of various widths.

### A German study of moisture and insulation in single leaf brick walls

In 1998 Doctor Hartwig Künzel <sup>1</sup> of the Fraunhofer Institute in Germany had an excellent paper published on what effects the moisture content of walls. He was particularly focused on single leaf walls (or 'massive') walls and how to upgrade them. He recognised that many brick building of architectural or cultural significance can't be overclad or rendered to reduce the effect of wind-driven rain.

*"Massive walls exposed to the natural climate without special rain protection show a dynamic moisture equilibrium governed by the alternate events of rain and sunshine. The moisture further reduces the rather low insulation level of the wall."*

The paper used the WUFI simulation software for a number of tests but also validated some of these with field tests showing good agreement. He looked first at a brick wall, that had previously been dry-lined in a range of ways, starting the measurements just after its outer surface had been impregnated (to protect against driving-rain)<sup>2</sup>, and then studied an equivalent wall with two types of external insulation. His conclusions were:

*"... that an exterior insulation leads to the drying of the wall, with the drying rate depending on the vapour permeability of the insulation system. An interior insulation, however, results in a rising water content of the wall due to the decreasing masonry temperature... Therefore the interior insulation of exposed walls should be combined with rain protection measures at the facade."*

This author came to similar conclusion in a new study of hollow blocks walls discussed below, see Figure 4 below. Dr. Künzel did not specify which 'siloxane' compound he was referring to in his test but 'Thompson's Water Seal' and various products from 'Igoe International' should give a similar effect. Careful specification from an accredited conservation consultant is advisable.

<sup>1</sup> Künzel, H.M., 'Effect of interior and exterior insulation on the hygrothermal behaviour of exposed walls', *Materials and Structures*, Vol. 31 (March 1998), pp 99-103

<sup>2</sup> The rain protection used is a particular siloxane compound.

## Dry-lining

The solid line in Figure 01, representing the protected but un-insulated brick wall, drops steeply from a high moisture content in the first year (10%) and reaches equilibrium at about 0.8% mid-way through the second year<sup>3</sup>. The relative speed of this is because vapour can escape out of the wall in two directions and the additional impact of rainwater ingress has been minimised. All the other lines show how dry-lining inhibits the drying-out of single-leaf walls.

The dotted line represents the effect of the insulating plaster (a thick lime plaster with embedded expanded polystyrene beads), the short dashed line is the effect of fibrous mineral wool dry-lining and the long-dashed line is for expanded polystyrene board dry-lining. Each is 60mm thick. In this study no vapour barrier or vapour control layer was

through and absorbs almost nothing. The insulating plaster can also absorb & release but in vapour terms will behave more like an extension of the wall itself.

Alternate examples to the insulating plaster which are gaining popularity for use in historic buildings are thick clay plasters and hemp-lime biocomposite plaster. Both are typically applied ~35mm thick. Ecological Building Systems of Athboy supply the first and Hempire of Clones the second. **Both should only be applied to walls that have already been cared for and are dry.**

In masonry buildings of all ages designing for a drier wall (which will consequently have a lower conductivity) with an appropriate dry-lining buildup is a better goal than focusing only on high-performing insulants, without regard for the masonry's current or future moisture content, dew point, mould potential etc. In historic buildings the best approach is to accept a modest improvement at the walls but to seek the biggest increases in energy efficiency in the attic, the heating system, thermal bridging around sliding sash windows and air infiltration.

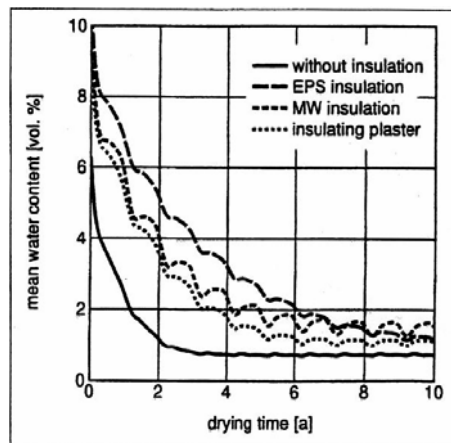
## Externally insulating

Like the compound used to impregnate the brick wall before the dry-lining study, the external insulation blocks the driving rain and creates a wind-tight seal. Because it also makes the wall warmer and leaves its inner (plastered) surface unclad it gives the masonry the best chance to dry out. The question then becomes which insulant allows this happen quicker. Again the fibrous insulant scores highest. While both build-ups are non-hygroscopic, its fibrous structure and mineral render surface allow better vapour diffusion than the expanded polystyrene with an acrylic finish. Interestingly Doctor Künzel found little difference in the drying time of different thicknesses. He suggested this might be because thicker, and therefore less diffuse, insulation also made the wall warmer.

FIGURE 1

The drying-out behavior (in years) of un-rendered brick walls without and with different types of interior insulation from the month that the outer surface of the brick had been impregnated to protect against driving rain onwards.

Source: Künzel '98



used. While the polystyrene has the highest U-value this wall also takes the longest to dry-out (10 years). The plaster takes 6 years and the mineral wool seven. The slower times relate directly to the varying abilities of the insulants to allow vapour move through them into the room. The polystyrene used was 23-times more resistant to vapour diffusion than the mineral wool.

The oscillations in the lines are due to higher quantities of moisture moving into the wall from inside each winter but being able to dry out in both directions each summer. The oscillations are most extreme for the fibrous insulant. This is because it can absorb and release higher quantities of moisture<sup>4</sup> while

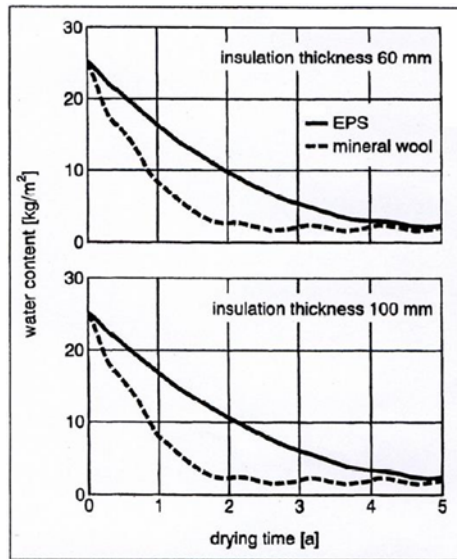
<sup>3</sup> The German standards regard 1.5% as a normal moisture content of factory-delivered bricks, so this level of drying-out is very healthy.

<sup>4</sup> Too much moisture and the mineral wool will collapse, whereas a natural fibrous insulant such

as hempwool, sheep's wool or a woodfibre batt will withstand far higher quantities.

FIGURE 2

The drying-out time (in years) of two different types and thicknesses of external wall insulation  
 Source: Künzel '98



wall upgrades using 'Therm 5.2'. To our knowledge this is the first study to look at hollow blocks in this way, showing as it does the impact of geometry and insulation position on Drawing A1 of Figure 3 shows a typical uninsulated hollow block wall, plastered on the inside and rendered on the outside. B1 shows the same wall after it has been filled with cavity foam insulation. C1 shows an alternative approach with a dry-lining system 5 and D1 shows the original wall externally insulated 6. In all cases the original plaster and render are shown left in place 7. Figure 4 shows the thermal impact of these upgrades with 'isotherms', lines or colours represent areas of the same temperature. In Figure 5 the tiny back arrows and colours now represent the rate of energy flow. Note that in this case the blue colour, for instance, means slower energy flow, not a cooler temperature.

Bear in mind an external insulation system needn't have an Irish Agrément Board (IAB) certificate but should have the equivalent European CE mark (passed for use by the NSAI), and be carried out by a trained installer with good track record. Current favourites of this author are the 'Brillux' expanded polystyrene system from Greenspan, and wood fibre

In all cases of this test the outside temperature is 0°C and the room is heated to 20°C. The light red colour in detail A2 shows the wall surface is 4.5 degrees cooler than the room air temperature, the yellow colour coming to the surface at the corner is 7.5°C cooler. If a body of air loses half its moisture content every drop of ~11°C it is no surprise that this area will be a prime spot for damp. It will be necessary for

FIGURE 3, 4 & 5

Figures 3 - 5: Analysis of the corner of a hollow block wall viewed in plan

Insulation location in hollow block walls

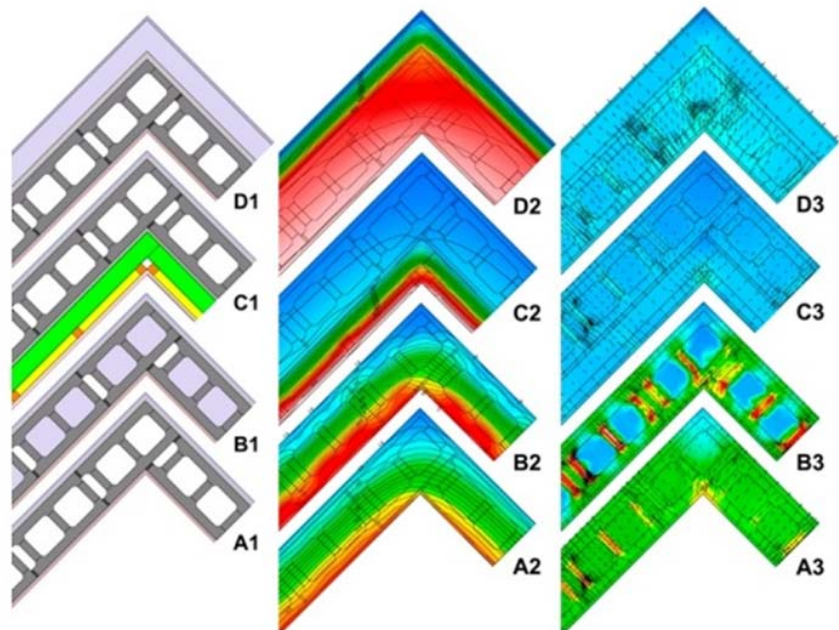


Figure 3: upgrade options flux

Figure 4: Resulting isotherms

Figure 5: Resulting energy flux

insulation systems from NBT (agents Econstruction and Lochplace) and Ecological Building Systems: 'Diffutherm' and 'Gutex' respectively. Much of Doctor Künzel's work is borne out by this study of hollow block

<sup>5</sup> The dry-lining system shown has woodfibre insulation boards fixed to the original plastered wall, an airtightness membrane, a services zone filled with hempwool, then plasterboard.  
<sup>6</sup> A system with expanded polystyrene is shown here.  
<sup>7</sup> Note only one or two external wall insulation systems can clad over pebbledash, others need the dash removed first.

constant warm convection currents within the room to keep mould away here. This is why mould often shows first in a corner cupboard or behind a bed pressed to the wall. Walking past any part of this wall a sensitive occupant will be aware of radiating more heat to the wall than s/he receives back: they will sense its coldness without needing to touch. B2 shows the thermal effect of filling the linked hollows. Note that the computer software fills every single crevice of the blocks' hollows. This will not happen in reality. As a nod to reality we haven't filled the smaller hollows which would be hard to locate with a drill.<sup>8</sup> The more undulating shape of the isotherms at the wall surface now reflects the greater difference in thermal performance at the connecting concrete webs compared to the filled hollows. Normal surface temperature registers as varying between 2.5 – 3.0°C, and the corner 6°C, cooler than room temperature. A long way from ideal.

The author suspects much of the improvement people note after getting the hollows filled is actually down to a reduction in infiltration (i.e. air leakage) of this dreadful form of construction.

Moving to the dry-lined and externally insulated walls we can see that the red colour is now continuous. The white colour (a thin line in C2 and a larger area in D2) shows that the surface of the wall is now room temperature, only the very tip of the corner is 1.0°C cooler. An occupant passing by may be aware of thermal equilibrium: that is of radiating as much heat to the wall as s/he receives back.

What is fascinating is that it is now graphically very clear what Doctor Kunzel was saying: external wall insulation aids the drying out of masonry, whilst dry-lining makes them uniformly colder and over time wet. In the external wall insulation the coldest portion of the wall is consigned to the outer few millimetres of insulation and render. Bear in mind that if the source of heat is fully extinguished during a cold spell (due perhaps to the boiler being shut down due to a winter trip abroad and little solar gain) the owner of

the externally insulated wall will know just how much thermal mass s/he has. It will take a long time to heat up while the dry-lined house will respond much quicker.

### Energy Flux in hollow block walls

Thermal transmittance, known as U-value (W/m<sup>2</sup>K), is the rate of energy flow per degree Kelvin through a portion of building fabric. A faster energy flow or flux (W/m<sup>2</sup>) will contribute to a larger U-value and poorer performance, at least locally<sup>9</sup>.

It is clear A3 of Figure 5 above exhibits faster energy flux along its thin concrete webs than through the air gaps or the rest of the concrete. As concrete blocks are highly porous water vapour will be drawn quickly along these narrow paths. What is fascinating is that B3, featuring insulated hollows, is far, far worse. In some places within 25mm the rate of energy flux changes by a factor of four (~20 W/m<sup>2</sup> to ~80 W/m<sup>2</sup>). The best illustration of how different the concrete webs now act compared to the concrete faces on either side might be to imagine that they have changed to another material entirely with quite different properties (i.e. faster energy and thus moisture transfer).

A Lucan-based client of this practice reported coming home to just such a hollow block wall after two weeks of no heat in Winter (a year after filling the hollows). He found his south-east facing stairwell wall covered in black mould. Warm convection currents usually kept the 'dew point' in the middle of the wall prior to the change. Now due to a combination of factors including (a) higher energy flux within filled blocks, (b) a week or two of lower temperatures inside the house, and (c) perhaps south-easterly winds with driving rain, a dramatic increase in the room surface's moisture content resulted. The fact that the centre of the wall now had a reduced ability to dry out via the linked hollows must have further exacerbated the problem.

This all changes in C3 and D3: they both look rather uneventful! Essentially energy flux is quite uniform and fairly slow, somewhere between 0 and 20 W/m<sup>2</sup>. Another sign of a better, more predictable form of insulation upgrade. In summary it must be evident to the reader that the condition shown in A2 and A3 is unpleasant and should be improved upon for

<sup>8</sup> The Author can't help but shudder at the idea of an insulation installer riddling the 40mm thick concrete outer face of the hollow block wall with a close matrix of drilled holes. Imagine parts of the rear portion of that face spalling away under the action of the drill thereby weakening these thin structures further. No homeowner could want that.

<sup>9</sup> Blue here represents 0 – 20 W/m<sup>2</sup>, green: 20 – 40, yellow: 40 – 60, red: 60 - 80 and white: 80 – 100 W/m<sup>2</sup>.



the health and wealth of the occupants. There are many acceptable forms of dry-lining and external wall insulation to remedy the situation (see C2, C3, D2, D3) but on no account should a homeowner settle for filling the linked hollows (see B3 or B2). If they do they are engaging in an unpredictable, unhealthy and possibly even structurally unstable experiment: buyer beware.

### Further penetrations

What is missing in the study above (see A3) is the additional impact of the vertical air flow within the linked hollows of uninsulated blocks. As a basic law of science warm air will rise if allowed to do so. It is therefore inevitable that, even in a hollow block wall that was made totally wind-tight, air would rise within vertically-linked hollows to be replaced by cooler air dropping down. This effect, known as 'thermal looping', was written about some years ago in 'Construct Ireland' magazine in relation to reduced performance in the insulation of partially-filled cavity walls.

floor room) and at its top (in a first floor room). This could be repeated on more than one external wall or house. Bear in mind if it happens in an uninsulated hollow block wall it will also occur in a dry-lined one, it just won't be as easy to capture with a thermal imaging camera (as details A3 and C3 of Figure 5 prove).

This effect of 'thermal looping' on thermal performance is compounded if external air, often of lower temperatures and higher humidity levels, can enter into this network of linked hollows. There are at least four reasons as to why this might occur:

1. Standard concrete blocks, even 100mm solid blocks, are not airtight as they are highly porous. The author has felt air passage through the middle of a block at first hand in an airtightness test.
2. A wall made of hollow blocks, the latter having an outer concrete face only 40mm wide connected by variable amounts of mortar and

FIGURE 6 & 7

Pictures of utility box recesses in a hollow block wall



Thermal Transmittance calculations ( $W/m^2K$ ) of walls are based on a steady horizontal heat flow from inside to outside. If this 'thermal looping' component is added the heat flow rate must surely accelerate, for the downstairs rooms at least. The result being poorer thermal performance, higher heating bills. The Author would be interested if anyone with a thermal-imaging camera could capture this effect by photographing the external walls of an uninsulated hollow block house *from the inside*, ideally on a cold day with the heating turned up (to accentuate the differences). Ideally the same stretch of external wall would be photographed at its base (in the ground

covered by a variable amount of render, is going to be hard to make wind-tight even if done with care.

3. These buildings were built at a time when there was no awareness of the issues of wind-tightness on the outside and airtightness on the inside: as the saying goes you can only solve a problem if you know it exists.
4. Penetrations through the outer face, including 'hole-in-the-wall' vents, inset telcon or gas-supply boxes, power or telephone cables, and eaves junction are highly likely to introduce external air. See Figures 6

and 7 below. The pictures were taken on a typical Co. Kildare housing estate, built in 2004. Figure 6 shows the recesses made for utility boxes and even an additional chasing route marked out for later cutting. Figure 7 shows how easy it will be for future air paths to go from outside to inside or rise through the linked hollows. How the wall manages to stay upright is an entirely different question!

The thermal imaging enthusiast mentioned earlier could widen his/her study to include the area of wall above a utility box penetration and below a timber or PVC fascia and soffit. If these items are present it might indicate a more recently-built wall which is also likely to be dry-lined.

What is interesting is that the choice of thermal upgrade can have a direct impact on the wind-tightness of an existing wall. External wall insulation, see D1 of Figure 3, can close the infiltration routes listed in items (a), (b) and (c) above with its insulation slabs, proprietary high performance render and wind-tightness detailing. A good system is designed to be wind-tight. To see a similar improvement with a dry-lining-focused thermal upgrade (see C1 of Figure 3) it would be necessary to examine each possible point of air ingress and apply an appropriate seal that would affect the outer 40mm wide face: no easy task.

However to get the most benefit the various pathways described in item (d) above also need to be addressed. For instance the wind-tightness of the eaves-wall junction could be examined and upgraded during a routine replacement of fascia and soffit boards, and the utility boxes could be moved to an adjacent blockwork wall or structure. Recent quality housing developments incorporated this 'utility wall' as part of a raised planter or a bin store and looked very well. As such a feature is easy to incorporate during the construction period and has a clear positive impact (in terms of wind-tightness) the Construction Industry Federation should insist its members adopt this approach for all new housing. The 'solution' shown in the photographs above cannot be allowed to continue. Unfortunately for those who

have houses with utility boxes so mounted it's an awkward thing to put right requiring removal of the box and the sealing of the surrounding masonry and pipe ingress points before its replacement. The quick-fix solution of spraying expanding foam into the holes to rear of the box may give an improvement but for how long?

#### Making the right choice

For those with brick external walls of historic or aesthetic value intent on dry-lining first examine the pointing of the mortar joints and see if repair is needed. If it is, make sure you use the right mortar. Check that no downpipes are leaking resulting in localised increases in moisture content. Repairing lime mortar with cement will exacerbate the damage to the bricks and water ingress. Next consider a tested, approved impregnation system that reduces water ingress without reducing vapour diffusion. Both are specialist jobs. Only after this has been completed (at least a few months) apply the dry-lining.

On no account have the linked hollows of a hollow block wall filled!

It must be clear at this point that the Author strongly recommends upgrading houses with hollow block walls with a proprietary external wall insulation system. Fibrous insulants with mineral render coats will allow better vapour diffusion than other systems, but any proprietary external wall insulation system should out-perform dry-lining a hollow block house given the many shortcomings of hollow block construction.

Financial cost is always an issue in Irish construction projects and can only increase in significance in the current straitened circumstances. This is only right, but our plea to homeowners embarking on an energy-efficient upgrade is that they would give greatest weight to long-term value, long-term costs and long-term benefits. A great example of this can be seen in the comparison of dry-lining and external wall insulation. Most forms of dry-lining are cheaper to install on 'day 1', per square metre of prepared surface, than external wall insulation. While this

article has discussed in detail hidden long-term costs that must be considered, such as the dependability of the thermal upgrade, mould potential etc, there are also other hidden financial costs.

Dry-lining requires that occupants move out and rent or stay elsewhere, that they put furniture and paintings etc in storage (even if still on site) and re-decorate after. External wall insulation on the other hand requires that scaffolding be erected (some external wall insulation installers do this: some leave it to the general builder). For a proper installation with minimum thermal bridging, windows should be unfixed and moved to the outside line of the original wall, drainpipes should also be moved out, roof eave fascias need adapting and any concrete paving surrounding the house should be cut back to ensure the insulation clads the full height of the relevant external walls. This may sound expensive, but that view may be countered by the shorter construction time, the fact that the occupants can often remain resident, and the fact that the only re-decoration needed inside is the cladding of the widened internal window reveals with timber liner boards. However the final, and perhaps most persuasive hidden cost in this comparison, may be the remaining size of the house.

Take a typical Dublin 3-bed semi-detached house with hollow block walls, a floor area of ~100m<sup>2</sup> and overall internal dimensions of 10m x 5m. It has an external wall perimeter of 20m per floor, giving 40m over two floors. This excludes the party wall of course. Assume the external walls are built of hollow block with sand-cement internal plaster and pebbledash outside. A best practice, healthy approach to dry-lining these walls (to achieve the 0.27 U-value target of the 'Home Energy Saving' scheme) would be to use 80mm of 'Warmcell 100' or equivalent blown cellulose insulation ( $\lambda$ -value of 0.035), continuously sealed with an intelligent vapour control layer (to surrounding structure), and a 38mm service zone filled with hemp or sheep's wool with a plasterboard finish. This buildup can be 130mm thick. The floor area lost would be 40m x 0.13m = 5.2 m<sup>2</sup> of lost floor area, which converts to (5.2 x 10.76 =) 56 ft<sup>2</sup>. Assuming a conservative

average value of €250 per ft<sup>2</sup> for residential floor space (the value could be double this in certain parts of the city) means that this 'lost' floor area has a value of €13,988.<sup>10</sup>

Where the discussion is about insulating inside or outside the deciding question could be 'can we afford to lose further value by losing space in a market already falling?' An alternate response to this news, wherein the thinnest or cheapest dry-lining is selected, would be a mistake if those installations have dubious credentials, don't allow a proper airtight installation, or result in poor thermal bridging or health. As with almost anything it is better to do a little work well than a lot badly.

One caveat: external wall insulation may not always suit a household with low daytime occupancy. Dry-lining makes a building thermally 'lightweight' and will result in a quicker heating time which could suit a family of commuters. Externally insulating leaves the original thermally 'heavyweight' structure exposed to the inside. The best way to heat 'heavyweight' structures is to supply constant low-level heat to them. This can be from the free heat of the sun (through good orientation and appropriately-sized windows) and a low temperature radiant heating system, such as can be supplied by under-floor heating or skirting radiators. Remember 'heavyweight' building fabric can store cold just as well as warmth...

Finally the right thermal upgrade and heating system are those that suit your specific lifestyle and your house's construction while safeguarding health and the greater Environment on into the future.

<sup>10</sup> The Author is grateful to Jay Stuart of DWME Ecoco for persuading him over a cool draught beer that the financial impact of lost space needed to be highlighted here.