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# Stochastic Hybrid Embodied CO2-eq Analysis: an Application to the Irish Apartment Building Sector

Adolf Acquaye Technological University Dublin, adolf.acquaye@tudublin.ie

Aidan Duffy Technological University Dublin, aidan.duffy@tudublin.ie

Biswajit Basu Trinity College Dublin, basub@tcd.ie

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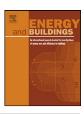
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# Stochastic hybrid embodied CO<sub>2</sub>-eq analysis: An application to the Irish apartment building sector

## Adolf A. Acquaye<sup>a</sup>, Aidan P. Duffy<sup>a,\*</sup>, Biswajit Basu<sup>b</sup>

<sup>a</sup> School of Civil and Building Services Engineering and Dublin Energy Lab, Dublin Institute of Technology, Ireland <sup>b</sup> Department of Civil, Structural and Environmental Engineering, Trinity College, Dublin 2, Ireland

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## ABSTRACT

The development of embodied CO<sub>2</sub>-eq analysis has progressed significantly in recent years and has become a mainstream practice in many industries as evidenced by the development of the ISO 14040 and 14044 life cycle assessment (LCA) standards. However, it is recognized that due to weaknesses in gathering data on product-related emissions, embodied CO<sub>2</sub>-eq values are probabilistic. This paper therefore presents a stochastic analysis of hybrid embodied CO<sub>2</sub>-eq values are probabilistic. This weakness in traditional methods and, by way of example, applies it to an Irish construction-sector case study. Using seven apartment buildings, 70,000 results are simulated with Monte Carlo analysis and used to derive probabilistic and cumulative embodied CO<sub>2</sub>-eq intensity distributions for apartment buildings in Ireland. A Wakeby distribution with known statistical parameters and uncertainty was derived for the average embodied CO<sub>2</sub>-eq intensity of apartment buildings in Ireland. The mean hybrid embodied CO<sub>2</sub>-eq (ECO<sub>2</sub>eq)-intensity was estimated to be 1636 gCO<sub>2</sub>-eq/ $\in$  with an uncertainty of 73 gCO<sub>2</sub>-eq/ $\in$ . The stochastic analysis helps to account for variability in input variables into LCA and embodied energy and CO<sub>2</sub>-eq analysis. The application of the stochastic embodied CO<sub>2</sub>-eq analysis as demonstrated in this study can be extended to other building sectors and countries and can form the basis for the development of evidencebased policy formulation since it provides greater information of embodied CO<sub>2</sub>-eq intensities of building than deterministic approaches.

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## 21 **1. Introduction**

Greenhouse gas (GHG) mitigation is now a central policy of 22 almost all developed economies. Because buildings account for 23 approximately 40–50% of total emissions in these countries [1,2] 24 such policies focus on emissions' reductions from the built environ-25 ment through measures such as promoting energy efficiency and 26 the deployment of renewable energy supply (RES) technologies. 27 These measures, however, fail to address the increasingly impor-28 tant role that embodied energy (the energy required to produce 29 a building) plays in building-related emissions, which can repre-30 sent as much as 40% of life cycle emissions for residential buildings 31 [3].

Scheckels [4] define the embodied energy of a building as the energy consumed by all the process associated with its production. The embodied  $CO_2$ -eq of a building can therefore be defined as the equivalent carbon dioxide ( $CO_2$ -eq) gas emitted into the atmosphere as a result of all the associated energy used in the production of that building. Equivalent carbon dioxide ( $CO_2$ -eq) represents the

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most important anthropogenic energy-related greenhouse gases (GHGs) with the highest environmental impacts. These are: carbon dioxide –  $CO_2$ ; nitrous oxide –  $N_2O$ ; and methane –  $CH_4$  [5]. These emissions are associated with the initial phase of a building's life cycle, preceding emissions resulting from operational energy use and energy used in demolition and recycling.

It is recognized that operational energy analysis has dominated building energy research for many years when compared to embodied energy analysis. It has been shown however, that the energy embodied in buildings is significant when compared to its operational energy use. For example, Yohanis et al. [6] showed that energy initially embodied in a single-storey office building could be as much as 67% of its operating energy over a 25-year period. Moreover, research carried out by the Commonwealth Scientific and Industrial Research Organisation [7] also shows that embodied energy of a building is a significant multiple of the annual operating energy consumed, ranging from around 10 times for typical dwellings to over 30 times for office buildings. It is also a well established fact that as buildings become more operationally energy efficient, the embodied energy to operational energy ratio increases. Embodied energy and emissions are therefore likely to account for an increasingly large proportion of building-related life cycle CO<sub>2</sub>-eq emissions in the future.

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<sup>\*</sup> Corresponding author. Tel.: +353 14023940; fax: +353 14023720. *E-mail address*: aidan.duffy@dit.ie (A.P. Duffy).

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The importance of embodied energy and embodied CO<sub>2</sub>-eq analysis should therefore not be underestimated when assessing life cycle energy requirements, resource depletion and related environmental impacts.

The development of embodied CO<sub>2</sub>-eq analysis and life cycle assessment (LCA) has progressed significantly in recent years, and LCA has become a mainstream practice in many industries as evidenced by the development of the ISO 14040 and 14044 Life Cycle Assessment Environmental Standards. However, it is recognized that due to weaknesses in gathering data on product-related energy use and emissions, embodied energy values are probabilistic [8,9]. For example: designers and contractors are currently unable to obtain embodied emissions in the products they employ (apart from in exceptional circumstances); and the use of sectoral emissions intensities (derived using input-output (I-O) techniques) to estimate emissions for a particular product or process is normal practice, although the intensity relates to a wide range of products and processes aggregated into one sector. Despite these uncertainties regarding the applicability of data to the product being analysed, it is noted by commentators (inter alia [9,10]) that even with the recent methodological improvements, the general approach to estimating embodied emissions and energy remains deterministic, thus obscuring both the uncertainty and true variability in embodied energy and life cycle assessment results.

Best practice in embodied emissions analysis involves a hybrid approach incorporating both process and input–output analysis (*inter alia* [11–13]). These two approaches rely respectively on process-related data and national sectoral economic data combined with environmental accounts to give emissions per unit monetary output from a sector. For process data, uncertainties arise due to variations in manufacturing processes and supply chains, measurement error and the use of out-of-date data. In the case of input–output data, a significant source of error is due to its highly aggregated nature: for example, construction sector emissions intensity is equally applied to house building and motorway construction. Pacca and Horvath [14] identify that uncertainties can also arise from economic boundary and methodological constraints.

A number of studies have deterministically calculated embodied energy and LCA values for a variety of building types in different countries. For example, Fay et al. [15] have estimated the energy intensity of an Australian residential building to be 1803 GJ while Thormark [16] calculated an embodied energy of  $2.9 \text{ GJ/m}^2$  for a Swedish apartment. Treloar et al. [17] also estimated the embodied energy of a three storey office building to be  $10.7 \,\text{G}/\text{m}^2$ . Dixit et al. [18] compiled a list showing different deterministic embodied energy values in residential and commercial buildings. Due to the constraints mentioned above, these data may be representative of a very small sample of buildings which do not provide sufficient information for decision makers to identify methods for reducing energy consumption in the building and construction supply chain. If however, the distributions of embodied CO2-eq can be estimated, then decision makers can design targeted policies to reduce the overall emissions in an industry sector or market segment. Understanding the distribution of embodied emissions in the construction sector or segment (for example in the apartment building sector) can therefore be useful in the formulation of effective policies. Furthermore, building designers and contractors will be better placed in terms of having more detailed information on their buildings which will enable them take informed environmental decisions on their designs as well as in their choice of building products and processes.

The main aim of this work is to develop and implement methodologies which measure the nature and extent of uncertainty when estimating embodied CO<sub>2</sub>-eq emissions in buildings. Specific objectives include:

- the presentation of a stochastic embodied CO<sub>2</sub>-eq assessment methodology incorporating both process and input-output analysis;
- using industry data to estimate the probability distributions of embodied  $CO_{2x}$  eq intensities for a particular building sector; and
- an evaluation of the embodied CO<sub>2</sub>-eq intensities and the uncertainty across a particular building type in Ireland

The stochastic embodied emissions methodology employed in this study is applicable to any type of structure, sectors other than construction as well as to other countries.

## 2. Methodology

The methodology adopted involves:

- the use of hybrid analysis to develop relationships between input parameters such as product emissions intensities, input-output (I-O) sectoral emissions intensities, disaggregated construction emissions intensities, construction materials employed and construction expenditure;
- an analysis of industry and economic (input-output) data to estimate probability distributions for certain input parameters;
- an application of the model to 7 Irish apartment buildings;
- the use of Monte Carlo simulation to derive probability and cumulative distributions for emissions intensities for the seven apartment buildings; and
- analysis and interpretation of results.

Hybrid embodied CO<sub>2</sub>-eq intensities are calculated where process analysis is used to determine the embodied CO<sub>2</sub>-eq in the main building materials, sub-sector direct embodied CO<sub>2</sub>-eq intensities to derive the direct embodied CO<sub>2</sub>-eq emitted on site in constructing the buildings, and input-output analysis to estimate the indirect embodied CO<sub>2</sub>-eq emitted in the construction of the building.

Seven apartment buildings in Dublin are investigated. For each apartment, the stochastic hybrid embodied CO<sub>2</sub>-eq intensities are evaluated using Monte Carlo analysis by deriving input distributions for the stochastic input variables. A distribution representative of the hybrid embodied CO<sub>2</sub>-eq distribution of apartment buildings in Ireland is derived by combining the distributions of the seven apartment buildings. This is based on the assumption that the samples are representative of the population of apartment buildings in Ireland. An analysis is then carried out on these distributions including deriving statistical parameters and the level of uncertainty in the results.

## 2.1. Stochastic hybrid embodied $CO_{2}-eq$ (ECO<sub>2</sub>-eq) intensity

Construction sector CO27eq emissions can be characterised as direct or indirect. The former are released as a result of activities directly related to construction processes on site (for example: excavation, fit-out, plant operation). The latter are associated with the use of energy in construction-related activities necessary for, but preceding site activities - these activities are 'upstream' of site work in the construction procurement supply chain (for example: energy used to manufacture building materials, excavation of raw aggregate, design team activities). The hybrid embodied  $CO_{23}$ eq (ECO<sub>2</sub>-eq) intensity can be broken down into three parts and expressed in terms of total grams of embodied CO<sub>2</sub>-eq per Euro [gCO<sub>2</sub>-eq/€] of total expenditure. Building materials embodied CO<sub>2</sub> eq intensities are calculated by process analysis, direct embodied CO<sub>2</sub>-eq emissions on the construction site are evaluated from disaggregated economic data of Irish construction firms and indirect embodied CO<sub>2</sub>-eq emissions are evaluated by input-output anal-

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ysis. Mathematically, the Hybrid ECO<sub>2</sub>-eq intensity is expressed as:

187 Hybrid ECO<sub>2</sub>-eq intensity

$$\frac{\left[\sum_{x=1}^{n} M_{x} e_{x}\right] + \left[i_{i} \sum_{j=1}^{5} S_{j} + \sum_{j=1}^{5} i_{dj} S_{j}\right]}{\sum_{i=1}^{5} S_{i} + C_{p}}$$

where  $M_x$  is the mass of building material x [tonnes, t]; n the number 189 of building materials for which process emissions intensities and 190 quantities exist;  $e_x$  the process embodied CO<sub>2</sub>-eq intensity of build-191 ing material x [gCO<sub>2</sub>-eq/t];  $i_i$  the input–output indirect embodied 192 CO<sub>2</sub>-eq intensity of construction [gCO<sub>2</sub>-eq/ $\in$ ];  $i_{dj}$  the direct embod-193 ied CO<sub>2</sub>-eq intensity of each construction sub-sector j [gCO<sub>2</sub>-eq/ $\in$ ]; 194 *i* the number of construction sub-sectors;  $S_i$  the expenditure clas-195 sified by construction sub-sector, j on activities associated with the 196 construction of the building  $[\in]$ ; and  $C_p$  the total cost of building 197 materials analysed using process  $CO_2$ -eq intensity inventory  $[\in]$ . 198

The following steps were undertaken in the calculation to avoid
 double counting of input-output inputs into the model for which
 process data (associated with building materials) has already been
 collected:

- the total cost of building materials,  $C_p$ , to which process data were applied was subtracted from the total expenditure extracted from the bill of quantities, therefore the remaining expenditure repre-
- sented by  $\sum_{j=1}^{N} S_j$  is only attributed to J-O inputs;
- this sum is multiplied by the 1-0 construction sector indirect

emissions to estimate total indirect emissions  $\left| i_i \sum_{i=1}^{J} S_i \right|$ 

• individual sub-sectoral expenditures,  $S_j$ , are multiplied by the corresponding direct emissions coefficients,  $i_{dj}$  and then summed

to estimate total direct emissions  $\left[\sum_{j=1}^{5} i_{dj}S_j\right]$ .

## 212 2.1.1. Material process embodied $CO_{2}$ -eq intensities

According to Goggins et al. [19] the sustainability credentials 213 of construction materials are gaining increasing importance as 214 the environmental impact of the construction industry becomes 215 apparent. Data on the ECO<sub>2</sub>-eq intensities of building materi-216 als however are uncertain. Industry (process) data was therefore 217 used to estimate probability distributions for all process embod-218 ied CO2-eq intensities of building materials. Available but limited 219 data of buildings materials process CO2, eq intensities obtained 220 from the Inventory of Carbon and Energy database, ICE v1.6a 221 [20] are fitted into a probability density function using EASYFIT 222 Statistical Application and the distributions ranked according to 223 Kolmogorov-Smirnov goodness of fit from a set of 57 different dis-224 tributions. Kolmogorov-Smirnov test (K-S test) was preferred to 225 other goodness of best fit tests such as Anderson-Darling goodness 226 of best fit because it is sensitive to differences in both the loca-227 tion and shape of different distributions [21]. It is also an exact 228 test, that is, the chi-square goodness-of-fit test depends on an ade-229 quate sample size for the approximations to be valid. Moreover, 230 Anderson-Darling test is only available for a few specific distribu-231 tions. Using the statistical parameters of the number one ranked 232 fitted distribution, a set of 10,000 random embodied CO2-eq inten-233 sities are then generated for each of the building materials and used 234 as input variables for the stochastic modeling. As an example, the 235 236 embodied CO<sub>2</sub>-eq intensity probability distribution of insulation is 237 shown in Fig. 1.

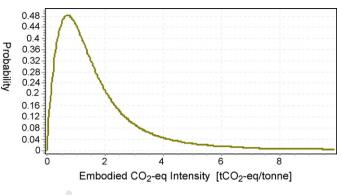




Table 1

Common building materials, their embodied  $CO_{2-eq}$  distributions and statistical parameters,

<b>Building materials</b>	Type of distribution	Distribution parameter
Concrete	Dagum function	$k = 0.11; \alpha = 0.4; \beta = 0.95; \gamma = 0.03$
Steel	Kumaraswany	$\alpha_1 = 2.1; \alpha_2 = 99.0; a = 0.22; b = 20$
Insulation	Burr function	$k = 1.5; \alpha = 1.8; \beta = 1.7; \gamma = 0$
Timber	Kumaraswany	$\alpha_1 = 0.34; \alpha_2 = 1.7; a = 0.27; b = 3.9$
Stone	Gamma	$\alpha_1 = 0.32; \ \beta = 0.21; \ \gamma = 0.06$
Brick	Kumaraswany	$\alpha_1 = 0.28; \alpha_2 = 1.7; a = 0.18; b = 2.8$

### Table 2

; and

Distributions and statistical parameters of the construction sub-sectors,

Construction sub-sectors	Type of distribution	Distribution parameter
Ground work Structural work Services Finishes Plant operation	Gen gamma (4P) Log-logistic Frechet Dagum Frechet	$\begin{array}{c} k = 1.2; \ \alpha = 0.56; \ \beta = 6.6; \ \gamma = 0.02 \\ \alpha = 1.1; \ \beta = 0.02; \ \gamma = 2.4 \times 10^{-6} \\ \alpha = 1.0; \ \beta = 0.02; \ \gamma = 0 \\ k = 0.73; \ \alpha = 1.6; \ \beta = 0.39; \ \gamma = 0 \\ \alpha = 1.1; \ \beta = 11.0; \ \gamma = -2.9 \end{array}$

Table 1 shows some common building materials used in apartment buildings and the number one ranked distribution the process embodied  $CO_2$ , eq intensities fits onto. In column 3 of Table 1, the statistical parameters used with the distribution type to generate the random embodied  $CO_2$ , eq intensities are shown.

## 2.1.2. Direct sub-sectoral embodied CO<sub>2</sub>-eq intensities

Probability distributions are also derived for the direct embodied  $CO_{2}$  eq intensities,  $i_{dj}$  of each of the five construction sub-sectors using disaggregated micro energy data collected by the Irish Central Statistics Office in their Census of Building and Construction [22-25] from 2003 to 2006. The sample data from the construction firms was chosen to be representative of the Irish construction sector and methodological notes are available from the Irish Central Statistics Office [26]. 682 firms were sampled in 2003, 628 in 2004, 728 in 2005 and 1291 in 2006. Table 2 shows a summary of the stochastic direct embodied CO<sub>2</sub>-eq intensity distributions and the statistical parameters of the construction sub-sector which was weighted from 2003 to 2006. It is assumed that all fuel used was diesel since the vast majority of plant and construction machinery in Ireland operates on diesel fuel [24]. Energy expenditure is divided among five construction sub-sectors defined by 'The General Industrial Classification of Economic Activities within the European Communities (NACE rev. 1)'. Construction sub-sectors 1-5 are hereafter referred to as 'Ground Works', 'Structural Work', 'Services', 'Finishes' and Plant Operation' respectively. The sub-sectors are defined in detailed below:

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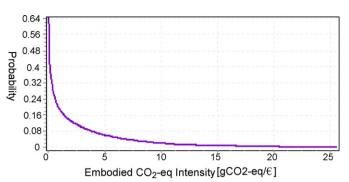
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**Fig. 2.** Direct embodied  $CO_2$ -eq intensity distribution of construction Sub-Sector 1: Ground Works,  $i_{d1}$ .

Ground works:	Site preparation, demolition of buildings, earth moving, ground work, drilling and boring, etc. (NACE 45.1)
Structural work:	Building of complete constructions or part thereof; civil and structural construction works, etc. (NACE 45.2)
Services:	Building installation, installation of electrical wiring and fittings, insulation, plumbing and other installations, etc. (NACE 45.3)
Finishes:	Building completion, joinery installation, plastering, floor and wall, covering, painting, glazing and general fit-out, etc. (NACE 45.4)
Plant operation:	Construction plant and equipments, etc. (NACE 45.5)

The equivalent primary energy [GJ] used in each construction sub-sector was calculated by multiplying energy expenditure [€] [22–25], average energy tariffs [G]/€] derived from the energy balance for Ireland [27] and primary energy factors [GJ/GJ] [28]. The energy intensity for each construction sub-sector is then derived in terms of the energy in GJ per Euro output of each sub-sector. Irish emission factors [g/G] [29] and global warming potentials (GWP) of the energy related GHG emissions are then multiplied by the energy intensities to obtain the direct sub-sector embodied  $CO_2$ -eq intensities  $i_{dj}$  [g $CO_2$ -eq/∈]. The GWP of the energy-related GHGs regulated under the Kyoto Protocol over a 100-year timeframe which are relevant to this study are: CO<sub>2</sub>-1; N<sub>2</sub>O-298; and CH<sub>4</sub>-25. To normalise all data used to the 2005 baseline year in the analysis, energy and construction price indices published by the Central Statistics Office [30] are applied to the average energy tariffs and construction sub-sector output respectively. 2005 was taken as the baseline year because it is the most recent year in which the national supply and use and input-output table has been published for Ireland.

Direct sub-sector  $CO_2$ -eq intensities  $i_{dj}$  of construction activities are treated as stochastic variables. The distributions for the direct sub-sector  $CO_2$ -eq intensities of the Irish construction sector are derived for each of the five sub-sectors. The distribution and statistical parameters are then used to generate input parameters in the Monte Carlo modeling. As an example, Fig. 2 shows the direct embodied  $CO_2$ -eq intensity distributions of Sub-Sector 1-Ground Works. The probability density functions of the distributions obtained for the sub-sectors are presented in Table 3.

### Table 3

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Construction sub-sector distributions and the probability density functions,

Distribution	Probability density function
4-parameter generalized gamma	$f(x) = \frac{k(x-\gamma)^{k\alpha-1}}{\beta^{k\alpha}\Gamma(\alpha)} \exp\left(\frac{\gamma-x}{\beta}\right)^k$
Log-logistic	$f(x) = \frac{\alpha}{\beta} \left(\frac{x-\gamma}{\beta}\right)^{\alpha-1} \left(1 + \left(\frac{x-\gamma}{\beta}\right)^{\alpha}\right)^{-2}$
Frechet	$f(x) = \frac{\alpha}{\beta} \left(\frac{\beta}{x-\gamma}\right)^{\alpha+1} \exp\left(-\left(\frac{\beta}{x-\gamma}\right)^{\alpha}\right)$
Dagum	$f(x) = \frac{ak \frac{(x-\gamma)}{\beta}k^{\alpha-1}}{\beta \left(1 + \left(\frac{x-\gamma}{\beta}\right)^{\alpha}\right)^{k+1}}$

## 2.2. Input–output indirect embodied CO<sub>2,</sub>eq intensity

Input–output (I–O) indirect embodied CO<sub>2</sub>-eq intensity of the construction sector as well as costs associated with each construction sub-sector (S<sub>1</sub>, S<sub>2</sub>, S<sub>3</sub>, S<sub>4</sub>, S<sub>5</sub>) in the bill of quantities and costs associated with building materials  $C_p$  are treated as deterministic input variables. Some uncertainties present in I-O analysis are outlined by eiolca.net [31] and some of these are addressed in Section 2.2.1. The level of uncertainty in input-output data is however difficult to estimate because the national input-output tables are compiled from a wide range of sources such as national systems of accounts, national economic sources, industry sector reports and statistical data. Lenzen and Dey [32] for instance stated that errors in **I-O** data depends largely on the error in the respective source data and estimated it to be in the region of 20%. The cost associated with energy use in the construction sub-sector and process analysis associated costs (building material costs) are used as deterministic input variables because they are assumed to be constant and are derived from standard construction industry approved costs of buildings material and construction activities.

Indirect I-O emissions are emissions arising from energy use not directly related to on-site construction but upstream of onsite construction and are calculated using I-O analysis. These were estimated using data from the Irish national I-O tables [33] which are compiled using data from national accounts as well as other national economic sources to show economic transactions between all product sectors of the national economy. The input coefficients of the economy-wide I-O tables are used to derive indirect I-O emissions intensities in the construction sector. This methodology is widely used and described in literature (see inter alia Bullard et al. [34], Lenzen and Dey [32] and Strømman and Solli [35]). In summary, the approach involves using the 2005 Irish I-O tables [33], average energy tariffs [27] and primary energy factors [28] to determine total I-O and direct I-O energy intensities per unit monetary value of construction sector output. The indirect I-O energy intensity is calculated as the difference between the total I-O and direct I-O energy intensities and is then converted to indirect I-O emissions intensity using the Irish emissions factors [29]. The direct requirement coefficient matrix of the Irish I-O tables was used to evaluate the direct I-O energy intensity and the Leontief inverse matrix used to calculate the total domestic energy intensity [13,36].

## 2.2.1. Limitations and the treatment of errors in I-O analysis

I-O analysis is known to suffer from well-documented limitations such as assumptions of homogeneity and proportionality [37]. For example, the proportionality assumption presumes that the inputs to each sector are proportional to their outputs so that if the output of a sector increases or decreases, then the consumption of intermediaries and primary inputs of that sector will also increase or decrease proportionally. In reality, there is not always a direct proportionality between activity and energy use. However, economies of scale should act to reduce marginal energy consumption. Homogeneity assumption proposes that each sector produces a single output using identical inputs and processes; however, this is obviously not the case with each sector containing many different products and services. Heterogeneity therefore occurs within the sector because of the aggregation of different production processes and products. Furthermore, I-O analysis assumes the uniform conversion of economic data into physical quantities (energy and emissions in this case) within a sector. For example, economic data are converted to energy consumed using national average energy tariffs, although such tariffs will vary across different industries.

This paper attempts to address some of these limitations. Disaggregation coefficients are used to disaggregate the energy supply sectors thus mitigating errors associated with the assumptions of 351

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homogeneity and uniform conversion [38]. Another limitation of I-O analysis is the aggregation of many different products into one sector in the national I-O tables [39]. This reduces applicability 359 of J-O derived embodied CO<sub>2</sub>-eq intensities to a specific product 360 or product sector. In Ireland, the national I-O table contains three aggregated energy supply sectors, namely: 362

- i. Coal, Peat, Crude Oil and Metal Ore Extraction; 363
- ii. Petroleum and Other Manufacturing Products; and 364
- iii. Electricity and Gas, 365

Some energy supply sectors are aggregated together either with 366 367 non-energy supply sectors or other energy supply sectors. For example, the 'Petroleum and Other Manufacturing' sector is an 368 aggregation of an energy supply sector, 'Petroleum' and non-energy supply sector 'Other Manufacturing'. Therefore, to address the 369 370 aggregation problem, disaggregation coefficients are introduced to 371 separate the energy supply sectors into individual energy sources 372 to which emissions factors can be applied. An analysis of the disag-373 gregation of the energy supply sectors in Ireland and its application 374 to embodied emissions was carried out by Acquaye and Duffy [38]. 375 The use of the disaggregation constants has a two-fold advantage. 376 Firstly, non-energy supply sectors are eliminated from the analysis. 377 Secondly, it enables individual primary energy factors and specific 378 energy tariffs to be used instead of average values for two or more 379 aggregated energy supply sectors (for example, for the aggregated 380 electricity and gas sector). 381

A further development of I-O analysis and its application to the 382 embodied CO<sub>2</sub>-eq analysis of buildings relates to the system bound-383 ary in the I-O analysis. Direct Requirement and Leontief Inverse I-O 384 coefficients for Ireland were derived for domestic product flows 385 386 only, omitting energy inputs into imported products and services. For example, EuroStat [40] states that in order to account for the 387 whole life energy use of a product using I–O analysis, the energy 388 used to produce imported inputs should also be included in such 389 an analysis. As such a methodology set out in the EuroStat Euro-390 pean System of Accounts I-O Manual [40] is applied to re-derive 391 the Irish direct and Leontief coefficients which are used to calculate 392 the **J**–O indirect CO<sub>2</sub>–eq emissions. The estimation of the addition 393 of energy inputs into imported construction sector goods and ser-394 vices is important in an open economy such as Ireland's [41] and 395 provides greater information for decision making by designers and 396 policy makers by considering total global impacts. Furthermore, 397 given that approximately 56% of Irish imports are from the EU [42] 398 an understanding of the sources of emissions are important from 399 an EU policy perspective. 400

#### 2.3. Case studies 401

The seven apartment buildings are all located in Ireland. They 402 comprise concrete strip foundations and ground floor slabs with 403 block-work rising elements, timber floors and roof structures. 404 External finishes included brickwork and render, double-glazed 405 timber-framed windows and concrete roof tiles. Internal finishes 406 407 included timber stud partitions, plasterwork, tiling, fitted kitchens and painting. Further details are presented in Table 4. 408

#### 3. Results 409

#### 3.1. Hybrid embodied CO<sub>2</sub>, eq intensity distributions 410

For each apartment building, 10,000 Monte Carlo simulations 411 were undertaken and the results (hybrid ECO<sub>2</sub>-eq intensities) were 412 413 plotted on a scatter diagram. The scatter diagram in Fig. 3 illustrates the variations that occur in the stochastically derived hybrid  $\mathrm{ECO}_{2\bar{\lambda}}$ 414

## Table 4

Description of apartment buildings used in the case studies.

Apartments	Description of apartment buildings
Apartment 1 Apartment 2	Concrete piled foundation, reinforced concrete frame with infill 215 mm block-work; 320 mm thick reinforced concrete slab with 400 mm × 600 mm reinforced concrete columns on 9 m × 9 m grids. External finishes included brickwork and render, double-glazed timber-framed windows, thermafloor insulation and concrete roof tiles. Internal finishes included timber stud partitions, plasterwork and painting. Reinforced concrete frame with minor structural steel to roof; 300 mm thick reinforced concrete slab with 400 mm × 400 mm reinforced concrete slab with grids. Thermafloor insulation and external finishes include plaster work with gloss paint to wood work. Roof work consists of mastic asphalt roofing with rigid sheet covering and decking. Extensive mechanical installations made up of
Apartment 3	waste, water, gas, heating, HVAC, and lift installations. Reinforced concrete substructure, block work external walls
Apartment 4	$440 \times 215 \times 100$ , concrete work in concrete frame structure, woodwork and precast pre-stressed concrete work for stairs, structural steel work fabricated members, internal walls partitioned with softwood and thermafloor insulation. Reinforced concrete substructure with reinforced concrete
	in situ concrete frame, fabricated members steel work, concrete work stairs 1.2 m wide, block work internal walls $100 \times 215 \times 440$ , in situ concrete floors and slabs exceeding 150 mm reinforced and thermafloor insulation.
Apartment 5	Structural steel work with fabricated members, brickwork and block work internal walls with concrete blocks 100 × 215 × 440. In-situ concrete floors slabs exceeding 150 mm thick and precast concrete 200 mm thick with span >5.00 m and <7.00 m. Thermafloor insulation and structural steel work roof 254 × 146 × 37 kg/m Universal Beam.
Apartment 6	Reinforced concrete substructure, brickwork and concrete work size $440 \times 215 \times 100$ , floor insulation laid to underside of floor, in situ concrete floor exceeding 150 mm thick. Concrete walls consist of reinforced in situ concrete with thickness not exceeding 0.20 m <sup>2</sup> . Concrete screed floor 75 mm thick with fabric reinforcement.
Apartment 7	Reinforced concrete substructure, brickwork and concrete work size 440 $\times$ 215 $\times$ 100; brick and block work external walls, coping to parapet 560 $\times$ 150. Precast concrete lintels, 100 $\times$ 65 mm, Insulation board 100 mm thick, structural steel work 50 $\times$ 90 $\times$ 10 kg/m stainless steel. Carcassing roof with insulation

eq intensities of Apartment 1. Scatter diagrams for Apartments 2-7 are presented in the AppendixBAppendix.

Fig. 4 is an illustration the ECO<sub>2</sub>-eq intensity probability distributions of each of the apartment buildings analysed in the study. Each distribution shows the ECO<sub>2</sub>-eq intensity probability variations relating to the scatter plots in Fig. 3 and the AppendixBAppendix.

Fig. 5 shows the scatter plot of the combined seven apartment buildings representing 70,000 Monte Carlo simulated results and assumed to be the average for the apartment building sector in Ireland. It shows the dispersion in embodied emissions intensities of the apartment buildings due to the variability in input parameters such as emission intensities of building materials.

The average hybrid ECO2-eq intensity distribution for apartment buildings in Ireland shown in Fig. 6 was obtained by combining the individual distributions of the seven apartment buildings and also represents the combined ECO<sub>2</sub>-eq intensity scatter plots in Fig. 5. The distribution can be characterised as a Wakeby distribution with five parameters:  $\beta = 1.4 \times 10^2$ ,  $\gamma = 1.3 \times 10^2$  and  $\delta = 0.77$  are shape parameters while  $\zeta = 0$  and  $\alpha = 1.5 \times 10^5$  are location parameters.

A general quantile function for a Wakeby Distribution is given by Eq. (2) below:

$$x(F) = \zeta + \frac{\alpha}{\beta} (1 - (1 - F)^{\beta}) - \frac{\gamma}{\delta} (1 - (1 - F)^{-\delta})$$
(2)

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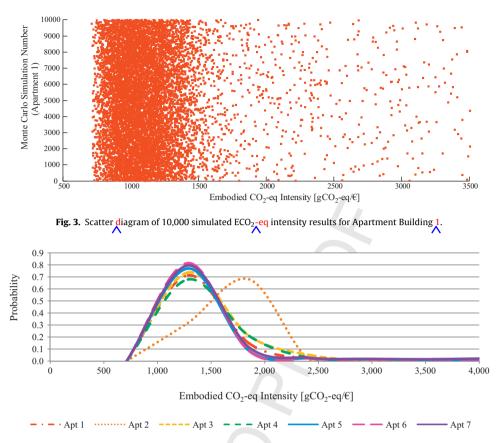
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**Fig. 4.** Hybrid embodied CO<sub>2</sub>-eq intensity probability distributions of the 7 apartment buildings.

Hence, the quantile function describing the derived average distribution for apartment buildings in Ireland is given by Eq. (3)
below:

$$x(F) = 1071(1 - (1 - F)^{1.4 \times 10^2}) - 168(1 - (1 - F)^{-0.77})$$
(3)

The ECO<sub>2</sub>-eq intensity distribution in Fig. 6 was derived using 100 class intervals with a bin or class size of  $570 \text{ gCO}_2$ -eq/ $\in$  The mean ECO<sub>2</sub>-eq intensity was found to be  $1636 \text{ gCO}_2$ -eq/ $\in$  while the median was  $1127 \text{ gCO}_2$ -eq/ $\in$ . This can be interpreted to imply that an 'average' design of Irish apartment buildings built in 2005 will result in the emissions of  $1636 \text{ gCO}_2$ -eq/ $\in$ . This is based on the assumption that the building samples analysed are representative of the population of apartment buildings in Ireland. Based on a class size of 570 gCO<sub>2</sub>-eq/ $\in$  (representing 100 class intervals) used in the distribution, the likeliest embodied CO<sub>2</sub>-eq intensity of an apartment building is  $1325 \text{ gCO}_2$ -eq/ $\in$  with a probability of 69%.

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Using the principle that the uncertainty of a measured result can be taken to represent the estimated standard deviation [43]

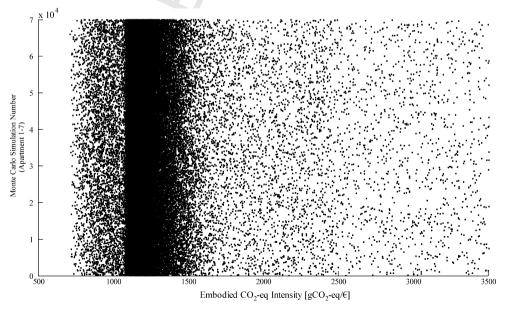


Fig. 5. Scatter diagram of 70,000 simulated ECO<sub>2</sub>-eq intensity results for apartment buildings in Ireland.

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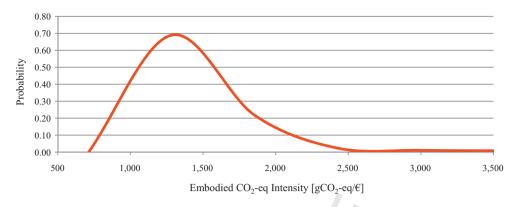


Fig. 6. Embodied CO<sub>2</sub>-eq intensity probability distribution of apartment buildings in Ireland.

the uncertainty associated with the stochastic ECO<sub>2</sub>-eq intensity 455 distribution can be evaluated. It is therefore estimated that the 456 mean of the stochastic distribution of  $ECO_{2}$  q intensity across the 457 apartment building sector is 1636gCO<sub>2</sub>-eq) ∈ with an uncertainty 458 of  $73 \text{gCO}_2 - \text{eq}/\epsilon$ . An embodied  $CO_2 - \text{eq}$  intensity of  $73 \text{gCO}_2 - \text{eq}/\epsilon$ 459 was estimated as the standard deviation of the Wakeby derived 460 average distribution of apartment buildings in Ireland after 70,000 461 stochastic simulations. It can therefore be assumed that an embod-462 ied CO2-eq intensity calculated for an apartment building in Ireland 463 would have an uncertainty of 73 gCO<sub>2</sub>, eq/∈. It is however rec-464 ognized that the addition of stochastic analysis for I-O indirect 465 emissions will change the level of uncertainty in the overall results. 466 467 **Q2** This is because Lenzen and Dey (2000) reported that the estimated inherent error and variability in I-O data is in the region of 20%. 468

The cumulative hybrid ECO<sub>2</sub>-eq intensity probability distribution of apartment buildings in Ireland is presented in Fig. 7. The median (50th percentile) and the 90th percentile are respectively 1127 gCO<sub>2</sub>-eq/ $\in$  and 1723 gCO<sub>2</sub>-eq/ $\in$ . This can be interpreted to mean that apartment buildings with embodied CO<sub>2</sub>-eq intensity greater or equal to 1723 gCO<sub>2</sub>-eq/ $\in$  are in the top 10% of apartment buildings with the highest embodied emissions impacts in Ireland.

## 476 **4. Discussion**

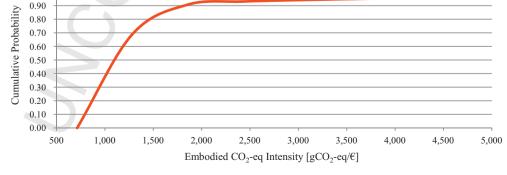
In Fig. 4, the hybrid ECO<sub>2</sub>, eq intensity distributions of the 477 individual apartment buildings can be observed. The differences 478 in the distribution of Apartment 2 relative to the others can be 470 attributed to two factors: firstly, Apartment 2 contained much 480 greater quantities of mechanical and electrical services, the pro-481 cess probability density function for which resulted in negative 482 skewing of the distribution for the overall building; secondly, indi-483 rect I-O data displaced a greater proportion of non-services-related 484 process data, thus excluding more positively skewed distributions 485

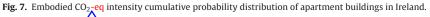
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from the result. The importance of using stochastic techniques in  $ECO_2$ -eq intensity analysis is seen in the ability of the model to capture the variability in the embodied emissions in each building. For the combined hybrid  $ECO_2$ -eq intensity distribution, the uncertainty measured as the standard deviation of the distribution is estimated to be 73 gCO\_2-eq/e. The uncertainty measured across the apartment building sector can therefore be factored into any calculation to account for any variability.

Obtaining the combined probability distribution represents an important step forward if embodied emissions policy measures are to be formulated. This helps both policymakers to formulate a basis for providing embodied CO<sub>2</sub>-eq intensity information in different sectors, and building designers to make informed decision on material selection based on their embodied CO<sub>2</sub>-eq intensities (see Venkatarama Reddy and Jagadish [44]).

The combined ECO<sub>2</sub>-eq intensity probability distributions yielded a Wakeby distribution. While this was derived from analysing seven apartment buildings because of limited data, the shape should remain the same because of representative variation (that is, similarity in construction methods, design, materials used, etc.) when it is updated with new information and data. To assess the basis of this assumption, a sensitivity analysis is carried out using the derived ECO<sub>2</sub>-eq intensity cumulative distribution in Fig. 7. The sensitivity analysis is undertaken based on the premise that despite using only seven buildings as case studies, statistical parameters would not significantly change if large numbers of buildings were sampled. Hence a comparison is made between the cumulative distributions derived from the seven buildings and those derived from a much more limited number of buildings (5 and 6 apartment buildings represented by Apartments 1–5 and Apartments 1-6 respectively). As can be observed in Fig. 8, there are marginal differences between the cumulative distribution for the 5 apartment buildings (median: 1.06%; 90th percentile: 0.08%; and





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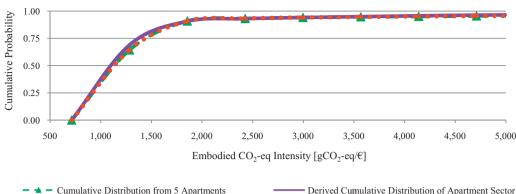
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Derived Cumulative Distribution of Apartment Sector

····· Cumulative Distribution from 6 Apartments

Fig. 8. Sensitivity analysis of the cumulative embodied CO<sub>2</sub>-eq intensities for different sample size.

mean: 5.04%) and that for 6 apartment buildings (median: 0.45%; 90th percentile: 0.08%; and mean: 2.5%) when compared to the average of the apartment building sector (7 buildings used in this study). While the reasoning behind the sensitivity analysis of ECO2eq intensity distribution based on the number of cases analysed is valid, for it to be statistically rigorous, a much larger sample size is required, especially if the distributions are to be used to inform policy making.

## 5. Conclusions

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This paper proposes a stochastic approach to estimating embodied emissions and, by way of example, applies it to an Irish case study of seven apartment buildings. Greater methodological and informational benefits are derived from the stochastic hybrid ECO<sub>2</sub>-eq intensity analysis of buildings compared to deterministic analysis. The stochastic ECO<sub>2</sub>-eq intensity employed integrates the accuracy of process analysis and the system boundary completeness of I-O analysis while providing a solution to the variability that exist in the ECO<sub>2</sub>-eq intensity data sets. Stochastic analysis also helps to establish the relationship between the ECO<sub>2</sub>-eq intensity of apartment buildings and the likelihood of obtaining a particular ECO<sub>2</sub>-eq intensity value. This can provide useful information if embodied CO<sub>2</sub>-eq standards and regulatory measures are to be formulated. A Wakeby distribution with known parameters and uncertainty was derived for the embodied CO2-eq intensities of apartment buildings in Ireland. Such a stochastic distribution with known parameters provides more useful information to building designers and policy makers. The stochastic embodied emissions methodology employed in this study is applicable to any type of structure, sectors other than construction as well as to other countries.

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#### Appendix A. Supplementary data 556

Supplementary data associated with this article can be found, in the online version, at doi:10.1016/j.enbuild.2011.01.006.

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