

2018

Daylight characteristics of a polymer dispersed liquid crystal switchable glazing

A. Ghosh

University of Exeter, United Kingdom

Brian Norton

Technological University Dublin, brian.norton@tudublin.ie

T.K. Mallik

University of Exeter, United Kingdom

Follow this and additional works at: <https://arrow.tudublin.ie/engschmanart>

Recommended Citation

Norton, B., Ghose, A. & Mallick, T.K. (2018). Daylight Characteristics of a Polymer Dispersed Liquid Crystal Switchable Glazing. *Solar Energy Materials and Solar Cells*, vol. 174, pp. 572-576. doi: 10.1016/j.solmat.2017.09.047.

This Article is brought to you for free and open access by the School of Manufacturing and Design Engineering at ARROW@TU Dublin. It has been accepted for inclusion in Articles by an authorized administrator of ARROW@TU Dublin. For more information, please contact arrow.admin@tudublin.ie, aisling.coyne@tudublin.ie.



This work is licensed under a [Creative Commons Attribution-Noncommercial-Share Alike 4.0 License](https://creativecommons.org/licenses/by-nc-sa/4.0/)

Daylight characteristics of a polymer dispersed liquid crystal switchable glazing

Aritra Ghosh^{a, b, *}

a.ghosh@exeter.ac.uk aritra.ghosh_9@yahoo.co.in

Brian Norton^b

Tapas Mallick^a

^aEnvironmental and Sustainability Institute, University of Exeter, Penryn, Cornwall, UK

^bDublin Energy Lab, Dublin Institute of Technology, Dublin, Ireland

*Corresponding author at: Environmental and Sustainability Institute, University of Exeter, Penryn, Cornwall, UK.

Abstract

The daylighting performance of a polymer dispersed liquid crystal (PDLC) switchable glazing has been evaluated using an unfurnished outdoor south-facing test cell with a glazing-to-wall ratio of 1:9. Useful daylight illuminance levels (UDI) were determined for clear sunny, intermittent cloudy and overcast cloudy days. Daylight glare indexes (DGI_n) was calculated for the PDLC glazing in its transparent and translucent states. An electrically-actuated adaptive PDLC switchable glazing with transparency that varied between 27% and 71% was able to control daylight glare.

Keywords: adaptive; PDLC; glazing; daylight; UDI; glare

1 Introduction

Replacing artificial light with daylight (i) reduces the building energy consumption [1] (ii) enhances visual comfort [2] (iii) prevents or reduces eyes tiredness and fatigue [3] and (iv) achieves natural daylight colour rendering [4,5]. Reducing artificial lighting energy demand in building during the day requires appropriate daylighting design [6–8]. Occupant visual comfort can be maintained via the use of curtains, blinds and adaptive glazings that actively or passively adjust their optical properties [9–11].

Acceptable illuminances for work and study inside a room can vary between 100 and 2000 lx as shown in Table 1 [12].

Table 1 Acceptability of illumination.

alt-text: Table 1

		Acceptability	Activity	Reference
Illuminance level (Lux)	≥ 150	Comfort	Working space	[13]
	500	Comfortable	Office work	[14]
	500	Comfortable	Office work	[15]
	840–2146 (morning)	Comfortable	Office work	[4,5,15]
	782–1278 (afternoon)	Comfortable		
	700–1800	Comfortable	Computer work	[16]
	100–2000	Useful Daylight Illuminance	Any types of work	[12]

Switchable glazing includes electrochromic (EC) [17–19], gasochromic [20], thermochromic [21], thermotropic [22,23], liquid crystal (LC) [24], suspended particle device (SPD) [25–28] and phase change materials (PCM) [29]. These glazing can be electrically,

thermally, or chemically actuated. Electrical actuation of switchable glazings EC, SPD, and LC gives control of the switchability of glazing [30–34]. EC glazing changes its transparency from transparent to opaque state in the presence of direct current power supply. EC glazing can control NIR [35,36]. Higher switching time of EC glazing can be mitigated using suitable powering [37]. Degraded EC films (both based on W oxide and Ti oxide) can be rejuvenated by galvanostatic treatment [38–40]. Large scale (1.2 m × 0.8 m × 0.8 m and 1.2 m × 0.5 m × 0.5 m) EC device was also investigated using PASSYS test cell [41]. Daylight and glare performance of EC glazing has been evaluated theoretically in a hot climate in a west orientated wall [42–44] and evaluated experimentally performed for computer tasks [45]. Operated by an alternating current power supply, SPD glazing changes its state from opaque to transparent [46]. SPD glazing has a low switching time [47] intermediate transmission states between opaque and transparent state and high stability [48]. However controlling thermal comfort with SPD requires additional coated panes as the near infrared transmission is high [49]. Daylight and glare performance of SPD glazing has been evaluated [50]. In a liquid crystal (LC) glazing, LC films are sandwiched between two glass panes as shown in Fig. 1. Due to the anisotropic electrooptic properties of the LC material, transmitted light through the cell is controllable by applying appropriate voltages [51–54]. Polymer dispersed liquid crystals (PDLC) types are suitable compared to twisted nematic, ferroelectric and guest host type LC as they don't need polarizer to operate [55]. Liquid crystal droplets with diameters in the range of 1–20 to 20 μm in a polymer matrix form a PDLC. In the presence of an electric field LC droplets are aligned with electric field so allowing light passes through it. In the absence of an electric field LC droplets orient isotropically, scattering incident beam so becoming white translucent.

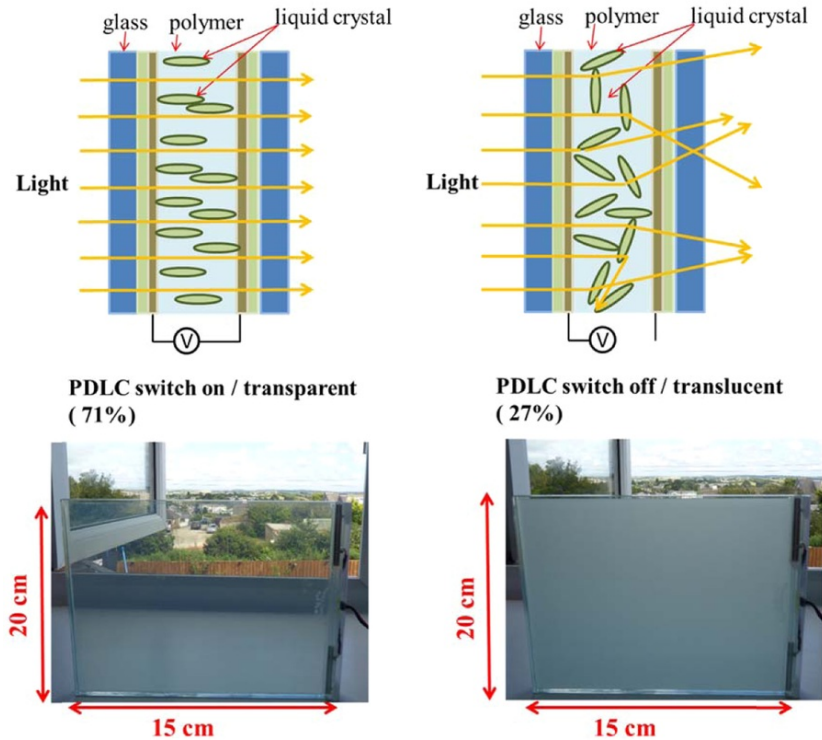


Fig. 1 The “transparent” and “translucent” states of a PDLC glazing. As PDLC glazings are intended for architectural applications, thus PDLC glazing daylight and glare results are essential information for building integrated PDLC switchable glazing. In this work first outdoor characterisation of PDLC glazing using test cell was performed to find out its glare and daylight control potential.

alt-text: Fig. 1

2 Methodology

Daylight glare index (DGI) [56,57] has been used to characterise EC glazing [42,43] and for SPD glazing [50] using data from a test cell. The DGI_N is given by

$$DGI_N = 10 \log_{10} 0.478 \sum_{i=1}^n \frac{L_{ext}^{1.6} \Omega_N^{0.8}}{L_{adp} + 0.07 \omega_N^{0.5} L_{win}} \quad (1)$$

where L_{ext} is the exterior luminance of the outdoor source including direct sunlight, diffuse skylight and reflected light from the ground and other external surfaces (cd/m²), L_{win} is window luminance (cd/m²), L_{adp} is adaptation luminance of the surroundings including reflections from internal surface (cd/m²), ω_N is solid angle subtended by the window, Ω_N is solid angle subtended by the glare source. Schematic diagram showing DGI_N is given in Fig. 2. The luminance level 5 provided by glazing, adaptation and exterior are

calculated from Eqs. (2)–(4).

$$L_{win} = \frac{E_{V,win}^{in}}{2\pi\phi} \quad (2)$$

$$L_{adp} = \frac{E_{V,adpt}^{in}}{\pi} \quad (3)$$

$$L_{neag} = \frac{E_{V,neag}^{in}}{2(\pi - 1)} \quad (4)$$

where

$$L_{ext} = L_{neag}$$

$$\omega_N = \frac{[ab \cos(\tan^{-1} X) \cos(\tan^{-1} Y)]}{d^2} \quad (5)$$

$$\Omega_N = 2\pi\phi \quad (6)$$

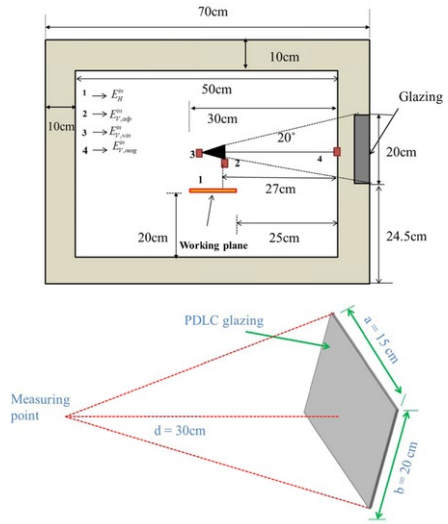


Fig. 2 Experimental set up used to obtain data for the calculation of DGI_N , with configuration factor calculation diagram.

alt-text: Fig. 2

The configuration factor ϕ was calculated from the Eq. (7) using (Fig. 2)

where

$$\phi = \frac{(A \tan^{-1} B + C \tan^{-1} D)}{\pi} \quad (7)$$

where

$$A = \frac{X}{\sqrt{(1 + X^2)}}, \quad B = \frac{Y}{\sqrt{(1 + X^2)}}, \quad C = \frac{Y}{\sqrt{(1 + Y^2)}}, \quad D = \frac{X}{\sqrt{(1 + Y^2)}}$$

X and Y can be calculated from Eqs. (8) and (9).

$$X = \frac{a}{2d} \quad (8)$$

$$Y = \frac{b}{2d} \quad (9)$$

where

a is the width of PDLC glazing, b is the height of PDLC glazing and d is the perpendicular distance from the observation place of the centre of glazing as shown in Fig. 2.

A PDLC glazing dimension of 0.2 m × 0.15 m was investigated that unpowered becomes translucent and powered become transparent. The PDLC glazing was connected with a 0–200 V variable AC supply. PDLC spectral measurements were performed using a LAMBDA 1050 UV/Vis/NIR Spectrophotometer. Fig. 3 shows the variation of PDLC transmission when “transparent” with 71% average transmittance and “translucent” with 27% average transmittance.

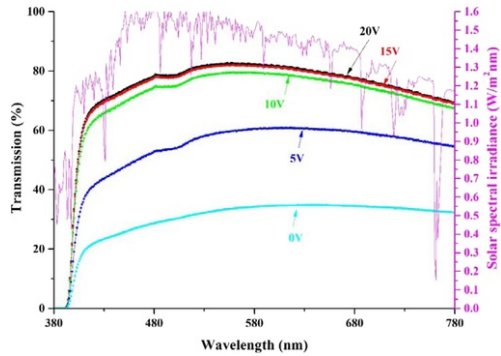


Fig. 3 Voltage dependant luminous transmission of a PDLC glazing in transparent, translucent and intermediate states.

alt-text: Fig. 3

A 0.7 × 0.7 m × 0.7 m test cell with unobstructed solar illuminance whose internal surfaces were painted with 0.8 reflectance matt white paint. The area of glazing on the test cell was in a ratio of 1:9. Six illuminance sensors were used. One on the vertical surface of the outside surface of the test cell and three inside the test cell. Horizontal measurements were made 27 cm distant from the glazing inner surface as shown in Fig. 2. All illuminance sensors had a 350–820 nm sensitivity spectral range with a spectral response curve adapted to human eye sensitivity [25,26,50]. Data were recorded at 1 min intervals. Outdoor experimental test cell characterisations were performed as functions of time, different types of day (clear, intermittent cloudy, overcast cloudy), and test-cell orientation (south) for two switching states 'transparent' and 'translucent'. Horizontal illuminances on a work plane inside the test cell and daylight glare index (DGI) were investigated using PDLC glazing transparent/switch on and translucent/ switch off conditions in the Dublin climate (53.3478°N latitude) for three days with different prevailing weather conditions.

3 Results and discussions

Internal illuminance into the test cell for PDLC glazing and exterior illuminance for clear sunny, intermittent cloudy and overcast cloudy days for Dublin are shown in Fig. 4. PDLC translucent perfectly achieved UDI level throughout the intermittent cloudy day. Due to higher diffuse transmission of PDLC translucent always offered higher UDI level.

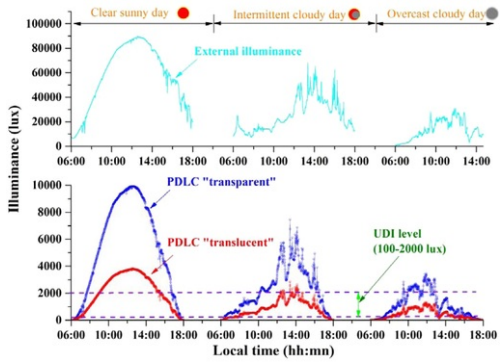


Fig. 4 External illuminance and internal illuminance for south facing PDLC transparent and translucent states for clear sunny, intermittent cloudy and overcast cloudy day in Dublin.

alt-text: Fig. 4

Figs. 5-7 show the daylight glare index (DGI_n) of PDLC glazing for its transparent and translucent state for clear sunny, intermittent cloudy and overcast cloudy sky conditions.

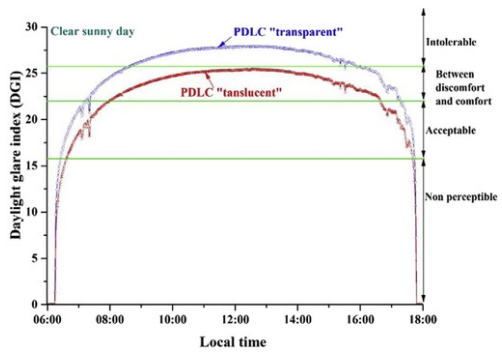


Fig. 5 DGI of PDLC glazing transparent and translucent states for a sunny day in Dublin.

alt-text: Fig. 5

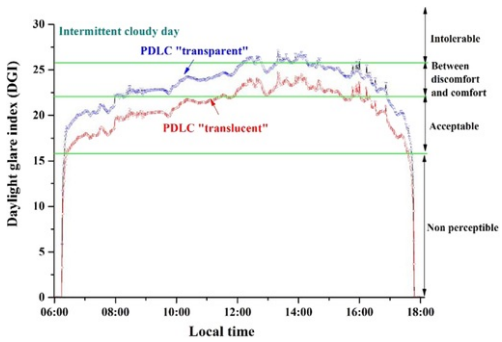


Fig. 6 DGI of PDLC glazing transparent and translucent states for an intermittent cloudy day in Dublin.

alt-text: Fig. 6

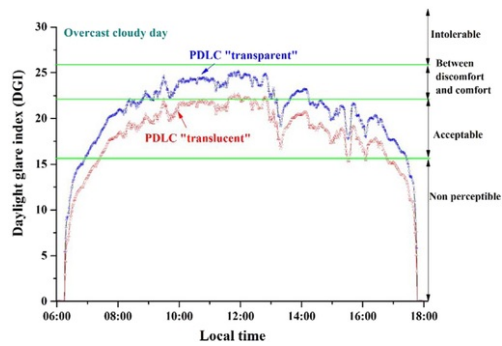


Fig. 7 DGI of PDLC glazing transparent and translucent states for an overcast cloudy day in Dublin.

alt-text: Fig. 7

The DGI represent the discomfort glare of occupant. DGI_N is the best method to evaluate as it deals with direct sunlight and vertical illuminance. In the equation L_{ext} was measured using illuminance sensor and shown in Fig. 4. The DGI of PDLC glazing in its transparent and translucent states was calculated using Eq. (1). The solid angles subtended by the glare source (Ω_N) and by the glazing (ω_N) were 0.057, 0.03 Sr and 0.35 Sr respectively.

For clear sunny day translucent PLDC always provided DGI level below the intolerable limit. For intermittent and overcast cloudy day translucent PDLC usually provided acceptable DGI level. PDLC glazing in its translucent state possess 83% haze which offer high diffuse light and increase the transmission in the switched off state [58]. Due to low contrast ratio (contrast ratio=transmission ratio between PDLC transparent and translucent) of this PDLC glazing variation of DGI level is less between two states. For a clear sunny day PDLC transparent was above the discomfort level where as translucent was above the comfort level. For intermittent day PDLC translucent was able to provide glare control from morning to mid-day and afternoon period. PDLC translucent was completely capable to control glare on an overcast cloudy day where as transparent state offered discomfort for short time span.

4 Conclusion

First outdoor daylighting characterisation using PDLC glazing was investigated using small scale test cell. Useful daylight illuminance (UDI) of a PDLC switchable glazing in “transparent” and “translucent” states has been measured using test cell for clear sunny, intermittent cloudy and overcast cloudy skies. It was found that PDLC “translucent” condition achieved the UDI level under intermittent and overcast cloudy day. Daylight glare index (DGI) was calculated for clear sunny, intermittent cloudy and overcast cloudy day. For clear sunny day PDLC glazing was not able to offer comfortable glare. However for intermittent and overcast cloudy day PDLC glazing's performance was impressive. Higher diffuse transmission on translucent state helped PDLC to offer higher transmission. This is suitable for building façade application where daylight penetration get higher priority than viewing. For self-powered (PV) PDLC application, excess power generated from PV can be stored during day time and stored power will be utilised in the night or cloudy day to make glazing transparent.

References

- [1] D.H. Li, A review of daylight illuminance determinations and energy implications, *Applied Appl. Energy* **87**, 2010, 2109–2118.
- [2] P.J. Littlefair, Prediction of Reflected Solar Dazzle reflected solar dazzle from Sloping Facades sloping facades, *Building and Environment Build. Environ.* **22**, 1987, 285–291.
- [3] N. Nasrollahi and E. Shokri, Daylight illuminance in urban environments for visual comfort and energy performance, *Renewable and Sustainable Renew. Sustain. Energy Reviews Rev.* **66**, 2016, 861–874.
- [4] L. Roache, E. Dewey and P. Littlefair, Occupant reaction to daylight in offices, *Lighting Research and Technology Light. Res. Technol.* **32**, 2000, 119–126.
- [5] L. Roache, Summer time performance of an automated lighting and blinds control system, *Lighting Research Technology Light. Res. Technol.* **34**, 2002, 11–25.
- [6] M. Bodart and A.D. Herde, Global energy savings in offices buildings by the use of daylighting, *Energy and Buildings Build.* **34**, 2002, 421–429.
- [7] A.D. Galasiu and J.A. Veitch, Occupant preferences and satisfaction with the luminous environment and control systems in daylit offices: a literature review, *Energy and Building Build.* **38**, 2006, 728–742.
- [8] X. Yu and Y. Su, Daylight availability assessment and its potential energy saving estimation –A–a literature review, *Renewable and Sustainable Renew. Sustain. Energy Reviews Rev.* **52**, 2015, 494–503.
- [9] F. Favoino, M. Overend and Q. Jin, The optimal thermos-optical properties and energy saving potential of adaptive glazing technologies, *Applied Appl. Energy* **156**, 2015, 1–15.

- [10] A. Ghosh, B. Norton and A. Duffy, Measured thermal & daylight performance of an evacuated glazing using an outdoor test cell, *Applied Appl. Energy* **177**, 2016, 196–203.
- [11] B.D. Hatton, I. Wheeldon, M.J. Hancock, M. Kolle, J. Aizenberg and D.E. Ingber, An artificial vasculature for adaptive thermal control of windows, *Solar Sol. Energy Materials and Solar Mater. Sol. Cells* **117**, 2013, 429–436.
- [12] A. Nabil and J. Mardaljevic, Useful daylight illuminances: a replacement for daylight factors, *Energy and Building Build.* **38**, 2006, 905–913.
- [13] E.S. Lee, D.L. DiBartolomeo and S. Selkowitz, [The effect of Venetian blinds on daylight photoelectric control performance](#), *The effect of Venetian blinds on daylight photoelectric control performance Journal of Illuminating Engineering Society J. Illum. Eng. Soc.* **28**, 1999, 3–23.
- [14] Chartered Institute of Building Services Engineers (CIBSE) (CIBSE), 1999. Daylighting and window design (design). Lighting guide 10.
- [15] E. Vine, E. Lee, R. Clear, D. DiBartolomeo and S. Selkowitz, Office workers response to an automated venetian blind and electric lighting system—a pilot study, *Energy and Building Build.* **28**, 1998, 205–218.
- [16] C.F. Reinhart, Effects of interior design on the daylight availability in open plan offices, *Conference Proceedings of the Conf. Proc. ACEEE Summer Study Energy Efficient Buildings Effic. Build.* 2002, 1–12.
- [17] C.G. Granqvist, Electrochromic tungsten oxide films: review of progress 1993–1998, *Solar Sol. Energy Materials and Solar Mater. Sol. Cells* **60**, 2000, 201–262.
- [18] C.G. Granqvist, Oxide electrochromics: an introduction to devices and materials, *Solar Sol. Energy Materials and Solar Mater. Sol. Cells* **99**, 2012, 1–13.
- [19] C.G. Granqvist and V. Wittwer, Materials for solar energy conversion: an overview, *Solar Sol. Energy Materials and Solar Mater. Sol. Cells* **54**, 1998, 39–48.
- [20] W. Feng, L. Zou, G. Gao, G. Wu, J. Shen and W. Li, Gasochromic smart window: optical and thermal properties, energy simulation and feasibility analysis, *Solar Sol. Energy Materials and Solar Mater. Sol. Cells* **144**, 2016, 316–323.
- [21] V. Costanzo, G. Evola and L. Marletta, Thermal and visual performance of real and theoretical thermochromic glazing solutions for office buildings, *Solar Sol. Energy Materials and Solar Mater. Sol. Cells* **149**, 2016, 110–120.
- [22] O. Muehling, A. Seeboth, T. Haeusler, R. Ruhmann, E. Potchius and R. Vetter, Variable solar control using thermotropic core/shell particles, *Solar Sol. Energy Materials and Solar Mater. Sol. Cells* **93**, 2009, 1510–1517.
- [23] P. Nitz and H. Hartwig, Solar control with thermotropic layers, *Solar Sol. Energy* **79**, 2005, 573–582.
- [24] D.J. Gardiner, S.M. Morris and H.J. Coles, High-efficiency multi stable switchable glazing using smectic A liquid crystals, *Solar Sol. Energy Materials & Solar Mater. Sol. Cells* **93**, 2009, 301–306.
- [25] A. Ghosh, B. Norton and A. Duffy, Measured overall heat transfer coefficient of a suspended particle device switchable glazing, *Applied Appl. Energy* **159**, 2015, 362–369.
- [26] A. Ghosh, B. Norton and A. Duffy, Behaviour of a SPD switchable glazing in an outdoor test cell with heat removal under varying weather conditions, *Applied Appl. Energy* **180**, 2016, 695–706.
- [27] D. Barrios, R. Vergaz, J.M.S.N. Pena, B.G. Cámara, C.G. Granqvist and G.A. Niklasson, Simulation of the thickness dependence of the optical properties of suspended particle devices, *Solar Sol. Energy Materials and Solar Mater. Sol. Cells* **143**, 2015, 613–622.
- [28] R. Vergaz, J.M.S.N. Pena, D. Barrios, C. Va'zquez and P.C. Lallana, Modelling and electro-optical testing of suspended particle devices, *Solar Sol. Energy Materials and Solar Mater. Sol. Cells* **92**, 2008, 1483–1487.
- [29] F. Goia, M. Zinzi, E. Carnielo and V. Serra, Spectral and angular solar properties of a PCM-filled double glazing unit, *Energy Building Build.* **87**, 2015, 302–312.
- [30] A. Ghosh, B. Norton and A. Duffy, Effect of atmospheric transmittance on performance of adaptive SPD-vacuum switchable glazing, *Solar Sol. Energy Materials and Solar Mater. Sol. Cells* **161**, 2017, 424–431.
- [31] A. Ghosh, B. Norton and A. Duffy, Effect of sky clearness index on transmission of evacuated (vacuum) glazing, *Renewable Renew. Energy* **105**, 2017, 160–166.
- [32] A. Ghosh, B. Norton and A. Duffy, Effect of sky conditions on light transmission through a suspended particle device switchable glazing, *Solar Sol. Energy Materials and Solar Mater. Sol. Cells* **160**, 2017, 134–140.
- [33] S.D. Rezaeia, S. Shannigrahi and S. Ramakrishna, A review of conventional, advanced, and smart glazing technologies and materials for improving indoor environment, *Solar Sol. Energy Materials and Solar Mater. Sol. Cells* **159**, 2017, 26–51.
- [34] B.P. Jelle, A. Hynd, A. Gustavsen, D. Arasteh, H. Goudey and R. Hart, Fenestration of today and tomorrow: a state-of-the-art review and future research opportunities, *Solar Sol. Energy Materials and Solar Mater. Sol. Cells* **96**, 2012, 1–28.
- [35] J.S. Hale and J.A. Woollam, Prospects of IR emissivity control using electrochromic structures, *Thin Solid Films* **339**, 1999, 174–180.
- [36] A.P. Schuster, D. Nguyen and O. Caporaletti, Solid state electrochromic infrared switchable windows, *Solar Sol. Energy Materials Mater.* **13**, 1986, 153–160.
- [37] J.D. Engfeldt, P. Georen, C. Lagergren and G. Lindbergh, Methodology for measuring current distribution effects in electrochromic smart windows, *Appl. Opt.* **50**, 2011, 5639, <https://doi.org/10.1364/AO.50.005639>.

- [38] M.A. Arvizu, R.T. Wen, D. Primetzhofer, J.E. Klemberg-Sapieha, L. Martinu, G.A. Niklasson and C.G. Granqvist, Galvanostatic [ion detrapping rejuvenates oxide thin films](#), *ACS Appl. Mater. Interfaces* **7**, 2015, 26387–26390.
- [39] R.-T. Wen, C.G. Granqvist and G.A. Niklasson, Eliminating degradation and uncovering ion-trapping dynamics in electrochromic WO₃ thin films, *Nat. Mater.* **14**, 2015, 996–1001.
- [40] R.T. Wen, G.A. Niklasson and C.G. Granqvist, Sustainable [Rejuvenation](#) of [Electrochromic](#) WO₃ [Films](#), *ACS Appl. Mater. Interfaces* **7**, 2015, 28100–28104.
- [41] A. Kraft and M. Rottmann, Properties, performance and current status of the laminated electrochromic glass of Gesimat, *Sol. Energy Mater. Sol. Cells* **93**, 2009, 2088–2092.
- [42] A. Piccolo, A. Pennisi and F. Simone, Daylighting performance of an electrochromic window in a small scale test-cell, *Sol. Energy* **83**, 2009, 832–844.
- [43] A. Piccolo and F. Simone, Effect of switchable glazing on discomfort glare from windows, *Building Environment* **44**, 2009, 1171–1180.
- [44] M. Moeck, E.S. Lee, M.D. Rubin, R.T. Sullivan and S.E. Selkowitz, Visual quality assessment of electrochromic and conventional glazings, *Solar Energy Materials & Solar Cells* **54**, 1998, 157–164.
- [45] E.S. Lee, D.L. DiBartolomeo and S.E. Selkowitz, Daylighting control performance of a thin-film ceramic electrochromic window: field study results, *Energy and Building* **38**, 2006, 30–44.
- [46] A. Ghosh, B. Norton and A. Duffy, First outdoor characterisation of a PV powered suspended particle device switchable glazing, *Solar Energy Materials & Solar Cells* **157**, 2016, 1–9.
- [47] A. Ghosh and B. Norton, Durability of switching behaviour after outdoor exposure for a suspended particle device switchable glazing, *Solar Energy Materials and Solar Cells* **163**, 2017, 178–184.
- [48] A. Ghosh and B. Norton, Interior colour rendering of daylight transmitted through a suspended particle device switchable glazing, *Solar Energy Materials and Solar Cells* **163**, 2017, 218–223.
- [49] A. Ghosh, B. Norton and A. Duffy, Measured thermal performance of a combined suspended particle switchable device evacuated glazing, *Applied Energy* **169**, 2016, 469–480.
- [50] A. Ghosh, B. Norton and A. Duffy, Daylighting performance and glare calculation of a suspended particle device switchable glazing, *Solar Energy* **132**, 2016, 114–128.
- [51] Y. Ajhaneyulu and D.W. Yoon, A PCGH liquid crystal window to control solar [energy](#), *Materials Solar Energy Mater.* **14**, 1986, 223–232.
- [52] C.M. Lampert, Large-area smart glass and integrated photovoltaics, *Solar Energy Materials and Solar Cells* **76**, 2003, 489–499.
- [53] C.M. Lampert, Optical-switching technology for glazings, *Thin Solid Films* **236**, 1993, 6–13.
- [54] C.M. Lampert, Smart switchable glazing for solar energy and daylight control, *Solar Energy Materials and Solar Cells* **52**, 1998, 207–221.
- [55] G. Macrelli, Optical [characterization](#) of commercial large area liquid crystal devices, *Solar Energy Materials and Solar Cells* **39**, 1995, 123–131.
- [56] A.A. Nazzal, A new daylight glare evaluation method Introduction of the monitoring protocol and calculation method, *Energy and Building* **33**, 2001, 257–265.
- [57] A.A. Nazzal, A new evaluation method for daylight discomfort glare, *International Journal of Industrial Ergonomics* **35**, 2005, 295–306.
- [58] **A. Ghosh, T.K. Mallick, Evaluation of optical properties and protection factors of a PDLC switchable glazing for low energy building integration, Solar Energy Materials and Solar Cells, (Accepted)** [A. Ghosh and T.K. Mallick, Evaluation of optical properties and protection factors of a PDLC switchable glazing for low energy building integration, Sol. Energy Mater. Sol. Cells 2017, \(In press\).](#)

Highlights

- Daylight indices and factors have been calculated for a PDLC glazing “translucent” and “transparent” states.
 - Voltage [dependent](#) transmission of a PDLC glazing is reported.
-

Queries and Answers

Query:

Please confirm that given names and surnames have been identified correctly and are presented in the desired order, and please carefully verify the spelling of all authors.

Answer: Tapas Mallick will be T.K. Mallick

Query:

Your article is registered as a regular item and is being processed for inclusion in a regular issue of the journal. If this is NOT correct and your article belongs to a Special Issue/Collection please contact m.ayyemperumal@elsevier.com immediately prior to returning your corrections.

Answer: Yes this is regular item and regular issue

Query:

Please validate if the address for the corresponding author that has been added here is correct.

Answer: All are correct

Query:

Highlights should consist of 3 – 5 bullet points. There are less bullet points provided. Please edit the highlights to meet the requirement.

Answer: Experiment was performed using outdoor test cell

Query:

Please complete and update the reference given here (preferably with a DOI if the publication data are not known): Ref. [58]. For references to articles that are to be included in the same (special) issue, please add the words 'this issue' wherever this occurs in the list and, if appropriate, in the text.

Answer: please delete this