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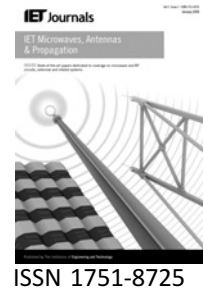
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# A printed CPW-fed slot-loop antenna with narrowband omnidirectional features

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**Abstract:** The design of a novel CPW-fed printed slot-loop antenna with narrowband omnidirectional attributes is proposed. The antenna geometry is selected to reduce slot coupling, thus achieving both a narrow bandwidth and an omnidirectional radiation pattern simultaneously. A gain of 2.1 dBi is accomplished with high radiation efficiency. Very narrow fractional impedance bandwidths as low as 2.9% are realised with good omnidirectional radiation characteristics. A technique providing unconstrained control of the bandwidth in the range of 1.7–6.9% is described.

## 1 Introduction

The sustained miniaturisation of electronic devices demands continued reduction in antenna size and profile. Studies have been carried out to determine how small an antenna can be, while maintaining high gain and bandwidth [1–4]. However, very few studies were carried out to design narrowband omnidirectional microstrip antennas with reasonable gain and high radiation efficiency. Narrow bandwidths are desirable in many applications such as in security and military systems, radiolocation, low power devices and digital enhanced cordless telecommunications (DECT), where system selectivity can be improved. Many military security communication systems prefer neighbouring antennas with high mismatch loss and decoupling preferably achieved by narrowband antennas [5, 6]. At present, complex impedance structures are needed to achieve good decoupling between omnidirectional antennas located in close proximity [7]. Omnidirectional printed antenna designs using CPW feed methods have been reported [8–10]. The printed loop antenna with a uniform current distribution is a suitable choice for omnidirectional radiation pattern. However, a small loop antenna with low radiation resistance and high reactance is difficult for impedance match. Although a larger loop antenna has a reasonable radiation resistance, the antenna current distribution along the loop becomes non-uniform and thus will not yield the desired omnidirectional pattern. To design a loop antenna with an omnidirectional radiation pattern with an acceptable input

impedance matching is challenging. A modified Alford open-loop antenna was proposed for omnidirectional radiation patterns in 2.4 GHz applications but with significantly lower gain and broader impedance bandwidth [11]. These omnidirectional antennas have broad impedance bandwidths, greater than 10%, which makes them inappropriate for narrowband applications [12]. No studies were reported to design narrowband omnidirectional microstrip antennas. The bandwidth of printed slot-loop antennas is increased at the cost of gain and directivity. That is, the smaller the bandwidth, the more directional the radiation becomes, with reduced beamwidth. In general, if a printed slot-loop antenna becomes omnidirectional, its bandwidth tends to become wider and gain deteriorates [13]. Therefore, physically, it is not easy to design an antenna with omnidirectional radiation pattern and narrow bandwidth, while maintaining reasonable gain. Microstrip slot-loop antennas have the advantage of being able to produce bidirectional and unidirectional radiation patterns with impedance bandwidths ranging from 10% to 70%. An interesting feature of slot antennas is this greater bandwidth because of the bidirectional radiation properties. But normal microstrip slot antennas are not compatible with monolithic fabrication and therefore easier integration with active solid state devices is not possible. CPW-fed slot antennas can solve these problems effectively [14–16].

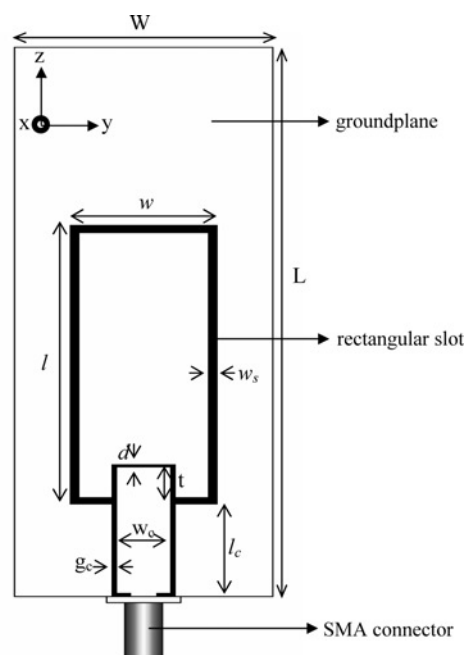
In this paper, a novel design of a compact CPW-fed slot-loop antenna that provides both omnidirectional and

narrowband characteristics is presented. The high cross-polarisation level typically seen in these types of slot-loop antennas is reduced in the proposed antenna. As maintaining a very good radiation efficiency and reasonable gain for a narrowband omnidirectional antenna is difficult, the design considerations made to implement this are described in the paper. Furthermore, good control of the antenna bandwidth is realised by varying the width of the radiating slot, without significantly affecting the antenna input impedance or resonant frequency.

## 2 Antenna design

Normal slot-loop configurations with CPW feeds require a long CPW transmission line to match the loop (owing to orthogonality of the feedline with respect to the loop long dimension), resulting in larger antenna size. Moreover, the large horizontal dimension of these loops limits the modification of the bidirectional radiation pattern of the slot-loop antenna into an omnidirectional one [17]. As the antenna operating frequency mainly depends on the total slot-loop length,  $2(l+w)$ , feeding it along the smaller dimension (width) of the loop with a tuning stub provides a better way to realise compactness and omnidirectionality. The operating bandwidth and the symmetry of the pattern depends mainly on the aspect ratio of the loop, which is given by  $\gamma = l/w$ . A square loop ( $\gamma = 1$ ) shows better symmetry of the bidirectional radiation patterns, but has a narrower band in terms of matching than a loop having a smaller aspect ratio. Therefore, a much greater aspect ratio has been chosen in this design to favour narrowband omnidirectional design. Furthermore, for slot-loop antenna designs with  $\gamma < 1$ , there is an abrupt rise in the input impedance close to the resonant frequency, as the width ( $w_s$ ) of the radiating slot increases [18]. This effect is significantly reduced with the appropriate selection of the aspect ratio in the proposed design.

The geometry of the proposed narrowband omnidirectional slot-loop antenna is shown in Fig. 1. The CPW arrangement employs single-sided laminate in order to realise an omnidirectional pattern. The CPW feedline is designed for  $50 \Omega$  characteristic impedance using Agilent AppCAD and optimised with CST Microwave Studio. The CPW centre strip has a width of  $w_c = 6.4$  mm and gap of  $g_c = 0.5$  mm. The antenna is fabricated on an FR-4 substrate with dielectric constant,  $\epsilon_r = 4.1$  and thickness  $h = 1.52$  mm. As there is a linear relationship between the total slot-loop length and the dominant resonant mode, the slot-loop length,  $l$  is chosen slightly less than one-half of the slot wavelength ( $l \approx 0.82 \lambda_s/2$ ). The slot-loop width,  $w$  is kept less than one-quarter of  $\lambda_s$  ( $w \approx 0.62 \lambda_s/4$ ) to minimise the magnetic current variation along the loop width,  $w$ . However, the slot-loop width is critical for impedance matching. The groundplane dimensions also affect the antenna input impedance and it is found that the groundplane width  $W$  must be optimised for good

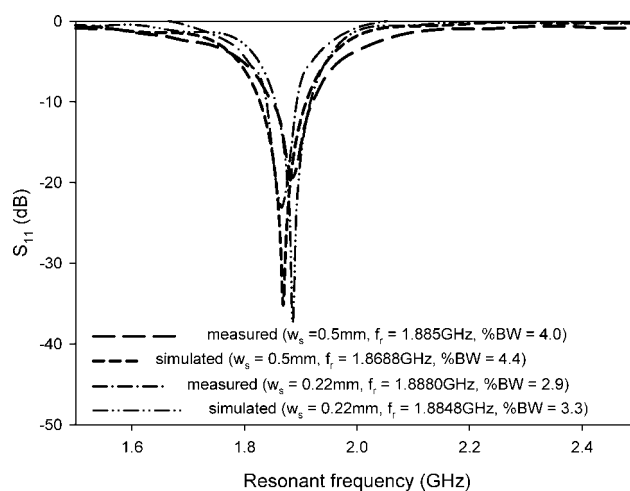


**Figure 1** Geometry of the proposed CPW fed slot-loop antenna

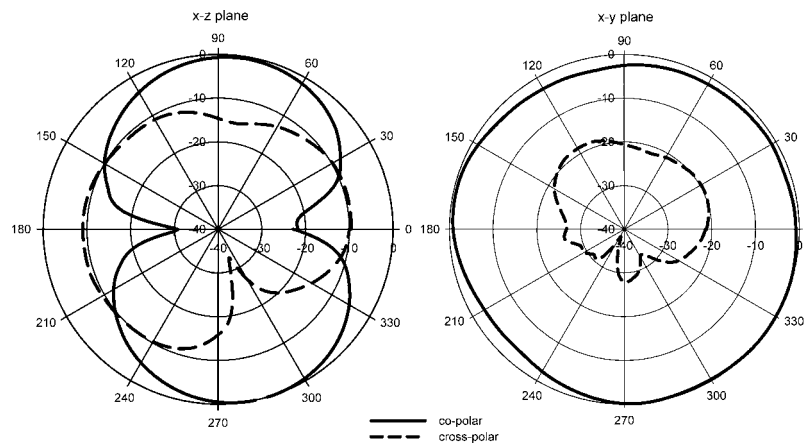
The various dimensions in mm are:  $L = 86$ ,  $W = 30$ ,  $w = 16$ ,  $l = 42.5$ ,  $w_s = 0.5$ ,  $w_c = 6.4$ ,  $l_c = 14.55$ ,  $g_c = 0.5$ ,  $t = 4.05$  and  $d = 0.3$

impedance matching. The optimised groundplane dimensions are  $L = 86$  mm and  $W = 30$  mm.

A new type of inset CPW feeding with a tuning stub is introduced to improve matching at the resonant frequency. The tuning stub length,  $t$  is 4.05 mm with a top slot gap,  $d = 0.3$  mm. The antenna bandwidth shows dependence on both the tuning stub length and the top slot width and therefore some fine tuning is needed to achieve narrow bandwidth. The geometry of the slot is different from that



**Figure 2** The measured and simulated  $S_{11}$  of the proposed narrowband omnidirectional CPW fed slot-loop antenna for a slot width,  $w_s = 0.5$  and  $0.22$  mm



**Figure 3** Measured far-field co-polar and cross-polar radiation patterns of the CPW fed slot-loop antenna at 1.885 GHz

of the conventional slot-loop CPW antennas and the slot-loop length;  $l$  is much larger compared with the slot-loop width  $w$ , giving an aspect ratio,  $\gamma = 2.65$ . This significantly reduces the coupling from the horizontal and vertical slots along the width and length of the rectangular slot and effectively decreases the antenna bandwidth.

The measured and simulated  $S_{11}$  of the proposed antenna for a slot width  $w_s = 0.5$  mm and 0.22 mm is illustrated in Fig. 2, showing good agreement. It is observed that for  $w_s = 0.22$  mm, the antenna resonates at 1.8880 GHz with a 10 dB RL impedance bandwidth of 55 MHz that corresponds to a narrow fractional bandwidth of 2.9%. The measured  $S_{11}$  clearly shows that unlike other slot-loop designs, the proposed antenna operates in a narrower band with good impedance matching. The bandwidths of ordinary slot-loop antennas range from 6% to 7% with the bidirectional radiation pattern. This bandwidth will

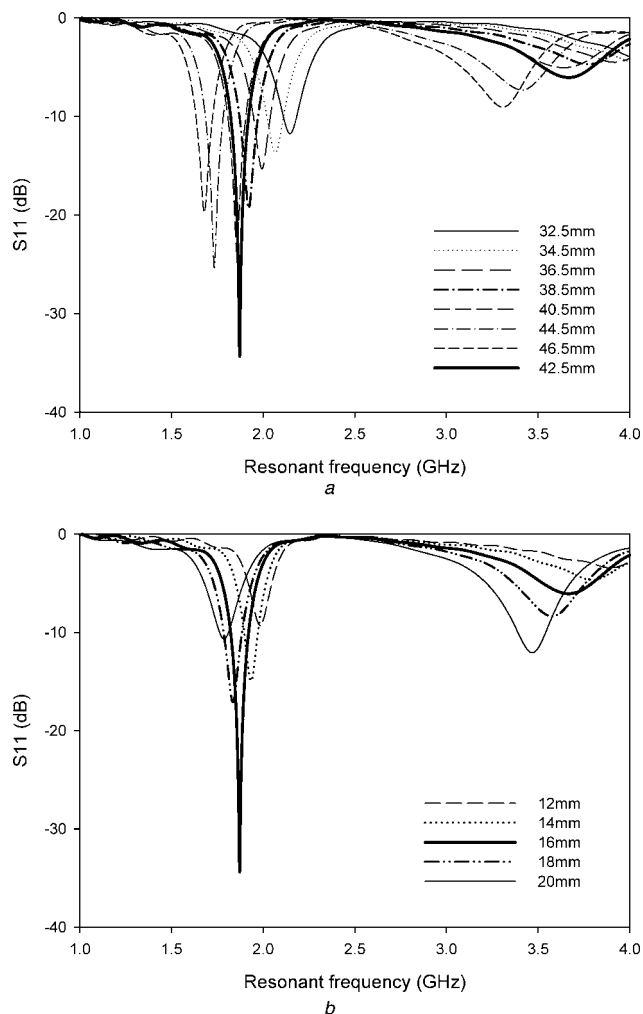
broaden again if an omnidirectional pattern is required. The measured antenna gain was found to be 2.1 dBi and the simulated radiation efficiency was 93%.

The measured radiation patterns for the two principal planes are plotted in Fig. 3. The design provides an omnidirectional radiation pattern, superior to that of the conventional slot-loop antennas, with an average pattern variation of 1.5 dB in the  $xy$ -plane. By choosing a large aspect ratio for the loop and hence a small slot loop width  $w$ , the radiated electric fields in the azimuth plane ( $xy$ -plane) of the proposed antenna are aligned along the direction of the current (along  $z$ -axis). The spacing of the excited surface currents on the two side edges of the antenna is electrically too small to allow asymmetry in the azimuthal pattern. The level of cross-polarisation in normal CPW-fed slot-loop antennas is very high [19]. The cross-polarisation mainly arises from the sides of the loop parallel

**Table 1** Performance of the proposed CPW fed slot-loop antenna with various rectangular slot-loop dimensions

Slot-loop width, $w$ (mm)	Slot-loop length, $l$ (mm)	Resonant frequency (GHz)	Bandwidth (MHz)	% bandwidth	Gain (dBi)	Rad. eff. (%)
16	34.5	2.1696	97.9	4.4	2.6	92.8
	38.5	2.0192	101.3	5.0	2.3	93.5
	42.5	1.8848	98.8	5.2	2.1	93.0
	46.5	1.7631	92.0	5.2	2.0	91.4
	48.5	1.7088	85.4	5.0	1.9	91.1
12	42.5	1.9840	–	–	2.0	90.0
14		1.9328	74.9	3.9	2.0	90.6
16		1.8848	98.8	5.2	2.1	93.0
18		1.8337	100.3	5.5	2.1	93.6
20		1.7868	–	–	–	2.1

The fixed dimensions are:  $L = 86$ ,  $W = 30$ ,  $w_s = 0.5$ ,  $w_c = 6.4$ ,  $l_c = 14.55$ ,  $g_c = 0.5$ ,  $t = 4.05$  and  $d = 0.3$



**Figure 4** Variation of resonant frequency and  $S_{11}$  with different slot-loop dimensions

*a* With slot-loop length,  $l$   
*b* With slot-loop width,  $w$

to the CPW feedline. But this cross-polarisation can be reduced by increasing the length  $l$  of the slot-loop. The field distribution is weaker when the slot-loop length,  $l$  is increased. By suitably selecting the aspect ratio for the rectangular slot-loop, this high level of cross-polarisation is reduced along the  $z$ -axis in the  $x$ - $z$  plane to better than  $-15$  dB in the proposed design.

### 3 Parametric studies and discussion

An important goal of this paper is to provide design information for the narrowband omnidirectional CPW-fed microstrip antenna. Rigorous parametric studies are carried out to investigate the effect of antenna geometry on the input impedance, resonant frequency, bandwidth, gain, radiation efficiency and level of cross-polarisation. The criteria to obtain a good omnidirectional radiation pattern are also discussed.

#### 3.1 Effect of rectangular slot-loop dimensions ( $l$ and $w$ )

The resonant frequency of the proposed slot-loop antenna depends on the total slot-loop length  $2(l + w)$ . Considering the presence of different dielectric properties on either side of the slot and the fact that the field components are not confined to the dielectric substrate alone, the wavelength in the slot-loop may be calculated as

$$\lambda_s = c/f_r \sqrt{\epsilon_{r \text{ eff}}}$$

where  $\epsilon_{r \text{ eff}}$  is the effective dielectric constant given by  $\epsilon_{r \text{ eff}} = (\epsilon_r + 1)/2$ .

A design equation can then be derived empirically, relating the resonant frequency ( $f_r$ ) of slot-loop and the total slot-loop length as

$$f_r = 1.14c/\{2(l + w)\sqrt{\epsilon_{r \text{ eff}}}\}$$

**Table 1** illustrates the variation in resonant frequency, fractional impedance bandwidth, gain and radiation efficiencies with change in slot dimensions. This has been studied by keeping the groundplane and tuning stub dimensions the same as described in **Fig. 1**. The variation of antenna resonant frequency with slot dimensions is plotted in **Fig. 4**. It is evident that the impedance matching of the antenna is heavily dependent on the slot-loop width,  $w$ . A similar observation is also made with the ground plane width  $W$ . Thus the dimensions of the antenna, orthogonal to the CPW feedline determine the impedance matching. The fractional impedance bandwidth shows an increase with increased slot-loop length  $l$ , while the gain decreases.

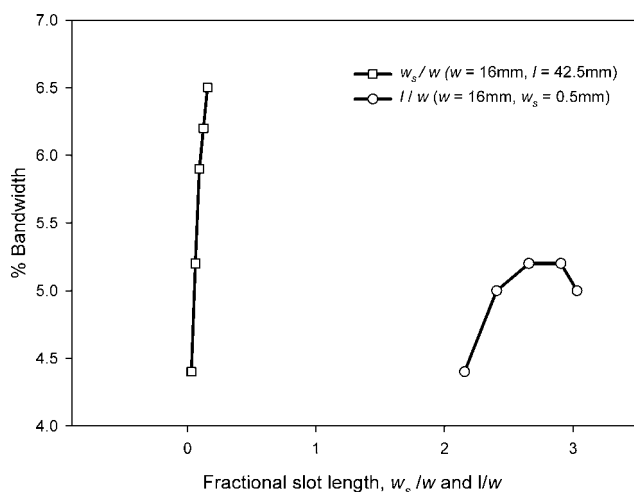
#### 3.2 Effect of groundplane dimension ( $L$ and $W$ )

The width of the groundplane  $W$  determines whether the radiation pattern of the proposed slot-loop antenna is omnidirectional or bidirectional in nature. Therefore the width of the groundplane is reduced to a minimum to yield better omnidirectional properties. But a reduction in the groundplane dimensions will increase the bandwidth. No significant reduction in antenna gain was observed when the ground plane dimension is changed. It was found that an increase in the groundplane width,  $W$ , affects the antenna's omnidirectional radiation pattern and for values greater than approximately 38 mm, the pattern becomes essentially bidirectional. A decrease in bandwidth is observed with increase in groundplane width, accompanied by poor impedance matching. Hence, the groundplane width needs to be adjusted to provide better omnidirectional pattern and good matching. **Table 2** tabulates the results for different values of  $L$  and  $W$  of the antenna for a particular slot loop and tuning stub dimension. No significant change in resonant frequency

**Table 2** Performance of the proposed CPW fed slot-loop antenna with different ground plane dimensions

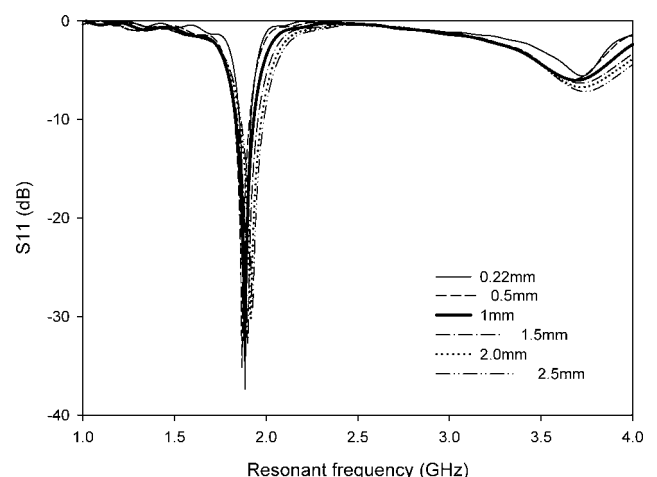
Ground plane width, $W$ (mm)	Ground plane length, $L$ (mm)	Resonant frequency (GHz)	Bandwidth (MHz)	% bandwidth	Gain (dBi)	Rad. eff. (%)
30	62	1.8368	126.8	6.9	2.3	94.7
	70	1.8688	113.6	6.1	2.2	94.1
	78	1.8848	104.8	5.6	2.1	92.8
	86	1.8848	98.8	5.2	2.1	93.0
	100	1.8752	77.7	4.1	2.3	90.4
30	86	1.8848	98.8	5.2	2.1	93.0
34		1.8816	88.7	4.7	2.0	90.7
38		1.8848	72.9	3.9	2.1	90.0
42		1.8847	51.5	2.7	2.3	91.7
46		1.8847	32.4	1.7	2.3	90.1

The fixed dimensions in mm are:  $l = 42.5$ ,  $w = 16$ ,  $w_s = 0.5$ ,  $w_c = 6.4$ ,  $l_c = 14.55$ ,  $g_c = 0.5$ ,  $t = 4.05$  and  $d = 0.3$ .



**Figure 5** Effect of slot width,  $w_s$ , and slot-loop length,  $l$ , relative to the slot-loop width,  $w$ , on the percentage bandwidth of the antenna

All other antenna dimensions are the same as in Fig. 1

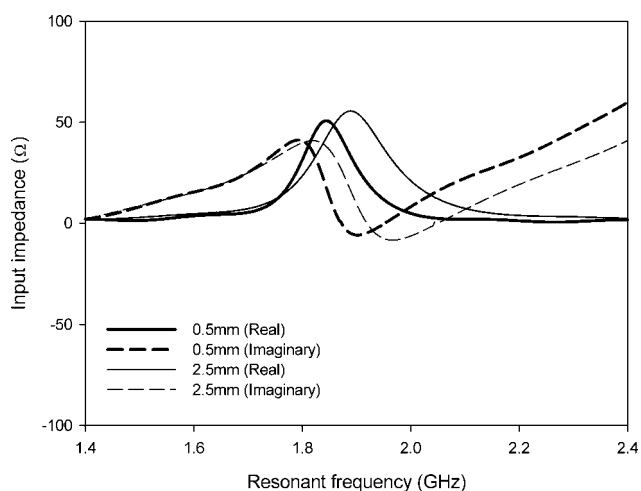


**Figure 6**  $S_{11}$  of the proposed slot-loop antenna for different slot widths,  $w_s$

**Table 3** Performance of proposed CPW fed slot-loop antenna with change in slot width,  $w_s$

Slot-loop width, $w$ (mm)	Slot-loop length, $l$ (mm)	Slot width, $w_s$ (mm)	Resonant frequency (GHz)	Bandwidth (MHz)	% bandwidth	Gain (dBi)	Rad. eff. (%)
16	42.5	0.5	1.8688	82.1	4.4	2.0	91.3
		1	1.8848	98.8	5.2	2.1	93.0
		1.5	1.9008	112.9	5.9	2.0	92.0
		2	1.9168	118.6	6.2	2.1	93.8
		2.5	1.9264	124.7	6.5	2.2	95.1





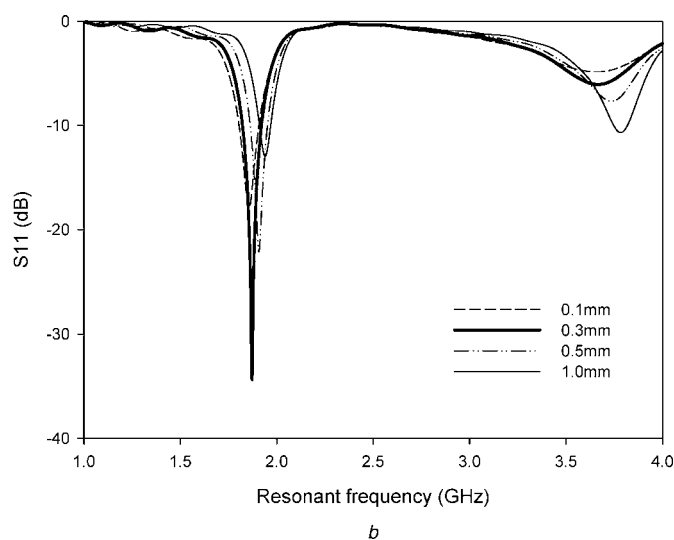
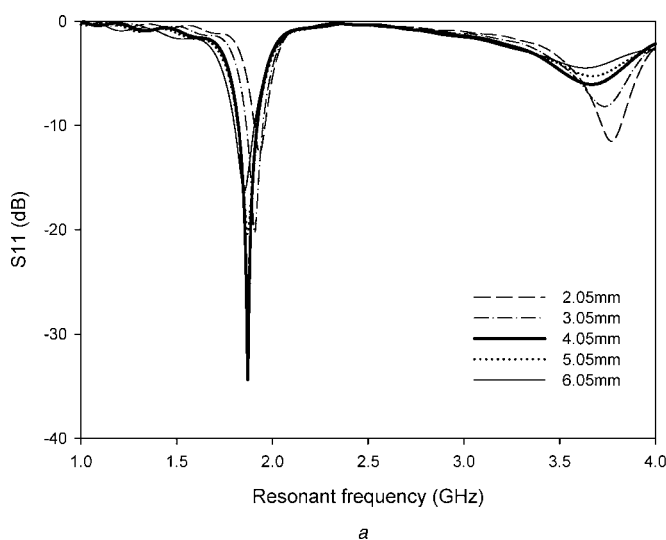
**Figure 7** Simulated input impedance variation of the antenna with slot width  $w_s$

All other dimensions of the antenna for these cases are given in Fig. 1.

was observed when  $L$  and  $W$  are varied. In this case, the antenna gain remains a constant only because of the fact that bandwidth increases with decrease in groundplane dimension. However, the cross-polarisation in the  $xz$ -plane increases with decreases in the groundplane size. This is mainly because of diffraction from the edges of the small ground plane.

### 3.3 Effect of slot width ( $w_s$ ) and tuning stub

The bandwidth of the proposed CPW-fed slot-loop antenna depends mainly on the rectangular slot width  $w_s$ . The dependence of the impedance bandwidth on the slot width,  $w_s$ , is given in Fig. 5. The effect of slot width ( $w_s$ ) and slot length ( $l$ ) relative to the slot-loop width ( $w$ ) on the antenna bandwidth is illustrated. It is evident from the plots that the antenna bandwidth is a strong function of slot width ( $w_s$ ) rather than the slot length ( $l$ ). Thus, the slot width provides a useful tuning dimension for tailoring



**Figure 8** Variation of  $S_{11}$  with change in tuning stub dimensions

a Stub length,  $t$   
b Top slot width,  $d$

**Table 4** Performance of the proposed CPW fed slot-loop antenna with change in tuning stub length

Slot-loop width, $w$ (mm)	Slot-loop length, $l$ (mm)	Slot width, $w_s$ (mm)	Tuning stub length, $t$ (mm)	Resonant frequency (GHz)	Bandwidth (MHz)	% bandwidth	Gain (dBi)	Rad. eff. (%)
16	42.5	1	2.05	1.9328	55.1	2.9	2.1	92.0
			3.05	1.9073	86.4	4.5	2.0	91.5
			4.05	1.8848	98.8	5.2	2.1	93.0
			5.05	1.8720	102.1	5.5	2.1	93.1
			6.05	1.8545	104.2	5.6	2.0	91.5

the antenna bandwidth, once all other dimensions are optimised. A relatively small shift in resonant frequency is observed when the slot width is varied (Fig. 6). This is mainly because of the change in the effective slot-loop length with the variation of slot width. The results obtained are given in Table 3. In order to realise a very narrow bandwidth, the slot width  $w_s$  must be as thin as possible. The change in input impedance of the antenna is plotted for different values of slot width in Fig. 7. A negligibly small impedance variation is observed with a change in  $w_s$ , from 0.5 mm to 2.5 mm. As the input impedance shows negligible variation with the change in slot width, this bandwidth-controlling mechanism of the proposed design is less constrained.

The length of the CPW tuning stub can be adjusted to improve the input impedance matching for the antenna. Good matching can also be achieved by tuning the top slot width,  $d$ . This is evident from the return loss plots in Fig. 8. Both the gain and radiation efficiency remains unaffected with the change in  $d$ . The resonant frequency shows a slight shift because of the change in effective length of the slot with the top slot width. The electric fields are mainly concentrated at the top and bottom slot sections of the loop. From the simulation results, it can be seen that these sections are excited in phase. As observed in Table 4, the bandwidth shows some dependence on tuning stub length for smaller values, but for  $t > 4.05$  mm, it shows less reliance. No change in the omnidirectional radiation pattern is observed with changes in tuning stub length.

## 4 Conclusion

A novel design of a CPW-fed slot-loop antenna specifically made for narrowband omnidirectional operation has been presented. The typical broad bandwidth of slot-loop antennas is reduced to 2.9% and a good omnidirectional radiation pattern was achieved, in contrast to the usual bidirectional patterns of slot-loops. The proposed antenna has a gain of 2.1 dBi with comparatively less cross-polarisation in both the principal planes. The design gives 93% radiation efficiency. A good control of the antenna bandwidth was realised by varying the radiating slot width without significantly affecting the antenna input impedance or resonant frequency. Bandwidths in the range of 1.7–6.9% are achievable with good omnidirectional radiation characteristics.

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